APPENDIX I

REGIONAL UPLAND SOIL PROFILE

DRAFT

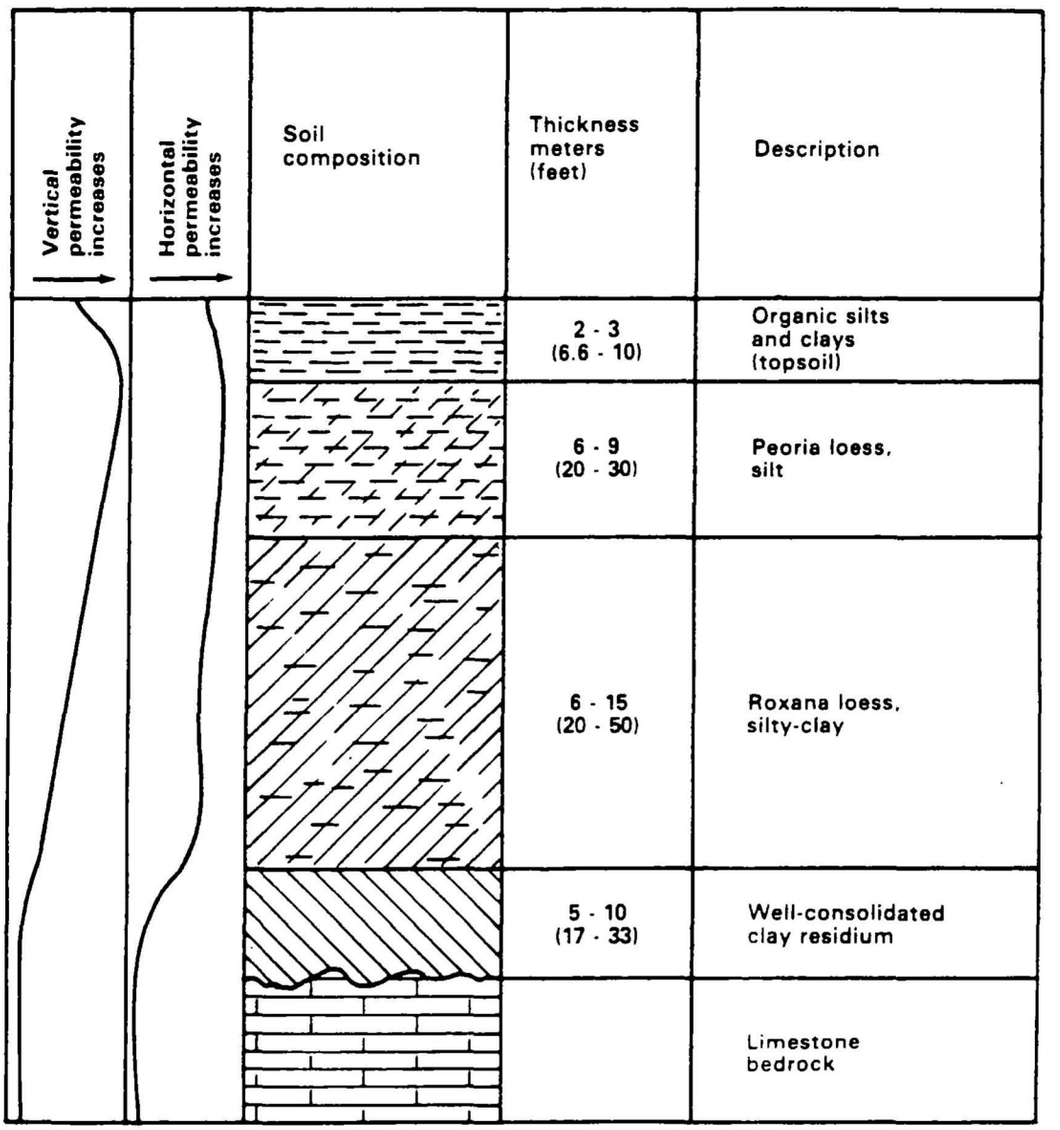


Figure 2.8 Soil profile of upland loessal soil

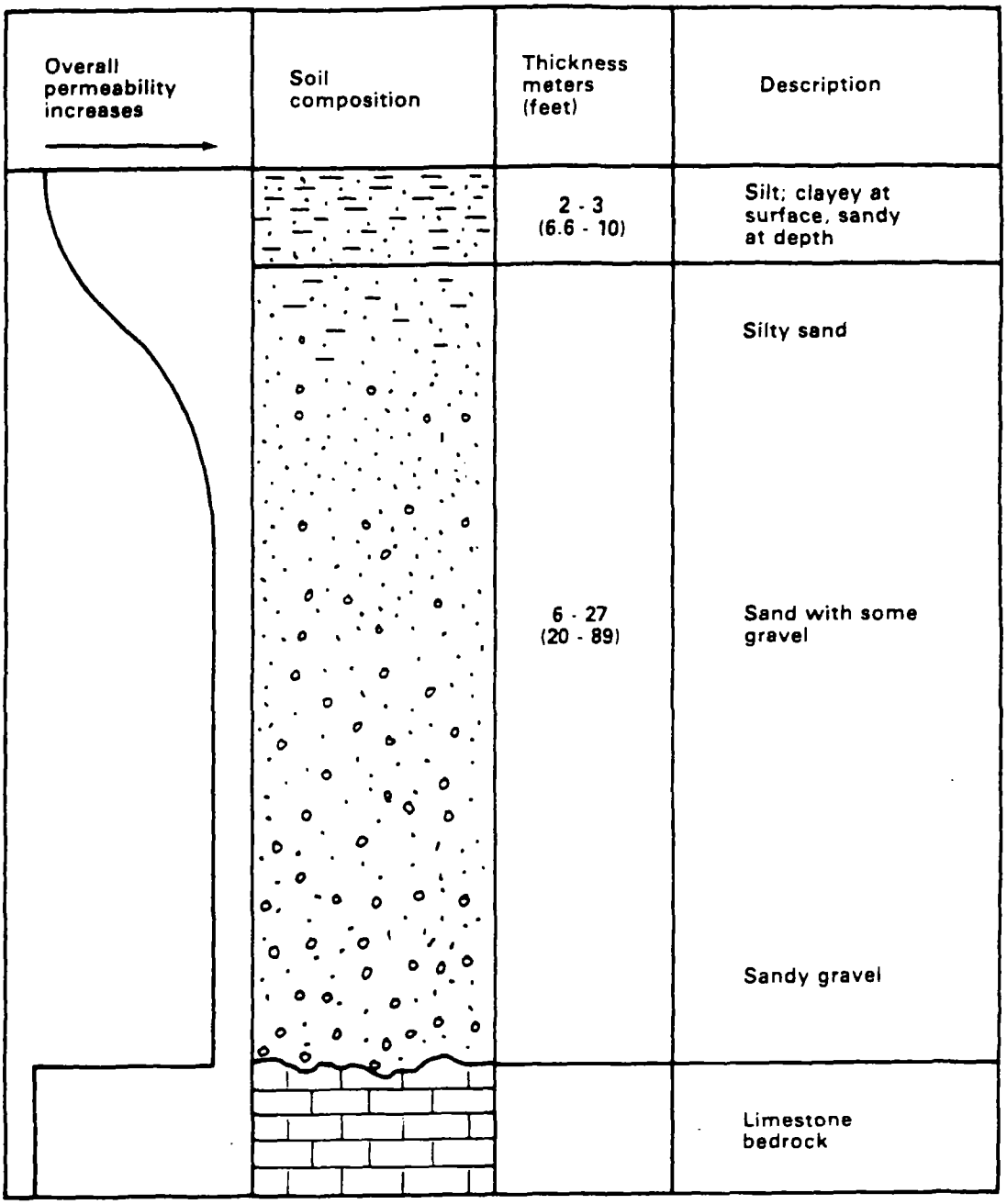


Figure 2.6 Soil profile of river alluvium

APPENDIX J

PRECIPITATION DATA

DRAFT

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
1938 Totals	**1938**	**0**	**1.05**	**0.28**	**0.61**	**0.53**	**0.32**	**2.14**	**1.6**	**0.93**	**2.65**	**2.38**	**0.31**	**0.6**	**0.09**	**0.04**	**0.72**	**1.17**	**3**	**0.39**	**0.2**	**0.14**	**1.55**	**1**	**1.06**	**0**	**1.03**	**0.2**	**1.39**	**0.14**	**0.37**	**0.01**	**25.9**
January	1																																
Feburary	2																																
March	3																																
April	4	0	0	0	0.01	0.11	0.03	0.07	0.57	0.85	0	0	0	0	0	0	0.43	0.05	0.2	0	0.1	0	0	0	0.21	0	0	0	0.06	0	0.37		3.06
May	5	0	0	0	0	0.37	0	0	0.93	0	0	0	0	0.02	0.01	0	0	0.18	0.05	0	0.1	0	0.66	0.84	0.83	0	0	0.01	0.27	0	0	0	4.27
June	6	0	0.01	0	0.02	0	0	0.34	0	0.08	2.63	2.38	0.14	0	0	0	0	0	0	0.05	0	0	0	0	0.02	0	0.78	0.01	0	0	0		6.46
July	7	0	0	0	0	0	0	0	0.02	0	0	0	0	0	0	0	0	0.24	1.7	0	0	0.07	0	0	0	0	0	0	0.45	0	0	0.01	2.49
August	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.04	0	0	0	0	0	0.07	0	0	0	0	0	0.18	0.61	0.14	0	0	1.04
September	9	0	0	0	0	0.05	0	0	0	0	0.02	0	0.04	0.54	0.08	0	0	0.26	0	0.01	0	0	0	0	0	0	0	0	0	0	0		1
October	10	0	0	0	0	0	0	0	0	0	0	0	0.12	0	0	0	0	0	0.67	0.33	0	0	0	0	0	0	0	0	0	0	0	0	1.12
November	11	0	0	0	0.58	0	0.29	1.73	0	0	0	0	0.01	0.04	0	0	0	0.44	0.38	0	0	0	0.27	0.16	0	0	0	0	0	0	0		3.9
December	12	0	1.04	0.28	0	0	0	0	0.08	0	0	0	0	0	0	0	0.29	0	0	0	0	0	0.62	0	0	0	0.25	0	0	0	0	0	2.56
1939 Totals	**1939**	**0.29**	**1.09**	**0**	**0.85**	**1.78**	**0.22**	**0.08**	**1.36**	**1.9**	**2.11**	**3.33**	**1.09**	**0.13**	**0.12**	**2.35**	**1.63**	**2.6**	**1.06**	**1.95**	**2.01**	**0.66**	**0.68**	**0.82**	**0.49**	**1.14**	**1.45**	**1.4**	**0.62**	**2.4**	**0.82**	**0.13**	**36.56**
January	1	0	0	0	0.4	0.36	0	0	0	0.17	0	0	0	0.1	0.03	0.08	0	0.34	0.01	0	0	0	0	0.17	0	0	0	0	0.44	1.41	0.42	0	3.93
Feburary	2	0.06	0	0	0	0	0	0	0	0.81	0	0	0	0	0	0	0	0	0.07	0.99	0.03	0.01	0	0	0.08	0.52	0	0.24	0.01				2.82
March	3	0	0	0	0.04	0.06	0	0	0	0	0.08	0.88	0	0	0	0	0	0	0.01	0	0	0	0	0	0	0	0.26	0.01	0	0.17	0	0.12	1.63
April	4	0	0.1	0	0	1.36	0	0	0	0	0.02	0	0	0	0.03	1.83	1.29	0.36	0.05	0	0.47	0.01	0	0	0	0	0.19	0	0	0	0		5.71
May	5	0	0	0	0	0	0	0.07	0.27	0.01	0.15	0.11	0	0	0.06	0	0	0	0	0.01	0	0	0	0	0	0	0.55	0.7	0.04	0	0	0	1.97
June	6	0	0	0	0	0	0	0	0.5	0.72	0.86	0	0.35	0.03	0	0	0	0	0	0.15	1.42	0.64	0.07	0	0	0	0	0.01	0	0	0		4.75
July	7	0	0	0	0.41	0	0	0	0.02	0	0	0	0	0	0	0.44	0.13	0	0.12	0.02	0	0	0	0.19	0	0.24	0.02	0	0.11	0	0	0	1.7
August	8	0	0.99	0	0	0	0	0	0.16	0	0	2.34	0.74	0	0	0	0.04	1.89	0.46	0.04	0	0	0.6	0.02	0	0.34	0	0	0	0	0	0	7.62
September	9	0	0	0	0	0	0	0	0	0.09	0.06	0	0	0	0	0	0.17	0	0	0	0	0	0	0	0	0	0	0	0	0.79	0		1.11
October	10	0	0	0	0	0	0.15	0	0.41	0.1	0.17	0	0	0	0	0	0	0	0	0	0	0	0	0	0.39	0.04	0.01	0.32	0	0.03	0.03	0	1.65
November	11	0	0	0	0	0	0.07	0.01	0	0	0.77	0	0	0	0	0	0	0.01	0.34	0.74	0.09	0	0	0	0.02	0	0	0	0	0	0.37		2.42
December	12	0.23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0.44	0	0	0.42	0.12	0.02	0	0	0.01	1.25
1940 Totals	**1940**	**0.21**	**0.78**	**0.17**	**0.47**	**0.34**	**1.68**	**0.74**	**0.01**	**0.26**	**0.5**	**3.87**	**0.86**	**0.56**	**0.7**	**0.8**	**1.43**	**1.29**	**1.71**	**0.77**	**0.13**	**0.47**	**0.3**	**0.66**	**0.11**	**0.19**	**0.87**	**1.56**	**1.57**	**0.08**	**1.36**	**0.28**	**24.73**
January	1	0	0	0	0.01	0	0.03	0.21	0	0.02	0.08	0	0	0.29	0.1	0	0	0.1	0.03	0	0	0	0	0.03	0	0	0	0	0	0	0	0	0.9
Feburary	2	0.08	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.12	0.41	0.31	0.03	0.02	0	0.13	0.05	0	0	0.31	0	0			1.46
March	3	0.01	0.78	0	0	0	0	0	0	0	0	0.02	0.7	0.09	0	0	0	0	0.16	0.01	0	0	0.01	0.03	0.03	0	0	0.07	0.36	0	0	0	2.27
April	4	0	0	0.17	0	0	0	0.23	0.01	0	0.01	0.66	0	0	0	0	0.03	0.41	0	0.01	0	0	0.29	0.03	0	0	0.01	0	0.21	0.06	1.36		3.49
May	5	0.12	0	0	0	0	0	0	0	0	0	0	0	0	0.25	0.02	0	0.51	0.48	0.44	0	0.32	0	0	0	0.1	0.02	0	0	0.01	0	0	2.27
June	6	0	0	0	0	0	0	0.3	0	0	0	0.49	0	0	0.06	0	0.1	0.05	0	0	0	0	0	0.21	0	0	0	0	0.96	0	0		2.17
July	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.3
August	8	0	0	0	0.01	0.34	0	0	0	0.01	0.38	0.22	0	0.04	0	0	0	0.1	0.62	0	0	0	0	0	0	0	0.04	1.02	0.02	0.01	0	0.02	2.83
September	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		0
October	10	0	0	0	0.42	0	1.65	0	0	0	0	0.04	0	0	0.28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.02	2.41
November	11	0	0	0	0.03	0	0	0	0	0.23	0.03	1.38	0	0	0	0	0	0	0	0	0.1	0.13	0	0.23	0	0.03	0.78	0	0	0	0		2.94
December	12	0	0	0	0	0	0	0	0	0	0	1.06	0.16	0.14	0.01	0.78	0	0	0.01	0	0	0	0	0	0.03	0.06	0.02	0.16	0.02	0	0	0.24	2.69
1941 Totals	**1941**	**0.76**	**0.71**	**1.02**	**1**	**1.78**	**1.28**	**0.43**	**0.21**	**2.03**	**1.15**	**0.82**	**0.13**	**0.78**	**1.2**	**0.96**	**0.68**	**2.6**	**0.16**	**1.87**	**0.01**	**0.74**	**2.4**	**0.38**	**3.54**	**0.69**	**0.85**	**0.14**	**0.13**	**0.69**	**1.37**	**0.86**	**31.37**
January	1	0.61	0	0	0.01	0	0	0	0	0	0	0	0	0.44	0.03	0.06	0.38	0.26	0	0	0	0	0.02	0.11	0.05	0.26	0.01	0	0	0	0.03	0	2.27
Feburary	2	0	0	0	0	0	0.07	0	0	0	0	0	0	0.19	0	0	0.01	0	0	0	0	0	0	0	0.04	0	0.15	0.02	0				0.48
March	3	0	0.01	0	0.01	0	0.01	0.03	0	0	0.44	0	0	0	0	0.06	0	0	0	0	0	0	0	0	0	0	0	0	0.02	0	0.01	0.13	0.72
April	4	0	0.24	0.68	0.45	0	0	0	0.11	0	0	0	0	0	0	0.84	0.13	1.31	0.04	1.65	0	0	0	0	0	0	0	0	0	0	0		5.45
May	5	0	0	0	0	0.36	0.38	0.27	0.04	0	0	0	0	0	0.68	0	0.05	0	0	0	0	0	0.36	0.01	0	0	0	0	0	0	0.17	0	2.32
June	6	0	0.32	0.04	0	0	0	0	0.06	0.85	0.2	0.81	0.01	0	0.03	0	0	0	0	0	0	0	0	0	0	0	0	0	0.11	0.11	0	0	2.54
July	7			0.28				0.02		0	0.13															0.03	0.04		0		0	0.02	0.52
August	8	0.04	0			0.07					0.38		0.01		0.09				0.09				0	0	0.87	0	0.25	0			0.37		2.17
September	9	0.1		0	0.17	0.3	0.01	0		0.31							0.09								2.57	0.1			0	0.65	0.15		4.45
October	10	0	0.14	0	0.36	0.41	0	0.1		0.87				0	0.37		0.02	1.03	0.03		0.01	0.74	0.82				0.4	0.01		0.04	0.64	0.68	6.67
November	11	0.01	0	0.02	0	0.64	0.81	0.01	0	0	0	0	0	0	0	0	0	0	0	0.22	0	0	1.07	0	0	0	0	0	0	0	0		2.78
December	12	0	0	0	0	0	0	0	0	0	0	0.01	0.11	0.15	0	0	0	0	0	0	0	0	0.13	0.26	0.01	0.3	0	0	0	0	0	0.03	1
1942 Totals	**1942**	**0.47**	**1.09**	**0.88**	**0.93**	**2.2**	**3.6**	**1.68**	**1.87**	**5.69**	**0.33**	**0.6**	**0.25**	**1.91**	**0.17**	**2.25**	**0.38**	**0.94**	**1.25**	**1.27**	**0.17**	**1.83**	**1.46**	**0.76**	**0.07**	**1.18**	**2.93**	**1.5**	**0.32**	**0.72**	**2.77**	**0.17**	**41.64**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0.21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.02	0	0	0	0	0	0	0	0	0	0	0	0.66	0.01	0.9
Feburary	2	0	0	0	0.55	0.04	0.55	0	0	0.17	0	0	0	0	0	0.09	0.36	0	0.01	0	0	0	0	0.62	0.05	0	0.09	0	0				2.53
March	3	0.1	0.04	0	0.05	0.02	0	0.6	0.01	0	0	0	0.16	0.34	0	0	0	0	0	0	0.02	0	0	0	0	0.3	0	0.03	0	0	0.08	0	1.75
April	4	0	0	0	0	0	0.49	0.5	0.71	0.34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0	0		2.05
May	5	0	0.75	0.29		0.62	0.06					0.09	0	0.49	0.05	0.56	0	0.2	0.55	0.02						0.03	0.17					0.09	3.97
June	6					0.37	1.01	0	0.01	0.8	0.28	0.51	0.01	1.08		0.24	0.02	0	0.67	0	0.13	0.39				0.8	2						8.32
July	7	0	0	0.03	0	0	0.01	0.02	0.81	4.04	0	0	0	0	0.08	0	0	0	0	0.04	0.02	0.26	0	0	0	0	0	0.03	0	0	0	0.07	5.41
August	8		0.27	0.48	0	0	1.48	0.17							0.04	1.31					0						0						3.75
September	9	0	0	0	0	0	0	0.2	0.32	0.02	0	0	0	0	0	0	0	0	0	0.79	0	0	0	0	0	0.04	0.09	0	0	0	0		1.46
October	10			0.08	0.01	0.15													0	0.21		0	0.01		0	0			0	0.7	2.03		3.19
November	11	0.01	0.03	0	0.32	0.82	0	0.19	0.01	0.32	0	0	0	0	0	0	0	0.74	0	0	0	1.18	1.15	0.14	0.02	0	0	0	0.14	0	0		5.07
December	12	0.15	0	0	0	0.18	0	0	0	0	0.05	0	0.08	0	0	0.05	0	0	0	0.21	0	0	0.3	0	0	0	0.58	1.44	0.18	0.02	0	0	3.24
1943 Totals	**1943**	**0.01**	**0.03**	**0.65**	**1.82**	**1.92**	**3.07**	**1.17**	**1.58**	**0.63**	**2.49**	**0.87**	**1.55**	**1.19**	**0.65**	**2.99**	**1.01**	**3.47**	**0.97**	**1.82**	**0.97**	**0.49**	**0.35**	**2.16**	**1.25**	**0.4**	**0.03**	**0.02**	**0.65**	**0.14**	**0.83**	**2.35**	**37.53**
January	1	0	0	0	0	0	0.16	0.02	0.01	0.05	0	0	0	0	0.08	0	0	0.02	0.07	0	0	0	0	0	0	0	0	0	0	0	0	0.19	0.6
Feburary	2	0	0	0.49	0	0.21	0	0	0	0	0	0	0	0	0	0.06	0	0	0	0	0	0	0	0	0	0	0	0	0				0.76
March	3	0	0.03	0	0	0.13	0.05	0	0	0	0.67	0	0	0	0	0.85	0.52	0	0.25	0.69	0	0	0	0	0	0	0.01	0	0	0	0	0	3.2
April	4				0		0.04	0		0.06		0.45	0.05	0.18	0		0.06			0.27	0.07	0	0.35	0.61		0.4	0	0					2.54
May	5		0		0	0	1.31	0.95	0.35	0.21	1.03	0.41	0	0.01	0.25	1	0.4	3.45	0.65	0.63	0.01			0.17	0.05		0.02				0.3	0	11.2
June	6				0.71	1.04	0.47		0.09		0.25			0.03	0.24	0.88	0.02				0.89	0		0.72	0.57	0			0		0		5.91
July	7	0	0	0.16	0.06	0	0								0				0	0.23		0.03			0.01				0.14	0.12	2.16	2.91
August	8	0	0	0	0.04	0	0	0	1.13	0.16	0	0	0	0	0	0	0.01	0	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0	1.35
September	9	0			1.01	0.28	0.05					0.01	1.34	0.67							0		0	0.1					0				3.46
October	10	0	0	0	0	0	0	0	0	0	0	0	0.16	0.3	0	0.2	0	0	0	0	0	0.46	0	0.56	0.62	0	0	0	0	0	0.41	0	2.71
November	11	0.01	0	0	0	0	0.9	0.2	0	0	0	0	0	0	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		1.12
December	12	0	0	0	0	0.26	0.09	0	0	0.15	0.54	0	0	0	0.07	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0.65	0	0	0	1.77
1944 Totals	**1944**	**0.53**	**1.23**	**1.62**	**1.08**	**0.76**	**0.2**	**0.34**	**1.4**	**0.91**	**3.02**	**2.35**	**1.31**	**0.09**	**1.21**	**0.62**	**0**	**0.56**	**0.63**	**0.66**	**0.34**	**3.13**	**5.24**	**1.12**	**0**	**2.28**	**1.19**	**0.76**	**1.41**	**0.22**	**0.69**	**0**	**34.9**
January	1	0	0.04	0.02	0.01	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.12	0	0	0	0	0.2
Feburary	2	0.07	0.24	0	0	0	0	0	0	0	0.4	0	0	0	0.26	0	0	0.07	0	0	0	0.65	0.01	0	0	0.42	0	0	0.53	0			2.65
March	3	0	0	0.41	0.1	0	0.19	0	0	0	0	0.08	0.27	0.07	0	0	0	0	0	0.52	0.39	0	0	0	0	0.15	0.26	0	0.27	0	0	0	2.71
April	4	0.01	0	0	0	0	0	0.25	0	0.36	2.42	0.08	0	0	0.94	0.37	0	0.11	0	0	0	0	4.15	0.32	0	0	0	0.06	0	0	0.47		9.54
May	5	0.45	0.67	0.67	0	0	0	0	0.68	0.05	0	0	0	0.02	0	0	0	0	0	0	0.04	0.02	1.07	0.59	0	0	0	0	0	0.2	0	0	4.46
June	6	0	0	0	0	0	0	0	0	0.02	0	0	1	0	0	0.23	0	0	0.11	0	0	0.14	0	0	0	0.61	0.08	0	0	0	0		2.19
July	7								0.63			0.83						0.38								0.87	0.25			0.01			2.97
August	8				0.3	0							0.04			0.02	0	0				2.07	0.01			0.01	0.57	0.01			0.22		3.25
September	9	0	0	0	0	0	0	0	0	0	0	1.28	0	0	0	0	0	0	0	0	0.26	0.25	0	0.21	0	0	0	0.35	0.61	0	0		2.96
October	10	0	0.28	0	0.67	0.05	0	0	0	0	0	0.07	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.07
November	11	0	0	0.52	0	0	0.01	0	0.09	0	0	0	0	0	0.01	0	0	0	0	0.27	0.04	0	0	0	0	0.17	0.03	0	0	0.01	0		1.15
December	12	0	0	0	0	0.7	0	0.09	0	0.48	0.2	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0	0.05	0	0.22	0	0	0	0	1.75
1945 Totals	**1945**	**1.74**	**3.1**	**0.28**	**0.5**	**1.11**	**0.72**	**2.28**	**1.04**	**1.09**	**0.47**	**1.66**	**3**	**5.96**	**2.77**	**0.25**	**2.92**	**0.74**	**2.94**	**0.68**	**0.65**	**3.33**	**0.2**	**0.18**	**1.2**	**2.34**	**0.69**	**1.79**	**0.48**	**1.34**	**1.95**	**0.15**	**47.55**
January	1	0	0	0	0	0	0	0	0.19	0	0	0	0	0	0.21	0.06	0	0	0	0.33	0	0.13	0	0	0	0.02	0	0.03	0	0.13	0	0	1.1
Feburary	2	0	0.01	0	0.01	0	0	0	0	0	0	0	0	0.07	0	0	0.5	0.12	0	0	0.18	0.92	0	0.01	0	0.44	0.17	0	0.06				2.49
March	3	0.2	1.21	0	0.02	0.82	0.71	0	0	0	0	0.01	0	0	0	0.04	0.01	0	0.55	0.25	0.17	0.01	0	0	0	1.4	0	0	0	0.86	1.37	0	7.63
April	4	0.51	0.68	0.09	0.41							0.06	1.19	1.09	0.78	0.07	0.5		0	0.06	0.02			0	0.16	0.21	0.03	0.05	0.27				6.18
May	5	0.19	0.1	0.18	0.06		0	0.3		0.07	0				1.02	0.08	0.45	0.08			0	0		0		0.07		0	0.08	0.02	0.01		2.71
June	6	0.23	0			0.11	0.01	1.66	0.06	0.39		0.05	0.83	0	0.04	0	1.46	0.48	1.64		0.02	0.08				0.14	0	0.11		0.15	0.41		7.87
July	7	0	0	0	0	0	0	0	0.28	0.32	0	0	0	0	0.46	0	0	0	0	0	0	0	0	0	0	0	0	0.32	0	0	0	0	1.38
August	8	0	1.07	0	0	0.18	0	0	0	0	0.03	1.54	0	0	0.07	0	0	0	0.25	0	0	0.44	0	0	0	0	0	0	0	0	0	0	3.58
September	9	0	0	0	0	0	0	0.32	0.15	0.31	0.44	0	0.34	4.61	0.03	0	0	0	0	0	0	1.14	0.19	0.08	0.57	0.06	0.16	1.28	0.07	0.13	0.16		10.04
October	10	0.42	0	0	0	0	0	0	0	0	0	0	0	0	0.16	0	0	0	0	0	0	0.56	0.01	0	0.07	0	0	0	0	0	0	0	1.22
November	11	0.08	0.03	0	0	0	0	0	0.36	0	0	0	0.49	0	0	0	0	0	0	0.03	0.26	0.05	0	0	0	0	0.33	0	0	0	0		1.63
December	12	0.11	0	0.01	0	0	0	0	0	0	0	0	0.15	0.19	0	0	0	0.06	0.5	0.01	0	0	0	0.09	0.4	0	0	0	0	0.05	0	0.15	1.72
1946 Totals	**1946**	**4.31**	**3.46**	**2**	**0.12**	**3.56**	**1.5**	**0.13**	**0.7**	**1.81**	**2.32**	**1.04**	**0.93**	**1.51**	**2.68**	**5.97**	**2.55**	**2.67**	**0.3**	**1.88**	**1.54**	**0**	**0.53**	**0.62**	**0.72**	**0.92**	**0.12**	**0.01**	**1.26**	**0.67**	**0.88**	**3.53**	**50.24**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0	0	0	0.05	0.02	0	0	0.46	0.05	0	0.51	0	0	0	0	0	0	0	0	0.28	0	0	0	0.01	0	0	0	0	0	0	0	1.38
Feburary	2	0	0	0	0	0.3	0	0	0	0	0	0	0.18	1.06	0.02	0	0	0	0.03	0.39	0	0	0	0.05	0	0	0	0	0				2.03
March	3	0.06	0	0	0.03	0.88	0.36	0	0.01	0	0	0	0	0	0.34	0	0	0.72	0.23	0.01	0	0	0	0.05	0	0	0	0	0	0.53	0	0	3.22
April	4	0	0	0	0	0.05	0	0	0	0.05	0	0.14	0	0	0	0.73	0	0	0	0	0	0	0	0.35	0	0	0	0	0.21	0	0.87		2.4
May	5	0.29	0.05	0.48	0	0	0.05	0	0	0.1	1.85	0.26	0	0	0.11	0.1	0	0.89	0	0.02	0	0	0	0.16	0.08	0	0.08	0	0	0	0	0.62	5.14
June	6	0.51	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0.54	0	0	0.04	1.11	0	0	0	0	0	0.01	0	0	0	0.09	0		2.31
July	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.42	0	0.27	0.87	0	0	0	0	0	0	0	0	0	0	0	1.56
August	8	0	0.95	1.45	0	2.31	0	0	0.23	0	0	0	0.18	0.45	2.21	4.31	2.35	0.01	0	0	0	0	0.09	0	0.14	0	0	0	0.1	0	0	0	14.78
September	9	1.27	0	0	0	0	0	0	0	0	0.11	0	0	0	0	0	0	0	0	0	0.39	0	0.44	0.01	0	0	0	0	0	0	0		2.22
October	10	0	0	0	0	0	0	0	0	0	0.15	0	0	0	0	0	0.01	0.63	0	0.08	0	0	0	0	0.35	0	0	0	0	0	0.01	2.91	4.14
November	11	2.18	2.45	0.07	0.04	0	1.09	0.13	0	1.18	0	0	0	0	0	0.29	0.19	0	0	0	0	0	0	0	0.14	0.91	0.04	0	0	0	0		8.71
December	12	0	0	0	0	0	0	0	0	0.43	0.21	0.13	0.57	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0.95	0.05	0	0	2.35
1947 Totals	**1947**	**1.28**	**0.57**	**0.54**	**1.06**	**1.17**	**0.21**	**0.25**	**0.4**	**0.11**	**2.14**	**0.39**	**0.16**	**0.53**	**1.07**	**0.87**	**0.12**	**0.31**	**0.23**	**0.39**	**3.11**	**1.81**	**0.06**	**0.45**	**2.26**	**2.98**	**0.69**	**2.46**	**0.59**	**1.79**	**3**	**2.63**	**33.63**
January	1	0.19	0.33	0.02	0	0	0	0.04	0	0	0	0	0	0	0	0	0	0	0	0	0.09	0	0	0	0	0	0	0	0	1.41	0	0	2.08
Feburary	2	0	0	0	0	0	0.02	0	0	0	0	0	0.1	0	0	0	0	0	0.01	0	0	0	0	0	0	0	0	0	0.14				0.27
March	3	0.13	0	0	0	0.19	0.08	0	0	0	0	0	0	0.53	0	0	0.02	0.04	0	0.26	0.1	0	0	0	0.23	0	0.19	0.58	0	0	0	0.23	2.58
April	4	0.07	0	0.18	0.28	0.26	0	0	0	0.11	0.81	0.01	0	0	0	0.6	0.02	0	0	0.1	0.43	0	0	0.34	0.98	1.01	0	0	0		0		5.2
May	5	0.16	0.24	0	0	0.01	0	0	0	0	0	0	0.06	0	0	0.09	0.08	0.06	0	0	1.66	0	0	0	0.38	0.05	0	0.01	0.38	0.04	0	0.01	3.23
June	6	0.63	0	0	0	0.47	0	0.01	0.4	0	0	0	0	0	0	0	0	0.21	0.11	0.03	0.14	0	0	0	0	0.68	0	1.42	0	0.34	3		7.44
July	7	0	0	0	0	0.24	0.01		0	0	0	0	0	0	0	0	0			0	0.69	0	0	0	0	0.02	0	0	0	0	0	0	0.96
August	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0.36	0.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.09	0.55
September	9	0	0	0	0	0	0	0	0	0	0.35	0.37	0	0	0.46	0.07	0	0	0	0	0	1.78	0	0	0	0	0	0	0	0	0		3.03
October	10	0.04	0	0	0.4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.67	1.22	0.5	0.45	0.07	0	0	0.7	4.05
November	11	0.06	0	0	0.17	0	0.1	0.04	0	0	0.85	0.01	0	0	0.25	0.01	0	0	0.11	0	0	0.03	0.06	0.11	0	0	0	0	0	0	0		1.8
December	12	0	0	0.34	0.21	0	0	0.16	0	0	0.13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.6	2.44
1948 Totals	**1948**	**1.72**	**0.55**	**0.25**	**2.39**	**6.46**	**1.7**	**0.16**	**0.39**	**0.62**	**1.34**	**0.69**	**2.05**	**1.36**	**0.27**	**1.4**	**1.81**	**0.11**	**0.45**	**1.78**	**0.68**	**2.37**	**1.05**	**0.73**	**0.41**	**3.54**	**2.22**	**2.08**	**1.08**	**0.81**	**0.91**	**0.88**	**42.26**
January	1	0.35	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0	0	0	0	0.18	0	0	0	0.12	0	0	0	0	0.19	0.85
Feburary	2	0	0	0.2	0	0.22	0	0	0	0	0	0.04	0.07	0.4	0	0	0	0	0	0	0	0.11	0	0	0	0.01	0	0.68	0	0			1.73
March	3	0.67	0.12	0	0	0.05	0.48	0	0	0	0.4	0.07	0	0	0	0	0	0	0.01	0	0	1.77	0.3	0.55	0	0	1.21	0.01	0	0	0.35	0.41	6.4
April	4	0	0	0	0	0.06	0.22	0	0	0	0.03	0.36	0.48	0.02	0	0	0	0	0	0	0	0	0	0	0.03	0.03	0.07	0	0	0	0.02		1.32
May	5	0.32	0.07	0	0.65	0.05	0.07	0	0	0	0.05	0.17	0.09	0	0	0.97	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.44
June	6	0	0	0	0	1.08	0	0	0.01	0	0	0	0	0	0	0.15	0	0.11	0.09	0	0.5	0.07	0.48	0	0	0.15	0.29	1.37	0.55	0.27	0		5.12
July	7	0	0	0	0.75	4.68	0	0	0	0	0.03	0.03	0.22	0.93	0	0.23	0	0	0	1.72	0.18	0.03	0.09	0	0	3.35	0.43	0	0	0	0.02	0	12.69
August	8	0	0	0	0.59	0	0	0.02	0	0	0	0	1.07	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0.1	0.02	0	0	0.27	0	2.08
September	9	0	0	0.05	0	0.16	0.15	0	0.35	0	0	0	0	0	0	0	0	0	0	0	0	0.32	0	0	0	0	0	0	0.14	0.54	0		1.71
October	10	0	0	0	0	0	0.78	0.14	0.03	0	0.83	0.02	0	0	0	0	1.51	0	0	0	0	0.04	0	0	0	0	0	0	0	0	0.25	0.28	3.88
November	11	0.38	0.36	0	0.4	0.01	0	0	0	0.62	0	0	0.12	0	0	0	0.3	0	0.25	0.06	0	0.03	0	0	0	0	0	0	0.02	0	0		2.55
December	12	0	0	0	0	0.15	0	0	0	0	0	0	0	0	0.26	0.05	0	0	0.1	0	0	0	0	0.18	0.38	0	0	0	0.37	0	0	0	1.49
1949 Totals	**1949**	**0.44**	**0.45**	**1.07**	**1.33**	**1.87**	**0.21**	**0.67**	**0.53**	**2.62**	**4.81**	**4.69**	**2.37**	**0.73**	**2.5**	**0.91**	**0.59**	**0.79**	**2.19**	**1.73**	**4.19**	**5.43**	**0.24**	**0.93**	**0.34**	**0.71**	**1.35**	**1.32**	**0.14**	**0.17**	**0.44**	**0.09**	**45.85**
January	1	0	0	0.36	0.09	0	0	0	0	0.08	1.14	0.02	0	0	0	0.18	0.14	0	1.62	0	0	0	0	0.71	0.01	0.2	0.16	1	0	0	0	0.03	5.74
Feburary	2	0	0	0.28	0	0	0	0	0	0	0	0	0	0.14	1.81	0	0	0	0	0	0	0.1	0	0	0.21	0	0	0.11	0				2.65
March	3	0	0	0	0	0	0	0	0	0.38	0	0	0.1	0.22	0.09	0.01	0	0.48	0.03	0.01	0	0.28	0.02	0	0	0.08	0.35	0	0	0	0.44	0	2.49
April	4	0	0	0.1	0	0.03	0.04	0	0	0	0.07	0	0	0	0.37	0.07	0	0	0	0	0	0.28	0.2	0	0	0	0.44	0	0	0	0		1.6
May	5	0.01	0	0	0	0	0	0	0.16	2.09	0	0	0	0	0	0	0	0	0.05	0.98	0	1.79	0	0.22	0.07	0.03	0	0	0	0	0	0	5.4
June	6	0.43	0	0	0	0	0.06	0	0	0	1.36	1.56	0	0.37	0.16	0	0	0	0	0	0	0.55	0	0	0	0	0.15	0.21	0.06	0	0		4.91
July	7	0	0	0	0	0	0.04	0.64	0.37	0	0	0	0.11	0	0	0.34	0.45	0	0.14	0	3.7	0	0	0	0	0	0	0	0	0.17	0	0	5.96
August	8	0	0.21	0	0	0	0	0	0	0	1.95	0.04	0.01	0	0	0.17	0	0	0	0.03	0	0	0	0	0	0	0	0	0	0.08	0	0	2.49
September	9	0	0	0	0.56	0.01	0	0.03	0	0	0	0.06	2.1	0	0.07	0.13	0	0	0.34	0	0	0.01	0.01	0	0	0	0	0	0	0	0		3.32
October	10	0	0.24	0.11	0.68	1.83	0.07	0	0	0	0.03	1.81	0	0	0	0.01	0	0	0	0.71	0.41	0.76	0	0	0	0	0	0	0	0	0	0	6.66
November	11	0	0	0	0	0	0	0	0	0	0	0	0.05	0	0	0	0	0	0	0	0	0.01	0	0	0.05	0	0	0	0	0	0		0.11
December	12	0	0	0.22	0	0	0	0	0	0.07	0.26	1.2	0	0	0	0	0	0.31	0.01	0	0.08	1.65	0.01	0	0	0.4	0.25	0	0	0	0	0.06	4.52
1950 Totals	**1950**	**0.43**	**1.9**	**6.85**	**1.19**	**0.39**	**0.33**	**1.96**	**0.92**	**1.79**	**1.08**	**1.44**	**2.42**	**2.84**	**0.45**	**0.65**	**0.36**	**0.28**	**0.52**	**2.5**	**0.35**	**1.45**	**0.17**	**0.19**	**0.16**	**1.15**	**1.88**	**0.55**	**1.45**	**0.58**	**0.93**	**0.47**	**37.63**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0	0.39	4.16	0.75	0.12	0.09	0	0	0.11	0	0	0.14	0.95	0.06	0.14	0	0	0	0	0	0	0	0.04	0	0.97	0	0	0	0	0.08	0	8
Feburary	2	0	0	0	0	0	0	0	0.09	0	0	0.09	0.89	0.18	0.08	0.01	0	0	0.14	0	0	0.88	0.16	0	0	0	0	0	0.22				2.74
March	3	0	0	0	0	0	0	0	0	0	0.16	1.22	0.74	0	0	0.12	0.2	0	0	0.69	0.01	0	0	0	0	0	0.22	0	0	0	0	0.24	3.6
April	4	0	0.85	1.01	0.42	0	0	0	0	0.11	0.34	0	0	0	0	0	0	0	0.1	0.07	0	0.01	0	0.09	0.16	0.13	0	0	0.99	0.2	0		4.48
May	5	0.01	0	0	0	0	0	0	0.03	0.79	0.1	0.11	0	0	0.04	0	0.02	0	0	0.35	0	0.1	0	0	0	0	1.17	0	0	0.38	0.03	0	3.13
June	6	0	0.24	1.18	0	0	0	0	0	0.59	0.17	0	0.03	0.51	0.15	0.01	0	0.01	0.06	0.05	0.21	0	0	0	0	0	0	0	0.05	0	0		3.26
July	7	0	0	0.08	0	0	0	0	0	0	0	0	0	0.09	0	0	0.14	0.27	0.05	0.31	0	0	0	0	0	0.05	0.27	0	0	0	0	0	1.26
August	8	0.01	0	0	0	0.01	0	0	0.06	0	0	0	0.62	1.11	0.12	0.1	0	0	0.17	0	0	0	0	0	0	0	0	0.28	0.19	0	0.82	0.23	3.72
September	9	0.39	0.02	0	0	0	0	0	0.64	0.19	0.31	0	0	0	0	0	0	0	0	0	0.12	0.46	0	0	0	0	0.22	0.27	0	0	0		2.62
October	10	0	0.39	0.42	0	0	0	0.64	0.03	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.48
November	11	0	0	0	0	0	0	1.32	0.07	0	0	0	0	0	0	0.27	0	0	0	1.02	0.01	0	0.01	0.06	0	0	0	0	0	0	0		2.76
December	12	0.02	0.01	0	0.02	0.26	0.24	0	0	0	0	0.02	0	0	0	0	0	0	0	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0.58
1951 Totals	**1951**	**0.24**	**0.65**	**0.35**	**0.43**	**0.88**	**2.72**	**0.05**	**1.53**	**1.78**	**1.66**	**2.15**	**2.96**	**1.48**	**1.33**	**1**	**1.23**	**0.8**	**0.79**	**0.51**	**2.74**	**0.78**	**2.02**	**2.76**	**0.24**	**1.34**	**0.67**	**0.42**	**0.85**	**0.41**	**0.16**	**1.41**	**36.34**
January	1	0	0.2	0.02	0	0	0.04	0	0	0	0.28	0	0	0.19	0.47	0	0	0	0	0	0	0	0	0.04	0	0	0	0.03	0.1	0	0	0.27	1.64
Feburary	2	0.01	0	0	0.04	0.01	1.11	0	0.02	0	0	0	0	0.29	0.27	0.49	0.28	0	0.49	0	1.59	0	0	0	0	0	0.04	0	0.34				4.98
March	3	0	0.09	0.1	0	0	0	0	0	0	0.41	0.33	0.06	0.66	0.1	0	0	0.62	0	0	0.03	0	0	0	0	0	0	0.02	0.02	0.23	0.08	0	2.75
April	4	0	0	0	0	0.19	0.05	0	0.2	0	0.01	0.91	0.44	0	0	0	0	0	0.3	0	0	0.36	0	0	0	0	0	0	0	0	0	0		2.46
May	5	0.22	0.35	0.05	0	0	0.05	0	0	0	0.9	0	0	0	0	0	0	0	0	0.02	0.01	0.1	0.47	0	0	0	0.15	0	0	0	0	0.25	2.57
June	6	0	0.01	0.01	0.01	0	0	0.05	0.38	0	0	0.07	0.93	0.18	0	0	0.92	0	0	0.49	0.03	0.08	0.14	1.02	0	0.83	0.4	0.18	0.35	0	0.08		6.16
July	7	0	0	0	0	0.09	0	0	0	0.86	0	0.84	0.01	0	0	0	0	0	0	0	0	0	0.02	0.24	0	0	0	0	0	0	0	0.89	2.95
August	8	0	0	0.01	0	0	0.02	0	0.66	0.36	0	0	0	0	0	0.42	0	0	0	0	1.02	0	0	0	0	0	0.02	0.15	0.04	0.08	0	0	2.78
September	9	0.01	0	0	0.38	0.03	0	0	0	0.56	0.06	0	0.95	0	0	0	0	0	0	0	0	0.24	0.05	0.6	0.19	0.02	0.06	0	0	0	0		3.15
October	10	0	0	0	0	0.02	0.58	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.96	0.78	0	0	0	0.04	0	0.1	0	0	2.48
November	11	0	0	0	0	0.31	0.87	0	0	0	0	0	0.55	0.16	0	0.09	0.03	0	0	0	0	0	0.38	0.08	0	0.13	0	0	0	0	0		2.6
December	12	0	0	0.16	0	0.23	0	0	0.27	0	0	0	0.02	0	0.49	0	0	0.18	0	0	0.06	0	0	0	0.05	0.36	0	0	0	0	0	0	1.82
1952 Totals	**1952**	**1**	**1.28**	**2.44**	**2.23**	**0.64**	**0.25**	**0.05**	**0.87**	**0.72**	**1.57**	**0.86**	**1.24**	**0.89**	**0.62**	**0.31**	**2.3**	**1.01**	**0.71**	**0.87**	**0.49**	**0.79**	**1.05**	**0.22**	**0.77**	**0.8**	**0.56**	**0.1**	**0.04**	**0.12**	**0**	**0.87**	**25.67**
January	1	0	0.35	0.06	0.13	0	0	0	0	0	0	0	0	0	0.09	0	0.08	0	0	0	0	0.14	0	0	0	0	0.56	0	0	0	0	0	1.41
Feburary	2	0.79	0	1.02	0.04	0.2	0.02	0	0	0	0	0	0	0.21	0	0	0	0	0	0.01	0	0	0.18	0.01	0	0	0	0	0	0.02			2.5
March	3	0	0.14	0.11	0.04	0	0	0	0	0	1.16	0	0.01	0	0.01	0.06	0	0.29	0.3	0	0	0.04	0.49	0	0	0	0	0	0	0	0	0.87	3.52
April	4	0	0	0.08	1.38	0	0	0	0	0.29	0.1	0.06	1.23	0.14	0.07	0	0	0	0	0	0	0.15	0.18	0.17	0	0	0	0	0	0	0		3.85
May	5	0	0	0	0	0.01	0.15	0.02	0.06	0.3	0	0.01	0	0	0	0	0	0.08	0	0	0	0	0	0.04	0.25	0.15	0	0.1	0.01	0	0	0	1.18
June	6	0	0	0	0	0.31	0	0	0	0.09	0.31	0	0	0	0	0	0	0	0	0.06	0.13	0.01	0.08	0	0	0	0	0	0	0	0		0.99
July	7	0	0.79	0.36	0	0	0	0.03	0.45	0	0	0	0	0.54	0.11	0.06	2.22	0.01	0	0	0	0	0	0	0	0	0	0	0.03	0.01	0	0	4.61
August	8	0	0	0.61	0.56	0.12	0.08	0	0	0.01	0	0.79	0	0	0	0.19	0	0	0	0	0.32	0.45	0	0	0	0	0	0	0	0	0	0	3.13
September	9	0.08	0	0	0	0	0	0	0	0	0	0	0	0	0.07	0	0	0.38	0	0	0.03	0	0	0	0	0	0	0	0	0	0		0.56
October	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0.24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.24
November	11	0	0	0	0	0	0	0	0.36	0.03	0	0	0	0	0.02	0	0	0.25	0.41	0	0	0	0	0	0.5	0.64	0	0	0	0.09	0		2.3
December	12	0.13	0	0.2	0.08	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0	0.8	0.01	0	0.12	0	0.02	0.01	0	0	0	0	0	0	1.38
1953 Totals	**1953**	**0.71**	**0.54**	**1.48**	**1.91**	**0.76**	**0.28**	**0.55**	**0.45**	**0.01**	**0.63**	**0.8**	**0.4**	**0.67**	**0.28**	**0.01**	**1.32**	**0.72**	**0.23**	**0.34**	**1.36**	**0.79**	**0.12**	**2**	**0.22**	**0.48**	**1.77**	**0.51**	**0**	**0.12**	**0.72**	**0.41**	**20.59**
January	1	0	0.46	0	0	0	0.1	0.01	0.02	0	0	0	0	0	0	0	0.12	0.33	0	0	0.1	0	0	0.39	0	0	0	0	0	0	0	0	1.53
Feburary	2	0	0	0	0	0.02	0	0	0	0	0.63	0.28	0	0	0	0	0	0	0	0.11	0.34	0	0	0	0	0	0	0	0				1.38
March	3	0.68	0	1.31	0.01	0	0	0.07	0	0	0	0	0.2	0	0.28	0	0	0.11	0.18	0	0.02	0.19	0.04	0	0	0	0	0	0	0.09	0.47	0.41	4.06
April	4	0.01	0	0.02	0	0.24	0	0	0.37	0	0	0.52	0.03	0.05	0	0.01	0	0.24	0.04	0	0	0	0	1.52	0.22	0.02	0	0	0	0.03	0.11		3.43
May	5	0	0	0	0.19	0.22	0.04	0	0	0	0	0	0	0.15	0	0	1.05	0.03	0	0	0	0	0	0.09	0	0	0	0	0	0	0	0	1.77
June	6	0	0	0	0	0.04	0	0	0	0	0	0	0.08	0.47	0	0	0	0	0	0	0	0	0	0	0	0.46	0.99	0	0	0	0		2.04
July	7	0	0	0	0.12	0	0	0	0	0	0	0	0	0	0	0	0.11	0.01	0	0	0.8	0.13	0	0	0	0	0	0	0	0	0.14	0	1.31
August	8	0.02	0	0	0.18	0	0	0.47	0.06	0	0	0	0.09	0	0	0	0.04	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.86
September	9	0	0	0.1	0.21	0	0.08	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0		0.4
October	10	0	0	0	1.2	0.02	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.77	0.51	0	0	0	0	2.5
November	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0.23	0.1	0.43	0.06	0	0	0	0	0	0	0	0		0.83
December	12	0	0.08	0.05	0	0.22	0.06	0	0	0.01	0	0	0	0	0	0	0	0	0	0	0	0.04	0.02	0	0	0	0	0	0	0	0	0	0.48
1954 Totals	**1954**	**0.94**	**1.78**	**0.54**	**1.5**	**0.59**	**0.81**	**0.58**	**1.13**	**0.32**	**0.12**	**3.09**	**0.75**	**0.03**	**0.22**	**0.97**	**0.4**	**0.92**	**1.09**	**2.34**	**1.93**	**0.27**	**1.03**	**0.12**	**0.15**	**1.01**	**1.49**	**0.47**	**0.51**	**1.59**	**0.36**	**0.56**	**27.61**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0	0	0	0	0	0	0	0	0	0	0	0	0.03	0	0.03	0	0	0	0	0.51	0	0	0	0	0	0.63	0	0.03	0	0	0	1.23
Feburary	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.12	0.35	0	0	0.01	0.07	0	0	0.01	0	0.01	0	0.1	0				0.67
March	3	0	0.36	0	0	0	0	0	0	0	0	0	0.04	0	0	0	0	0	0.19	0.03	0	0	0	0	0.02	0.48	0	0	0.01	0.01	0	0	1.14
April	4	0	0	0	0.01	0	0.34	0	0	0	0.12	0.42	0	0	0.09	0.23	0	0	0	0	0	0	0.99	0	0	0.01	0.06	0.01	0	0	0.13			2.41
May	5	0	0.51	0	0	0	0.45	0.01	0	0	0	0	0	0	0	0	0.05	0.02	0.06	0.29	0	0.1	0.02	0	0	0.31	0.09	0.12	0	0	0.03	0.44		2.5
June	6	0.02	0.56	0.03	0	0	0	0.04	0.44	0.31	0	0	0	0	0	0.44	0	0.29	0	0	0	0	0.02	0	0	0	0	0	0	0.56	0			2.71
July	7	0	0	0.25	1.33	0	0	0.17	0	0	0	0	0	0	0	0.06	0	0	0	0	0	0.15	0	0	0	0	0	0	0	0	0	0.12		2.08
August	8	0.92	0.32	0.05	0	0.07	0	0.24	0.66	0	0	0.56	0.5	0	0	0.01	0	0.57	0.18	0.17	0	0	0	0.09	0	0	0	0	0.22	0	0	0	4.56
September	9	0	0	0	0	0	0	0.12	0	0	0	0	0	0	0	0	0	0	0	1.82	1.35	0	0	0	0	0	0	0	0	0	0			3.29
October	10	0	0.03	0	0	0.4	0.02	0	0	0	0	2.01	0.09	0	0.13	0.08	0	0	0	0	0	0	0	0	0.13	0.2	0.71	0	0.09	0	0.04	0	3.93
November	11	0	0	0.21	0.15	0	0	0	0	0	0	0	0	0	0	0	0	0	0.61	0.02	0	0.02	0	0.02	0	0	0	0	0	0	0.16			1.19
December	12	0	0	0	0.01	0.12	0	0	0.03	0.01	0	0.1	0.12	0	0	0	0	0.04	0.05	0	0	0	0	0	0	0	0	0.24	0.16	1.02	0	0	1.9
1955 Totals	**1955**	**0.79**	**0.57**	**0.44**	**3.12**	**2.58**	**0.68**	**1.36**	**0**	**0.06**	**2.08**	**1.72**	**0.8**	**0.67**	**0.89**	**0.18**	**0.04**	**0.16**	**0.26**	**1.75**	**1.32**	**1.13**	**2.03**	**2.54**	**0.73**	**1.78**	**1.6**	**0.24**	**1.51**	**0.24**	**0.06**	**0**	**31.33**
January	1	0	0	0.42	1.08	0.45	0.06	0	0	0	0	0	0.01	0	0.03	0	0	0	0.05	0.03	0	0	0	0	0	0	0	0	0.01	0	0	0	2.14
Feburary	2	0.23	0	0	0.09	0.2	0	0	0	0	0.08	0	0	0	0	0	0	0	0.13	1.47	0.22	0	0	0	0	0.01	1.02	0	0				3.45
March	3	0	0	0.02	0.41	0	0	0	0	0	0	0	0	0	0	0.07	0	0.07	0	0	0.89	0.36	0.05	0	0	0.28	0	0	0	0	0	0	2.15
April	4	0	0	0	0.44	0.1	0	0	0	0	0.32	0.48	0.32	0.5	0	0	0	0	0	0	0.13	0	0.6	0.53	0.15	0	0	0	0	0	0		3.57
May	5	0	0	0	0	0	0	0.05	0	0.03	0.44	0.05	0.23	0.09	0	0	0	0	0	0	0	0.33	0.05	0	0	0	0.58	0	0.52	0.08	0	0	2.45
June	6	0	0	0	0.8	0.1	0.33	0.01	0	0.01	0.36	1.16	0.01	0	0	0	0	0	0	0	0	0	0.01	0	0.5	1.49	0	0	0	0	0			4.78
July	7	0	0	0	0.04	1.11	0.02	0	0	0	0	0	0	0.08	0.62	0	0	0.06	0	0.25	0	0.02	0	0.69	0.08	0	0	0	0	0	0	0	2.97
August	8	0	0.3	0	0	0	0	1.3	0	0.02	0.49	0	0	0	0	0	0	0	0	0	0	0	0.06	0	0	0	0	0	0	0.16	0	0	2.33
September	9	0	0	0	0	0	0	0	0	0	0.39	0	0	0	0	0	0	0	0	0	0.08	0.42	0.99	1.07	0	0	0	0.24	0	0	0		3.19
October	10	0	0	0	0.26	0.62	0.27	0	0	0	0	0.03	0.23	0	0	0	0	0.03	0	0	0	0	0	0.25	0	0	0	0	0.98	0	0.06	0	2.73
November	11	0.53	0.27	0	0	0	0	0	0	0	0	0	0	0	0.24	0.11	0.04	0	0.08	0	0	0	0.27	0	0	0	0	0	0	0	0		1.54
December	12	0.03	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.03
1956 Totals	**1956**	**0.69**	**0.13**	**1.19**	**0.19**	**1.82**	**1.85**	**0.82**	**1.74**	**1.36**	**0.81**	**0.19**	**0.1**	**0.23**	**1.32**	**2.55**	**0.98**	**0.23**	**1.07**	**2.87**	**2.33**	**0.05**	**0.3**	**0.81**	**0.78**	**1.79**	**1.45**	**0.25**	**0.96**	**3.97**	**1.42**	**0.18**	**34.43**
January	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.1	0.07	0	0	0	0	0	0.07	0	0	0	0.44	0.05	0	0.73
Feburary	2	0.55	0	0	0	0.2	0	0	0.15	0.02	0.33	0.19	0	0	0.94	0	0.13	0.22	0	0	0	0	0	0	0.33	0.51	0	0.12	0	0				3.69
March	3	0	0	0	0	0	0	0.02	0	0	0	0	0	0.16	0.33	0.26	0.06	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.84
April	4	0	0.12	0	0	0	0.02	0	0	0.48	0.45	0	0	0	0.05	0	0.06	0	0	0	0	0	0.02	0.03	0	0.57	0	0	0.68	0.37	0		2.85
May	5	0	0	0	0	0	0.05	0.59	0	0	0	0	0	0	0	0.92	0	0	0.09	0.39	0	0	0	0.32	0	0	0.67	0.13	0.15	0.24	1.23	0.06	4.84
June	6	0	0	0	0	0	0	0.17	0	0	0	0	0.03	0	0	0.01	0.02	0	0	1.47	0.14	0	0	0	0.45	0	0.78	0	0	0	0			3.07
July	7	0	0.01	1.17	0.19	0	0	0	0.36	0	0	0	0.07	0.06	0	0.07	0.7	0	0.88	0.46	0	0	0	0.19	0	0	0	0	0.13	2.74	0	0	7.03
August	8	0.09	0	0	0	0	0	0	0	0.86	0	0	0	0.01	0	0	0	0	0	0.16	0	0	0	0	0	0	0	0	0	0.15	0.14	0.12	1.53
September	9	0.05	0	0	0	0	0	0	0	0	0	0	0	0	0	0.83	0.01	0	0	0.01	0	0	0.16	0.15	0	0	0	0	0	0	0		1.21
October	10	0	0	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.12	0.05	0	0	0	0.47	0	0	0	0	0	0	0	0.65
November	11	0	0	0.01	0	1.62	0.19	0	0	0	0	0	0	0	0	0.4	0	0	0	0.16	1.64	0	0	0	0	0.17	0	0	0	0	0			4.19
December	12	0	0	0	0	0	1.59	0.04	1.23	0	0.03	0	0	0	0	0.06	0	0	0	0.15	0.43	0	0.12	0.12	0	0	0	0	0	0.03	0	0	3.8
1957 Totals	**1957**	**0.16**	**0.64**	**1.62**	**0.46**	**0.43**	**0.42**	**1.01**	**1.87**	**0.69**	**0.2**	**0.26**	**1.08**	**0.54**	**4.43**	**1.45**	**0.91**	**1.72**	**1.81**	**1.24**	**0.56**	**3.42**	**2.82**	**1.69**	**2.1**	**2.35**	**4**	**1.96**	**4.03**	**2.08**	**0.52**	**0.69**	**47.16**
January	1	0	0	0	0	0	0.02	0	0	0.13	0	0	0	0	0	0	0	0	0	0	0.02	0	0.5	0	0.03	0	0.01	0	0.03	0.08	0.07	0.08	0.97
Feburary	2	0	0	0.03	0	0.33	0	0.05	0.24	0.22	0	0	0	0	0	0.02	0	0	0.05	0	0	0	0.02	0.13	0	0.55	2.1	0	0				3.74
March	3	0	0	0	0	0	0	0.01	0	0.02	0	0.19	0	0	0.01	0	0	0	0.14	0	0	0.32	0	0.21	1.6	0.11	0.23	0	0	0.02	0	0.01	2.87
April	4	0.07	0	1.21	0.27	0.1	0	0.43	0.61	0	0	0.07	0.01	0	0	0	0	0.34	0.25	0.14	0.45	0.45	0.62	0	0.1	1.08	1.02	0.8	0.16	0	0		8.18
May	5	0	0	0	0	0	0	0	0	0.26	0.06	0	0.08	0.2	0	0	0.02	0.98	0.13	0.54	0	2	1.3	0.15	0	0.35	0	0	0	0	0.3	0.33	6.7
June	6	0	0	0	0.19	0	0	0.09	1	0	0.14	0	0.78	0.2	3.95	0.8	0	0	0	0	0	0	0	0.05	0.12	0	0.64	0.82	1.65	0.05	0		10.48
July	7	0	0	0	0	0	0	0	0	0.06	0	0	0	0	0.09	0.25	0	0	0	0	0	0	0	0.02	0	0	0	0.13	2.18	1.92	0	0	4.65
August	8	0	0	0.36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.25	0	0	0	0	0	0	0	0.61
September	9	0	0	0	0	0	0.12	0	0	0	0	0	0	0	0	0.04	0	0	0	0.07	0	0.65	0	0	0	0	0	0	0	0	0		0.88
October	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0.08	0.34	0.41	0	0	0	0	0	0.38	1.13	0	0	0	0	0	0	0	0	2.34
November	11	0.09	0.64	0	0	0	0	0.27	0.02	0	0	0	0.21	0.14	0.3	0	0	0.25	1.01	0	0	0	0	0	0	0	0	0	0.01	0.01	0.01	0		2.96
December	12	0	0	0.02	0	0	0.28	0.16	0	0	0	0	0	0	0	0	0.48	0.15	0.23	0.49	0.09	0	0	0	0	0.26	0	0.2	0	0	0.15	0.27	2.78
1958 Totals	**1958**	**0.62**	**0.43**	**1.43**	**0.16**	**1**	**0.11**	**1.68**	**1.14**	**2.39**	**1.66**	**1.6**	**0.91**	**0.39**	**1.75**	**1.99**	**2.44**	**1.16**	**0.19**	**3.32**	**0.5**	**1.48**	**0.81**	**1.37**	**1.04**	**1.63**	**0.39**	**2.59**	**0.44**	**0.08**	**0.66**	**2.02**	**37.38**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.74	0.01	0	0	0	0.02	0	0	0	0	0.86	2.13
Feburary	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0.05	0	0	0	0	0	0	0	0	0	0	0	0.04	0.38	0				0.47
March	3	0	0	0	0	0.1	0	0.22	0.84	0.94	0.13	0	0	0	0	0	0.01	0.04	0	0	0	0	0	0.73	0.84	0	0	0	0	0.02	0	0	3.87
April	4	0	0	0.18	0	0.72	0.02	0	0	0	0	0	0	0	0.28	0	0	0	0	0.16	0	0.32	0.25	0.64	0	0	0.03	0.09	0.12	0	0		2.81
May	5	0	0.3	1.25	0.07	0.13	0	0	0.16	0	0	0	0	0	0	0	0	0	0	0	0	0	0.46	0	0.09	0	0	0.22	0	0	0	0.05	2.73
June	6	0.21	0	0	0	0	0	0	0	0	1.53	0	0.61	0.39	0.66	0.76	0	0	0	0	0	0.08	0.09	0	0.11	0.87	0	0	0	0	0		5.31
July	7	0	0	0	0.02	0.05	0	0.15	0	0	0	0.04	0	0	0.04	0.36	0.05	0.6	0.19	3.16	0	0	0	0	0	0.02	0	1.82	0.06	0	0.43	0.82	7.81
August	8	0.21	0	0	0	0	0	0.29	0	0	0	1.56	0.3	0	0	0.37	0.5	0	0	0	0	0.09	0	0	0	0	0	0	0	0	0	0	3.32
September	9	0.12	0.1	0	0	0	0.09	0	0	0	0	0	0	0	0	0.34	0.82	0	0	0	0	0.1	0	0	0	0	0.3	0	0	0.06	0.23		2.16
October	10	0	0	0	0	0	0	1.02	0	1.45	0	0	0	0	0	0.11	0	0	0	0	0	0.15	0	0	0	0	0	0	0	0	0	0.04	2.77
November	11	0.08	0.03	0	0	0	0	0	0.14	0	0	0	0	0	0.72	0.05	1.06	0.52	0	0	0	0	0	0	0	0.74	0	0.08	0.26	0	0		3.68
December	12	0	0	0	0.07	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.25	0.32
1959 Totals	**1959**	**0.77**	**0.22**	**1.56**	**1.96**	**2.67**	**0.1**	**0**	**0.43**	**3.04**	**1.83**	**0.9**	**0.11**	**1.1**	**0.34**	**0.01**	**0.44**	**2.2**	**1.13**	**0.42**	**0.7**	**0.94**	**1.1**	**0.81**	**0.02**	**0.56**	**1.88**	**1.18**	**1.37**	**0.2**	**0.29**	**0.03**	**28.31**
January	1	0	0	0.07	0	0	0	0	0	0	0	0	0	0	0.03	0	0	0	0	0	0.7	0.53	0	0	0	0	0	0.09	0	0	0	0	1.42
Feburary	2	0	0	0.29	0	0	0	0	0	2.36	0.2	0	0	0.01	0.02	0	0	0	0	0	0	0	0.49	0	0	0	0	0	0.02				3.39
March	3	0	0	0	0	0.57	0.01	0	0.33	0.2	0	0.05	0.01	0	0.28	0.01	0	0	0	0	0	0	0	0	0	0.03	0.65	0	0	0.04	0.22	0	2.4
April	4	0.24	0	0	0	0	0	0	0.1	0	0	0	0	0	0	0	0	0.13	0	0.42	0	0	0	0	0	0	0	0.4	0.02	0	0.06		1.37
May	5	0	0	0.02	0.06	0	0	0	0	0.41	0.16	0.69	0	0	0.01	0	0	0.8	0.31	0	0	0.32	0.18	0	0	0.36	0.07	0.14	0	0	0	0.03	3.56
June	6	0.01	0	0	0	0	0	0	0	0.07	0.02	0	0	0	0	0	0	0	0	0	0	0	0.37	0	0	0	0	0	0	0	0		0.47
July	7	0	0	0	0.04	0.26	0	0	0	0	0	0	0	0	0	0	0	0	0.82	0	0	0	0.03	0.57	0	0	0.36	0	0	0	0	0	2.08
August	8	0	0	0	0.65	0.27	0.03	0	0	0	0	0	0	0	0	0	0.42	0.25	0	0	0	0.09	0.03	0	0	0	0.03	0.21	0	0.15	0	0	2.13
September	9	0.52	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.08	0	0.17	0.61	0.2	1.27	0	0		2.85
October	10	0	0.22	0.26	0.26	1.54	0.06	0	0	0	1.16	0	0	0.15	0	0	0	0	0	0	0	0	0	0	0.13	0	0	0.02	0	0	0	0.01	0	3.81
November	11	0	0	0.92	0.91	0	0	0	0	0	0	0	0.1	0.94	0	0	0	0	0	0	0	0	0	0	0.01	0.02	0	0	0	0	0		2.9
December	12	0	0	0	0.04	0.03	0	0	0	0	0.29	0.16	0	0	0	0	0.02	1.02	0	0	0	0	0	0	0.02	0	0	0.14	0.14	0.06	0.01	0	0	1.93
1960 Totals	**1960**	**0.89**	**0.61**	**0.66**	**1.22**	**1.8**	**0.93**	**0**	**0.8**	**0.37**	**1**	**0.73**	**1.49**	**0.22**	**1.13**	**1.69**	**1.55**	**0.67**	**0.79**	**0.71**	**1.18**	**0.04**	**0.63**	**0.23**	**1.59**	**1.44**	**0.24**	**0.45**	**1.87**	**3.87**	**2.95**	**0.03**	**31.78**
January	1	0	0	0	0	0	0	0	0	0	0	0.05	0.19	0	0.36	0.04	0	0.24	0.01	0	0	0	0	0	0	0	0.07	0.02	0.11	0.02	0	0	1.11
Feburary	2	0	0	0	0.18	0.34	0	0	0.01	0	0.06	0	0	0	0	0	0	0	0	0	0.02	0.04	0	0.13	0.02	0.28	0	0.04	0.07	0			1.19
March	3	0	0.55	0.11	0	0	0.02	0	0.21	0.18	0.01	0.1	0	0	0	0.4	0.04	0	0	0.07	0	0	0	0	0	0	0	0	0	0.57	0.51	0	2.77
April	4	0.06	0	0	0.04	0	0	0	0	0	0	0	0	0	0.02	0.17	0.4	0.43	0	0	0.82	0	0	0	0	0.13	0	0	0.09	0.78	0.17		3.11
May	5	0	0	0	0.05	0.41	0.62	0	0	0	0.01	0.02	0	0	0	0	0.71	0	0.15	0.17	0.08	0	0	0	1.19	0.55	0	0.07	0	0.69	0	0	4.72
June	6	0.06	0	0	0	0	0	0	0	0	0	0.02	1.08	0.18	0.7	0	0.22	0	0	0	0	0	0	0.07	0.02	0	0	0	0.32	1.48	1.81	2.01		7.97
July	7	0.77	0.01	0.01	0	0	0	0	0	0.12	0.74	0	0.22	0.04	0	0	0	0	0	0	0	0	0	0	0	0.36	0	0	0	0	0	0	2.27
August	8	0	0	0	0	0	0.07	0	0.07	0	0	0	0	0	0.05	0	0	0	0.37	0.15	0.05	0	0.2	0	0	0	0	0	0.02	0	0	0	0.98
September	9	0	0	0	0	0	0	0	0.07	0	0	0	0	0	0	0.03	0.18	0	0	0	0	0	0	0.01	0.38	0.09	0	0	0	0	0		0.76
October	10	0	0	0.54	0.95	0.15	0	0	0.19	0	0	0	0	0	0	0.46	0	0	0.26	0.32	0	0	0	0	0	0.03	0.17	0	0	0	0.26	0.03	3.36
November	11	0	0.05	0	0	0	0	0	0.25	0.07	0	0	0	0	0	0.58	0	0	0	0	0	0	0.36	0	0	0	0	0	0.1	0	0		1.41
December	12	0	0	0	0	0.9	0.22	0	0	0	0.18	0.54	0	0	0	0.01	0	0	0	0	0	0.21	0	0	0.07	0	0	0	0	0	0	0	2.13
1961 Totals	**1961**	**0.01**	**2.52**	**0.29**	**0.71**	**2.63**	**1.4**	**2.82**	**2.8**	**1.23**	**0.65**	**1.03**	**3.34**	**2.22**	**0.33**	**0.73**	**0.5**	**1.19**	**1.12**	**1.54**	**0.88**	**0.8**	**1.18**	**1.29**	**1.97**	**3.81**	**0.18**	**0.33**	**0.64**	**0**	**2.79**	**0.27**	**41.2**
January	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0.04	0.04	0.01	0	0	0.03	0.13	0	0	0	0	0	0.14	0	0	0	0	0	0.39
Feburary	2	0	0.55	0	0	0	0.09	0.24	0	0	0	0	0	0	0	0	0	0.44	0.33	0	0	0	0.15	0	0.02	0	0	0.14	0.1				2.06
March	3	0	0	0	0.12	0.74	0.67	0.31	0.01	0	0	0	1.42	0.02	0	0	0	0	0.52	0	0.69	0.01	0.02	0	0	0	0	0.1	0	0	0	0.12	4.75
April	4	0	0.12	0.11	0	0	0	0	0.24	0.76	0	0.13	0.52	0	0	0.08	0	0	0	0	0	0.31	0.25	0.01	0.13	0.7	0	0.08	0.03	0	0		3.47
May	5	0	0	0	0.02	1.24	0.26	2.26	2.3	0	0	0	0	0	0.18	0	0	0.75	0	0	0	0	0	0	0	0.24	0	0	0	0	0	0	7.25
June	6	0	0.07	0	0	0.14	0.38	0.01	0.04	0.01	0	0	0	0.46	0	0.31	0	0	0	0	0	0.01	0	0	0	0	0	0	0	0	0	2.24		3.67
July	7	0	0.26	0	0	0	0	0	0	0	0	0	1.28	0.12	0.11	0	0	0	0	1.01	0.04	0.28	0.5	0	0.1	2.5	0	0	0	0	0	0	6.2
August	8	0.01	0.11	0	0.01	0.45	0	0	0	0.24	0.65	0.31	0	0	0	0	0	0	0	0.05	0.01	0	0.04	0	0	0	0	0	0	0	0	0	1.88
September	9	0	0	0	0.12	0.06	0	0	0	0	0	0.22	0.12	1.4	0	0	0	0	0	0	0	0	0	0	1.56	0.37	0	0	0	0	0.16		4.01
October	10	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0	0	0.18	0	0	0	1.27	0.16	0	0	0	0.51	0	0.39	0.15	2.67
November	11	0	1.41	0.18	0	0	0	0	0	0	0	0	0	0.21	0	0.3	0	0	0.22	0.14	0	0.2	0.22	0.01	0	0	0	0.01	0	0	0		2.9
December	12	0	0	0	0.44	0	0	0	0.21	0.22	0	0.37	0	0	0	0	0.49	0	0.05	0.13	0	0	0	0	0	0	0.04	0	0	0	0	0	1.95
1962 Totals	**1962**	**1.88**	**0.14**	**1.6**	**2.03**	**2.34**	**1.72**	**1.31**	**2.26**	**0.98**	**0.71**	**2.25**	**0.42**	**0.09**	**1.96**	**0.36**	**0.85**	**0.14**	**0.55**	**0.39**	**4.09**	**0.33**	**0.36**	**0.34**	**2.76**	**0.77**	**0.56**	**0.23**	**0.54**	**0.22**	**2.27**	**0.18**	**34.63**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0	0	0	0.01	0.5	0.63	0.14	0.02	0	0	0	0	0	1.14	0.14	0	0	0.14	0.14	0	0.1	0	0	0	0.04	0.56	0	0	0	0	0	3.56
Feburary	2	0	0	0	0	0	0	0	0.34	0.81	0	0	0	0	0	0.2	0	0.02	0.29	0	0.07	0.13	0	0.34	0.01	0.18	0	0.14	0				2.53
March	3	0	0	0	0	0.02	0	0	0.45	0	0.02	0.15	0.01	0	0	0	0	0	0	0.05	1.76	0.09	0	0	0	0.17	0	0	0	0.12	0	0.16	3
April	4	0.09	0.05	0	0.01	0.3	0	0	0.32	0	0.08	0.03	0	0	0.16	0	0.15	0	0	0	0	0	0.14	0	0	0	0	0	0.06	0	1.15		2.54
May	5	0.86	0	0.01	0	0	0.02	0	0.06	0	0.55	0.23	0	0	0	0	0	0.1	0	0	0	0	0	0	0	0.34	0	0.07	0	0	0.2	0	2.44
June	6	0	0	0.02	0.02	0	0	0.86	0.4	0.13	0	1.79	0	0	0	0	0	0	0.1	0	0.01	0	0.22	0	1.2	0	0	0	0	0	0		4.75
July	7	0	0	1.38	1.24	1.51	0.9	0.3	0.07	0	0	0	0	0.09	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5.49
August	8	0	0	0.02	0.66	0	0	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0.32	0	0	0	1.26	0	0	0	0	0	0	0.02	2.29
September	9	0	0	0.16	0.05	0	0	0	0.6	0.04	0	0	0	0	0.66	0.02	0	0	0	0	0	0	0	0	0.16	0	0	0.02	0	0	0.92		2.63
October	10	0.93	0	0	0	0	0.14	0	0	0	0	0	0.41	0	0	0	0.22	0	0	0	0.57	0	0	0	0.13	0	0	0	0.3	0	0	0	2.7
November	11	0	0.09	0.01	0.01	0	0.03	0	0	0	0	0.05	0	0	0	0	0.48	0.02	0.02	0	0	0	0	0	0	0	0	0	0	0	0		0.71
December	12	0	0	0	0.03	0.01	0	0	0	0	0.06	0	0	0	0	0	0	0	0	0.2	1.36	0.01	0	0	0	0.04	0	0	0.18	0.1	0	0	1.99
1963 Totals	**1963**	**0.01**	**0.09**	**0.2**	**1.48**	**0.95**	**0.13**	**0.24**	**0.35**	**0.46**	**1.24**	**1.3**	**2.35**	**1.86**	**0**	**1.77**	**2.33**	**2**	**1.22**	**2.38**	**0.26**	**0.32**	**2.37**	**0.03**	**0.12**	**0.98**	**0.14**	**0.64**	**0.91**	**0.84**	**0.63**	**1.02**	**28.62**
January	1	0.01	0.03	0	0	0.33	0	0	0	0	0	0.03	0	0	0	0	0	0	0	0.16	0	0	0.09	0	0	0	0.09	0	0	0	0	0	0.74
Feburary	2	0	0	0	0	0	0	0	0	0	0.16	0	0	0	0	0	0	0	0	0	0.05	0	0	0.03	0.01	0	0	0	0				0.25
March	3	0	0	0.04	1.44	0.22	0.02	0	0.34	0.24	0	0.18	0	0	0	0.02	0.68	0	0.22	0	0	0	0	0	0	0.9	0.04	0	0	0.03	0.63	0.54	5.54
April	4	0	0	0.05	0	0	0	0	0	0	0.2	0	0	0	0	0	0.06	0	0	0.17	0	0	0	0	0	0	0	0.17	0.53	0.8	0		1.98
May	5	0	0	0	0.01	0.03	0	0	0	0	0	0	1.46	0	0	0.74	1.52	0.01	0	0.36	0	0	0	0	0	0.08	0.01	0.46	0.09	0	0	0	4.77
June	6	0	0	0	0	0	0	0	0	0	0.84	0	0	1.36	0	0.52	0.07	0	0	0.96	0.12	0	0	0	0	0	0	0	0	0	0		3.87
July	7	0	0.06	0	0	0.02	0.11	0	0	0	0	0	0	0.5	0	0	0	0.38	0	0	0	0	0	0	0	0	0	0.01	0.29	0	0	0	1.37
August	8	0	0	0	0	0	0	0	0	0.22	0	0	0.72	0	0	0	0	0	0.76	0.73	0	0	0	0	0.11	0	0	0	0	0.01	0	0	2.55
September	9	0	0	0	0	0.34	0	0	0	0	0	0.79	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		1.13
October	10	0	0	0	0	0	0	0	0	0	0	0	0.17	0	0	0.49	0	1.48	0.23	0	0	0	0	0	0	0	0	0	0	0	0	0.48	2.85
November	11	0	0	0.11	0.03	0.01	0	0	0	0	0	0	0	0	0	0	0	0.06	0	0	0.09	0.32	2.28	0	0	0	0	0	0	0	0		2.9
December	12	0	0	0	0	0	0	0.24	0.01	0	0.04	0.3	0	0	0	0	0	0.07	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0	0.67
1964 Totals	**1964**	**0.21**	**0.84**	**0.45**	**1.46**	**2.66**	**0.21**	**0.01**	**0.92**	**1.55**	**0.21**	**3.16**	**1.58**	**0.23**	**0.73**	**0.84**	**0.87**	**0.38**	**0.7**	**1.16**	**0.53**	**3.03**	**0.3**	**0.21**	**1.25**	**1.21**	**2.12**	**2.85**	**1.34**	**0.54**	**0.23**	**0.38**	**32.16**
January	1	0	0	0	0	0	0	0	0	0.11	0	0.13	0.53	0.04	0	0	0	0	0	0.08	0	0	0	0	0.45	0	0	0	0	0	0.04	0.32	1.7
Feburary	2	0	0	0	0	0.38	0.17	0	0	0.04	0.1	0	0.68	0	0	0.55	0	0	0.24	0.11	0	0	0	0	0	0.03	0	0	0	0			2.3
March	3	0	0	0	0.35	0.07	0	0.01	0.86	1.33	0.04	0.01	0	0	0.13	0	0	0	0	0.47	0.22	0	0	0	0.02	0.32	0	0	0.01	0	0	0	3.84
April	4	0	0.6	0.37	0.34	1.14	0	0	0	0	0	0	0.03	0.11	0	0	0	0	0.22	0.01	0.31	0.6	0	0.21	0.69	0	0	0.34	0.01	0.01	0		4.99
May	5	0	0	0	0	0	0.04	0	0	0	0	0.22	0	0.04	0	0	0	0	0	0	0	0	0	0	0.07	0	0.75	0.31	1.25	0	0	0	2.68
June	6	0	0	0	0.56	0.81	0	0	0	0	0	0.05	0.12	0.04	0.6	0.02	0	0.04	0	0	0	0	0	0	0	0	0	0	0	0.32	0.17		2.73
July	7	0.21	0	0.01	0	0.26	0	0	0.06	0.07	0	2.6	0.21	0	0	0	0	0	0	0	0	0.57	0.26	0	0	0	0	0	0	0	0	0	4.25
August	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.72	0.04	0	0	0.55	0	0.04	0.04	0	0	0	2.39
September	9	0	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0	0	0.33	0.02	0	0	0.14	0	0	0	0	0.95	0.02	0	0	0		1.47
October	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.39	0.34	0	0	0	0	0.73
November	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.27	0.87	0.01	0.22	0.49	0	0	0	0	0	0	1.8	0.03	0.15	0		3.84
December	12	0	0.24	0.07	0.21	0	0	0	0	0	0.07	0.14	0.01	0	0	0	0	0	0	0	0	0	0	0	0.02	0.34	0	0	0	0.06	0.02	0.06	1.24
1965 Totals	**1965**	**1.29**	**0.71**	**0.74**	**1.18**	**1.27**	**1.22**	**2.04**	**1.28**	**1.33**	**0.31**	**1.05**	**0.51**	**0**	**0.69**	**0.66**	**0.43**	**0.31**	**0.17**	**0.44**	**0.75**	**0.92**	**1.49**	**1.17**	**1.74**	**0.93**	**1.54**	**0.95**	**0.08**	**0.57**	**0.5**	**1.99**	**28.26**
January	1	0.06	0.3	0	0	0	0	0	0.74	0	0	0	0	0	0	0.42	0	0	0	0	0	0	0.4	0.3	0	0.05	0.01	0	0.08	0.15	0	0	2.51
Feburary	2	0.04	0	0	0	0	0	0	0.01	0.66	0	0.12	0	0	0	0	0	0	0	0	0	0.1	0	0.01	0.22	0	0	0	0				1.16
March	3	0.6	0.35	0.18	0.26	0.02	0	0.08	0	0	0	0	0	0	0.05	0	0	0.31	0	0	0	0	0.02	0.24	0.09	0.14	0	0	0	0	0	0	2.34
April	4	0	0	0.54	0.06	1.18	0	0	0	0	0.2	0	0	0	0.49	0.08	0	0	0	0	0	0	0	0	0.36	0.64	0.01	0.11	0	0	0		3.67
May	5	0	0	0	0	0	0.19	0	0	0.06	0	0	0	0	0	0	0	0	0.15	0	0	0	0	0.31	0.03	0	0.64	0	0	0	0	0	1.38
June	6	0.27	0	0.02	0	0	0.37	0	0.53	0	0	0	0	0	0	0	0	0	0	0	0.72	0.04	0.28	0.31	0	0	0	0	0	0.42	0.07		3.03
July	7	0	0.04	0	0.04	0	0	1.32	0	0.53	0	0	0	0	0	0	0	0	0	0.43	0.03	0	0	0	0	0	0	0.78	0	0	0	0	3.17
August	8	0.32	0	0	0	0	0.48	0.64	0	0	0	0	0	0	0	0.01	0	0.02	0	0	0	0.03	0	0	0.14	0.1	0.69	0.06	0	0	0.38	0.72	3.59
September	9	0	0	0	0.82	0	0	0	0	0	0	0.22	0	0	0.02	0.08	0.41	0	0	0	0	0.62	0.78	0	0	0	0	0	0	0	0.05		3
October	10	0	0	0	0	0	0.18	0	0	0	0	0	0	0	0.06	0.07	0	0	0	0.01	0	0.13	0.01	0	0	0	0	0	0	0	0	0	0.46
November	11	0	0	0	0	0.07	0	0	0	0	0	0	0.43	0	0	0	0	0	0	0	0	0	0	0	0.09	0	0.19	0	0	0	0		0.78
December	12	0	0.02	0	0	0	0	0	0	0.08	0.11	0.71	0.08	0	0.07	0.01	0.01	0	0	0	0	0	0	0	0.81	0	0	0	0	0	0	1.27	3.17
1966 Totals	**1966**	**1.96**	**0**	**0.5**	**0.8**	**0.64**	**0.47**	**0.97**	**1.79**	**3.89**	**1.62**	**1.87**	**1.71**	**0.42**	**1.67**	**1.48**	**0.23**	**2.24**	**1.11**	**0.89**	**1.98**	**0.29**	**0.14**	**1.66**	**0.21**	**0.47**	**0.6**	**0.69**	**1.36**	**0.18**	**0.31**	**0.19**	**32.34**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0.24	0	0	0	0	0	0	0	0	0	0	0.17	0	0	0	0	0	0	0	0	0	0.06	0	0	0	0	0	0	0	0	0.18	0.65
Feburary	2	0.65	0	0	0	0	0	0	0	2.28	0.41	0	0	0	0.05	0	0	0	0	0	0	0.01	0	0	0	0	0	0.03	0.69				4.12
March	3	0	0	0.5	0	0.06	0	0	0	0	0	0.05	0.39	0	0	0	0	0	0.09	0	0	0	0	0	0	0	0	0	0	0	0	0	1.09
April	4	0.01	0	0	0	0	0	0	0.23	0	0	0.82	0.51	0.02	0	0.06	0	0.14	0.35	0.36	1.84	0	0	1.1	0.18	0	0.13	0.07	0.2	0	0.01		6.03
May	5	0.02	0	0	0	0	0	0	0.37	0	0.02	0.98	0.01	0.17	0	0.21	0	2.03	0	0	0	0.22	0	0.56	0	0	0	0	0	0	0	0	4.59
June	6	0	0	0	0	0	0.47	0	0.36	0	0	0	0.35	0	0	0.2	0.21	0	0	0	0	0	0	0	0	0	0	0	0	0	0		1.59
July	7	0.15	0	0	0	0	0	0	0	0.12	0	0	0	0	0	0.04	0	0	0.02	0.26	0	0	0	0	0	0.16	0	0	0.34	0.17	0	0	1.26
August	8	0.89	0	0	0	0	0	0	0	0	1.19	0	0	0.05	0.46	0.97	0.02	0	0	0	0	0.06	0.08	0	0	0	0	0	0	0	0	0	3.72
September	9	0	0	0	0	0.09	0	0	0	0	0	0.02	0.28	0	0.4	0	0	0	0.31	0.22	0.14	0	0	0	0	0.13	0	0.25	0	0.01	0.3		2.15
October	10	0	0	0	0	0	0	0	0.32	0.46	0	0	0	0.18	0.76	0	0	0.07	0.34	0.05	0	0	0	0	0	0	0	0	0	0	0	0	2.18
November	11	0	0	0	0.25	0.27	0	0	0.02	1.03	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.03	0.18	0.47	0.22	0	0	0		2.47
December	12	0	0	0	0.55	0.22	0	0.97	0.49	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.12	0.13	0	0	0.01	2.49
1967 Totals	**1967**	**0.87**	**2.14**	**0.93**	**0.29**	**1.42**	**2.03**	**0.19**	**0.37**	**1.77**	**1.42**	**0.73**	**1.79**	**1.77**	**0.68**	**1.2**	**2.63**	**0.82**	**1.29**	**0.53**	**1.56**	**4.31**	**0.08**	**0.38**	**2.47**	**0.54**	**2.98**	**2.24**	**0.55**	**1.47**	**1.04**	**0.81**	**41.3**
January	1	0	0	0	0	0	0.34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.37	0.03	2.13	0.02	0	0	0	0	2.89
Feburary	2	0.81	0.26	0	0	0.01	0	0	0	0	0	0	0	0	0	0	0.01	0.01	0	0	0	0	0.02	0.01	0	0	0.03	0.56	0				1.72
March	3	0	0	0	0.29	1.06	0	0	0.07	0	0	0	0.31	0	0	0	0	0	0	0.27	0.76	0	0	0	0	0	0.01	0	0	0	0	0	2.77
April	4	0	0	0.62	0	0	0	0	0.07	0.38	0	0	0.14	0.23	0	0	0.21	0.1	0	0	0	0.42	0	0.28	0	0.41	0.02	0	0	0.52	0		3.4
May	5	0	0	0	0	0.02	1.3	0.08	0	0	0	0	0	1.35	0.46	0.02	0.17	0	0	0.05	0	0	0	0	0	0	0	0	0.27	0.2	0.36	0.45	4.73
June	6	0.06	0	0	0	0	0.38	0.01	0	0	0.45	0	1.32	0	0	0	0.28	0	0	0	0	1.22	0	0	0.08	0	0	0.63	0.01	0.02	0		4.46
July	7	0	0.01	0	0	0	0	0	0	1.03	0.12	0	0.02	0	0	0	0	0	0	0.12	0	0	0	0.09	1.48	0	0	0.48	0.27	0	0	0.22	3.84
August	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.27	0.09	0	0	0	0	0	0	0	0	0	0	0	0	1.36
September	9	0	0	0	0	0	0	0	0.04	0	0	0	0	0	0	0.31	1.19	0.16	0.02	0	0.73	0.83	0	0	0	0	0.7	0.35	0	0	0		4.33
October	10	0	0	0	0	0	0.01	0.1	0.15	0.02	0	0	0	0.11	0	0.87	0.77	0.25	0	0	0	0	0	0	0.51	0	0.09	0.11	0	0	0.33	0.13	3.45
November	11	0	0.14	0.31	0	0	0	0	0	0	0.54	0.07	0	0	0	0	0	0	0	0	0	0.01	0	0.06	0	0.03	0	0	0	0	0.73	0.26		2.15
December	12	0	1.73	0	0	0.33	0	0	0.04	0.34	0.31	0.66	0	0.08	0.22	0	0	0.3	0	0	0.06	1.84	0	0	0	0.1	0	0.09	0	0	0.09	0.01	6.2
1968 Totals	**1968**	**1.76**	**0.3**	**2.85**	**0.15**	**0**	**0.42**	**0.02**	**0.62**	**0.17**	**0.65**	**0.36**	**0.78**	**0.65**	**0.71**	**3.87**	**0.25**	**3.88**	**0.27**	**0.68**	**0.07**	**0.15**	**1.15**	**1.42**	**0.81**	**2.93**	**0.21**	**1.57**	**2.44**	**1.06**	**0.74**	**1.55**	**32.49**
January	1	0	0	0	0	0	0.07	0	0.01	0.04	0	0	0.13	0.21	0.16	0	0	0	0	0	0	0	0	0	0	0	0	0	0.14	0	0.95	0.15	0	1.86
Feburary	2	0.98	0	0	0	0	0.02	0	0	0	0	0	0	0	0	0.02	0	0	0	0	0	0	0	0	0	0	0	0.07	0	0	0			1.09
March	3	0	0	0	0	0	0	0	0.08	0	0.05	0.09	0.61	0	0	0.72	0	0	0.12	0.2	0.06	0.08	0	0	0	0	0	0	0	0	0.04	0	0.01	2.06
April	4	0	0.11	0.95	0	0	0	0	0	0	0	0	0	0.04	0.01	0	0.13	0.04	0	0.16	0.01	0	0.03	0	0	0	0	0	0	0	0	0		1.48
May	5	0	0	0	0	0	0	0.01	0	0	0.58	0.13	0	0.11	0	0.38	0	0.19	0	0	0	0	0.48	1.22	0.01	2.47	0	0	0.52	0.07	0	0.61	6.78
June	6	0.03	0	0	0	0	0	0	0	0	0	0.02	0	0	0	0.3	0.02	0	0	0.08	0	0	0.24	0	0.06	0.11	0.04	0	0	0	0		0.9
July	7	0.08	0	0	0	0	0	0	0.03	0	0	0	0	0	0.46	0.44	0	0.7	0	0	0	0	0	0	0.67	0.35	0.03	0.31	0	0	0	0.85	3.92
August	8	0	0.01	0.75	0	0	0	0	0.25	0	0.02	0	0	0	0	0.24	0	0.15	0	0	0	0	0	0	0	0	0	0	0	0	0	0.1	0.08	1.6
September	9	0.31	0	0	0.15	0	0	0	0.25	0	0	0	0	0	0	0	0.09	2.25	0	0.24	0	0	0.25	0.13	0.07	0	0	0	0	0	0		3.74
October	10	0	0	0	0	0	0.03	0	0	0.13	0	0	0	0.29	0.02	0	0	0.21	0	0	0	0	0.01	0	0	0	0	0	0	0	0	0	0.69
November	11	0	0.18	1.15	0	0	0.3	0.01	0	0	0	0.12	0	0	0.06	1.77	0.01	0.34	0.01	0	0	0	0	0.07	0	0	0.07	0.09	1.56	0	0		5.74
December	12	0.36	0	0	0	0	0	0	0	0	0	0	0.04	0	0	0	0	0	0.14	0	0	0.07	0.14	0	0	0	0	1.03	0.36	0	0.49	0	2.63
1969 Totals	**1969**	**1.53**	**1.83**	**0.07**	**1.1**	**0.46**	**1.65**	**0.99**	**2.33**	**1.97**	**1.54**	**1.53**	**1.52**	**1.67**	**1.78**	**0.47**	**3.37**	**1.15**	**3.28**	**0**	**0.86**	**1.23**	**2.68**	**2.44**	**0.47**	**0.11**	**0.63**	**1.94**	**2.86**	**1.43**	**0.57**	**0.26**	**43.72**
January	1	0	0	0	0	0.05	0	0	0	0	0	0	0	0	0	0.02	0.53	0.4	0	0	0	0.01	0	0.59	0	0	0.13	0.3	0.21	1.33	0.01	0.03	3.61
Feburary	2	0	0.06	0	0	0.03	0.02	0	0.67	0	0	0	0	0	0	0.15	0.01	0	0	0	0	0	0.35	0	0	0	0	0.3	0.45				2.04
March	3	0	0	0	0	0	0	0	0.6	0	0	0	0	0	0	0	0	0	0	0	0	0	0.04	1.35	0.41	0.01	0.03	0	0.03	0	0	0	2.47
April	4	0	0.13	0	0.73	0.07	0	0	0	0.67	0	0	0	0.6	0.16	0	0	0.02	1.37	0	0	0	0	0	0	0	0	0.26	0	0	0		4.01
May	5	0	0	0	0	0	0	0.08	0.2	0	0	0	0	0.34	0	0	0	0	0.04	0	0	1.13	0.2	0	0	0	0	0	0	0	0.01	0.11	2.11
June	6	1.32	0	0	0	0	0	0	0.37	0.01	0	0	0	0	1.6	0.02	0	0.05	0.99	0	0	0	1.99	0	0	0	0	0.15	2.1	0	0.05		8.65
July	7	0.2	1.54	0.01	0	0.31	0.87	0.41	0.36	1.29	0.26	0.49	0	0	0	0	0	0.21	0	0	0.5	0	0	0	0.01	0	0.47	0.15	0	0	0	0	7.08
August	8	0	0	0	0	0	0	0	0.13	0	0	0	0	0	0	0.05	0	0	0	0	0.33	0.01	0	0	0	0	0	0	0	0	0	0	0.52
September	9	0.01	0.03	0.06	0.37	0	0.06	0.36	0	0	0	0.1	0	0	0	0.27	2.78	0.29	0	0	0	0	0	0	0.12	0	0	0	0.58	0	0	0		5.03
October	10	0	0.07	0	0	0	0.32	0	0	0	1.2	0.88	1.51	0.73	0	0	0	0	0.63	0	0.03	0	0	0	0	0	0	0	0	0	0.28	0.12	5.77
November	11	0	0	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0	0.18	0.25	0	0	0	0	0	0	0	0	0	0	0	0		0.44
December	12	0	0	0	0	0	0.38	0.14	0	0	0.08	0.06	0	0	0.02	0.01	0	0	0	0	0	0.08	0.1	0.38	0.05	0.1	0	0.2	0.07	0.1	0.22	0	1.99
1970 Totals	**1970**	**1.8**	**0.45**	**0.8**	**0.35**	**1.82**	**0.63**	**0.23**	**3.02**	**2.22**	**0.1**	**0.2**	**2.03**	**2.01**	**1.54**	**0.86**	**0.74**	**1.64**	**1.28**	**2.08**	**1.58**	**0.56**	**1.56**	**3.05**	**0.94**	**0.52**	**0.5**	**0.47**	**0.73**	**0.01**	**2.47**	**0.01**	**36.2**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0	0.07	0	0	0	0	0	0	0	0.06	0.01	0	0	0	0	0	0.06	0	0	0	0	0.01	0.01	0	0	0	0	0	0	0	0	0.22
Feburary	2	0.1	0.07	0	0	0	0	0.04	0.06	0.09	0	0	0	0.04	0.19	0	0	0	0	0	0	0	0	0	0	0	0	0	0.05				0.64
March	3	0.34	0.21	0.11	0	0	0	0	0	0	0	0.1	0.21	0	0	0	0.02	0.18	0.16	0.14	0	0	0.14	0	0	0.49	0.03	0	0.04	0	0	0	2.17
April	4	0.34	0.04	0	0.16	0.01	0	0	0	0	0	0	0.86	0.01	0	0	0.09	0.28	0.86	1.35	0.04	0	0.05	2.31	0.01	0	0	0.35	0	0	2.33		9.09
May	5	0	0	0	0	0.01	0	0	0	0.99	0.03	0	0	0.01	0.66	0.12	0	0	0	0	0	0	0.09	0.02	0	0	0	0	0	0.01	0.1	0	2.04
June	6	0.87	0.03	0.68	0.09	0.22	0	0	0	0	0	0	0.94	0.59	0.08	0.07	0	0	0	0.05	0.56	0	0	0	0.9	0	0	0	0	0	0		5.08
July	7	0	0	0.01	0	0	0	0	0	0	0	0	0	0	0	0.2	0	0	0.03	0.28	0	0	0	0.05	0	0	0	0.03	0	0	0	0	0.6
August	8	0	0	0	0.06	1.55	0.63	0	1.94	0.34	0.01	0.08	0	0	0	0	0.02	0.83	0	0	0.97	0	0.01	0	0	0	0	0	0	0	0	0	6.44
September	9	0	0.01	0	0	0.03	0	0.18	0.91	0.28	0	0	0	0.57	0.56	0	0.33	0.29	0.23	0.06	0	0	1.09	0.65	0	0.03	0.32	0	0	0	0		5.54
October	10	0.15	0	0	0	0	0	0.01	0.11	0.02	0	0	0.02	0.79	0	0	0	0	0	0.03	0	0	0.17	0.01	0.03	0	0.15	0.09	0.63	0	0	0	2.21
November	11	0	0.02	0	0.04	0	0	0	0	0.5	0	0.01	0	0	0.05	0	0	0	0	0.14	0	0	0	0	0	0	0	0	0.01	0	0		0.77
December	12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.47	0.28	0	0	0.03	0.01	0.56	0	0	0	0	0	0	0	0	0.04	0.01	1.4
1971 Totals	**1971**	**0.36**	**0.36**	**1.1**	**2.4**	**0.61**	**3.1**	**1.51**	**0.27**	**0.67**	**4.13**	**1.6**	**0.23**	**0.4**	**4.08**	**0.29**	**0.7**	**0**	**1.55**	**1.12**	**0.87**	**2.03**	**0.37**	**3.22**	**0.64**	**0.2**	**0.54**	**0.06**	**0.75**	**0.43**	**0.14**	**0**	**33.73**
January	1	0	0	0.55	0	0	0	0	0	0	0	0	0.01	0.06	0	0	0	0	0	0	0	0	0	0	0	0	0	0.02	0	0	0.02	0	0.66
Feburary	2	0	0	0.21	1.36	0	0.01	0.04	0	0	0	0.03	0.11	0	0	0	0	0	0	0.04	0	1.12	0.14	0	0	0	0.01	0	0.01				3.08
March	3	0	0	0	0	0	0.59	0	0	0.18	0	0	0	0	0.96	0	0	0	0.04	0	0	0	0	0	0	0.04	0	0	0	0	0	0	1.81
April	4	0.04	0	0	0	0.33	0.52	0	0	0	0	0	0	0.05	0	0	0	0	0	0	0.67	0	0	0	0	0	0	0.04	0	0	0		1.65
May	5	0.2	0	0	0.02	0.09	0.84	1.04	0.01	0	0.4	0.09	0.06	0	0	0	0	0	0	0	0	0	0.23	2.02	0.6	0	0.06	0	0	0	0	0	5.66
June	6	0	0.36	0	0	0	0	0.2	0	0	0.5	1	0.02	0.15	0.01	0	0	0	0	0	0	0.18	0	0	0	0	0	0	0	0.01	0		2.43
July	7	0	0	0	1.02	0	0	0	0	0	0.95	0	0	0.04	0.72	0	0	0	0.7	0	0	0	0	0.67	0	0	0	0	0.3	0.3	0	0	4.7
August	8	0	0	0	0	0	0	0	0	0	0	0.04	0	0	0	0	0	0	0	0	0	0.04	0	0	0	0	0	0	0	0	0	0	0.08
September	9	0	0	0.1	0	0.18	0.75	0	0	0	0.13	0.44	0	0	0	0.08	0.7	0	0.29	0.95	0.2	0	0	0	0	0.16	0	0	0	0	0		3.98
October	10	0	0	0.24	0	0	0	0	0.08	0	0	0	0	0.02	0	0	0	0	0	0	0	0.69	0	0.48	0	0	0	0	0	0	0	0	1.51
November	11	0.12	0	0	0	0	0.01	0	0.01	0	0	0	0	0	0	0	0	0	0.52	0	0	0	0	0.05	0.04	0	0.47	0	0.44	0.01	0		1.67
December	12	0	0	0	0	0.01	0.38	0.23	0.17	0.49	2.15	0	0.03	0.08	2.39	0.21	0	0	0	0.13	0	0	0	0	0	0	0	0	0	0.11	0.12	0	6.5
1972 Totals	**1972**	**3.42**	**2.85**	**1.16**	**0.44**	**0.55**	**0.97**	**2.7**	**0.17**	**0.19**	**0.38**	**0.35**	**2.16**	**2.23**	**1.33**	**2.51**	**0.09**	**0.08**	**0.54**	**1.53**	**0.53**	**1.89**	**0.13**	**0.8**	**0.75**	**0.47**	**0.65**	**1.09**	**1.22**	**1.21**	**0.65**	**0.7**	**33.74**
January	1	0.01	0	0.08	0.2	0	0	0	0	0	0	0	0	0.08	0	0	0	0	0	0	0	0	0	0	0	0	0	0.4	0	0	0	0	0.77
Feburary	2	0	0.05	0.01	0	0	0.01	0	0.04	0.04	0	0	0.01	0.03	0.09	0.01	0	0.01	0	0	0	0	0	0.28	0	0.14	0.02	0	0	0			0.74
March	3	0	0	0	0	0	0	0	0	0	0	0	0.22	0.67	0	0.95	0.01	0	0	0	0	0.05	0	0	0	0.02	0.06	0.33	0.07	0.32	0	0.23	2.93
April	4	0	0	0.36	0	0	0	0.16	0	0.04	0	0.16	0	0.25	0.34	0.97	0.08	0	0	0.22	0.53	0.6	0	0	0	0	0	0	0.75	0	0.03		4.49
May	5	0.31	0	0	0	0	0	0	0.1	0	0	0	0.28	0.05	0.04	0	0	0	0	0	0	0	0	0	0	0	0	0.23	0	0.01	0	0	1.02
June	6	0	0	0	0	0	0	0	0	0.07	0.13	0	0	0	0.19	0.1	0	0	0	0.61	0	0	0	0	0.02	0	0	0	0.07	0	0		1.19
July	7	0.03	1.19	0	0.15	0	0	0	0	0	0	0	0	0	0	0.43	0	0.01	0.48	0	0	0	0	0.07	0	0	0.47	0.03	0.24	0	0	0	3.1
August	8	0	0.9	0.62	0	0	0.81	0	0.03	0	0	0	0.02	0	0	0	0	0	0	0	0	0	0	0.28	0.01	0.02	0	0	0	0	0	0	2.69
September	9	0.2	0.71	0	0	0	0	2.52	0	0	0	0	0	0	0.67	0	0	0	0	0	0	0.77	0.01	0.17	0.72	0.05	0.06	0	0.07	0.26	0		6.21
October	10	0	0	0	0	0	0.1	0	0	0	0	0	0.01	0	0	0	0	0.06	0	0	0	0.4	0.08	0	0	0	0	0.1	0	0	0.25	0.47	1.47
November	11	2.87	0	0	0	0	0.03	0	0	0.01	0.25	0	0.31	1.15	0	0	0	0	0.06	0.52	0	0.07	0.04	0	0	0.24	0.04	0	0	0	0		5.59
December	12	0	0	0.09	0.09	0.55	0.02	0.02	0	0.03	0	0.19	1.31	0	0	0.05	0	0	0	0.18	0	0	0	0	0	0	0	0	0.02	0.62	0.37	0	3.54
1973 Totals	**1973**	**0.68**	**0.55**	**1.43**	**3.1**	**0.28**	**1.27**	**1.8**	**0.55**	**4.27**	**1.75**	**0.01**	**0.63**	**2.02**	**1.23**	**0.57**	**0.83**	**0.7**	**2.21**	**2.38**	**0.8**	**0.6**	**1.58**	**2.06**	**2**	**1.04**	**0.65**	**0.73**	**0.53**	**0.55**	**1.61**	**1.41**	**39.82**
January	1	0	0	0.45	0	0	0	0.01	0.06	0.01	0	0	0	0	0	0	0	0	0.3	0	0	0.35	0.11	0	0	0	0.02	0	0.09	0	0	0	1.4
Feburary	2	0.38	0.01	0	0	0	0	0.26	0	0	0	0	0.19	0.17	0	0.01	0	0	0.02	0	0	0	0	0	0	0	0	0	0	0			1.04
March	3	0	0.17	0	0.74	0	0.96	0	0	0.41	0.99	0	0	0.01	0.46	0	0.16	0.04	0	0.34	0.3	0	0	0	0.09	0.28	0.02	0	0.01	0.14	0	0.69	5.81
April	4	0.01	0.01	0.23	0.04	0	0	0	0.38	0.58	0	0	0	0	0.55	0.12	0.64	0	0.03	0.43	0.05	0.1	1.08	0	0	0	0	0	0	0	0		4.25
May	5	0.14	0	0	0	0	0.3	1.53	0.01	0.3	0.76	0.01	0	0	0	0	0	0	0	0	0	0.12	0.34	0	0	0	0.19	0.16	0.04	0.02	0	0	3.92
June	6	0	0.3	0.09	0.85	0.28	0	0	0	0	0	0	0	0.1	0.07	0.04	0	0.18	1.66	0.45	0	0.03	0	0	0.02	0	0.14	0.02	0	0	0		4.23
July	7	0	0	0	0.15	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0	0.1	0.03	0	0	2.05	0	0.21	0	0.04	0	0.18	0.08	0	2.85
August	8	0	0	0	0.01	0	0	0	0	0.97	0	0	0.05	1.18	0.02	0	0.03	0.01	0	0	0	0	0	0	0	0	0	0	0	0.19	0	0	2.46
September	9	0	0	0.07	0.18	0	0	0	0.1	1.98	0	0	0	0	0	0	0	0.26	0	0	0	0	0.05	0	0.02	0	0	0	0.34	0	0.52		3.52
October	10	0.15	0.06	0	0.13	0	0	0	0	0	0	0	0.38	0.49	0	0	0	0	0	0	0	0	0	0	0	0	0	0.36	0.04	0	0.03	0.69	2.33
November	11	0	0	0	0.12	0	0	0	0	0	0	0	0	0	0	0.37	0	0.21	0	0	0.42	0	0	0	1.56	0.55	0.28	0.14	0	0	0		3.65
December	12	0	0	0.59	0.88	0	0.01	0	0	0.02	0	0	0.01	0.07	0.12	0.03	0	0	0.2	1.06	0	0	0	0.01	0.31	0	0	0.01	0.01	0.02	0.98	0.03	4.36
1974 Totals	**1974**	**0.13**	**0.61**	**0.87**	**1.26**	**0.15**	**0.8**	**0.89**	**0.5**	**1.12**	**2.61**	**1.93**	**0.15**	**0.13**	**3.49**	**0.35**	**0.51**	**0.45**	**1.08**	**1.26**	**1.4**	**2.55**	**1**	**0.5**	**0.58**	**0.09**	**0.32**	**0.17**	**5.6**	**1.17**	**3.03**	**2.13**	**36.83**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0	0	0	0	0	0	0	0.19	0.62	0.08	0.01	0	0	0	0	0	0	0.29	0.27	0.78	0	0.45	0	0	0	0.32	0	0.5	0	0	0	3.51
Feburary	2	0	0	0	0	0.02	0.68	0.02	0	0	0	0	0	0	0	0	0	0	0.77	0.45	0	1.68	0.08	0.04	0.43	0	0	0	0				4.17
March	3	0	0	0.02	0.27	0	0	0.02	0	0.2	0.05	0.31	0	0	0	0.35	0	0	0	0	0.27	0	0	0.41	0	0	0	0	0.44	0.24	0	0	2.58
April	4	0	0	0.25	0.05	0	0	0.41	0.12	0	0.19	0.11	0.04	0	0.07	0	0.35	0	0	0.02	0	0.61	0.02	0	0	0	0	0	0.06	0.05	0.05		2.4
May	5	0	0.19	0	0	0	0	0.14	0.05	0	0.12	0.66	0	0	0.68	0	0	0.45	0	0	0	0.26	0.01	0	0	0.07	0	0	0.01	0.32	2.63	0.31	5.9
June	6	0	0	0	0	0.02	0.05	0.24	0.14	0.25	0	0.14	0	0.01	1.62	0	0	0	0	0.52	0	0	0.4	0	0	0	0	0	0	0	0.06		3.45
July	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.35	0	0.04	0	0	0	0	0	0.51	0	0	0	0.9
August	8	0	0.04	0	0	0	0	0.02	0	0.05	1.09	0	0	0	0	0	0.01	0	0	0	0	0	0	0	0.05	0	0	0.16	2.53	0.14	0	0.96	5.05
September	9	0.01	0.35	0	0	0	0	0	0	0	0.11	0.36	0.02	0	0	0	0.14	0	0	0	0	0	0	0	0	0	0	0	1.51	0	0		2.5
October	10	0	0	0	0.02	0.06	0	0	0	0	0	0	0.09	0.01	1.1	0	0	0	0	0	0	0	0	0	0	0.02	0	0	0.04	0.17	0	0	1.51
November	11	0	0.03	0.6	0.92	0.05	0	0	0	0	0.97	0.01	0	0.11	0	0	0	0	0	0	0	0	0	0.02	0	0	0	0	0	0.17	0.27		3.15
December	12	0.12	0	0	0	0	0.07	0.04	0	0	0	0.33	0	0	0.02	0	0.01	0	0.02	0	0	0	0	0.03	0.1	0	0	0.01	0	0.08	0.02	0.86	1.71
1975 Totals	**1975**	**0.51**	**0.41**	**0.76**	**0.05**	**1.4**	**1.25**	**0.48**	**0.85**	**0.97**	**2.48**	**2.52**	**0.24**	**0.29**	**2.01**	**1.14**	**1.72**	**1.21**	**1.14**	**1.94**	**0.18**	**0.01**	**2.09**	**2.68**	**2.27**	**2.4**	**1.37**	**1.44**	**1.16**	**2.88**	**1.93**	**0.43**	**40.21**
January	1	0	0.16	0	0	0	0.02	0.01	0.08	0.34	2.09	0	0	0	0.06	0	0	0	0	0.43	0	0	0	0	0.21	0.09	0	0	0.08	0.03	1.41	0.37	5.38
Feburary	2	0.08	0	0	0.04	0.11	0	0	0.01	0.01	0	0.23	0	0	0.03	0.03	0.43	0	0.02	0	0	0	1.62	0.48	0.5	0	0	0	0				3.59
March	3	0.02	0	0	0	0	0.03	0.36	0	0.37	0.13	0.95	0	0	0	0	0	0	0.34	0	0	0.01	0	0.02	0	0	0.03	1.44	0.38	0	0	0	4.08
April	4	0	0.04	0	0	0	0	0	0.03	0	0	0	0	0	0.31	0	0.19	0	0.48	0	0	0	0	1.76	1.44	0	0	0	0	0.31	0		4.56
May	5	0	0	0.1	0	0	0.46	0.11	0.57	0	0	0.49	0	0	0	0	0	0	0	0.47	0.03	0	0	0	0.08	0.12	0	0	0.48	0.15	0.17	0	3.23
June	6	0.19	0	0	0	0	0	0	0	0	0	0	0	0.02	0.35	0.25	1.08	0.41	0	0	0	0	0.47	0.22	0	0.79	0	0	0	0	0		3.78
July	7	0	0	0	0	0.85	0.54	0	0	0	0	0	0.2	0.1	0	0	0	0.06	0.3	0.09	0	0	0	0.2	0	0	0	0	0	0	0.16	0.06	2.56
August	8	0.12	0.1	0	0	0.36	0	0	0	0	0	0	0	0.17	0.37	0.56	0	0.48	0	0	0	0	0	0	0	1.15	0.58	0	0.02	1.53	0	0	5.44
September	9	0	0	0	0	0	0	0	0	0	0.26	0.85	0	0	0	0	0.02	0.26	0	0.95	0	0	0	0	0	0	0	0	0	0.01	0.13		2.48
October	10	0	0	0	0	0	0	0	0.03	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.04	0	0	0	0.05	0.09	0	0	0.21
November	11	0.1	0.11	0.66	0.01	0	0.18	0	0	0.25	0	0	0	0	0	0	0	0	0	0	0.15	0	0	0	0	0	0.76	0	0	0.34	0.06		2.62
December	12	0	0	0	0	0.08	0.02	0	0.13	0	0	0	0.04	0	0.89	0.3	0	0	0	0	0	0	0	0	0	0.25	0	0	0.15	0.42	0	0	2.28
1976 Totals	**1976**	**0.02**	**0.6**	**1.49**	**1.05**	**1.55**	**1.13**	**0.54**	**0.04**	**0.26**	**0.06**	**0.26**	**0**	**0.68**	**0.81**	**0.62**	**0.21**	**0.04**	**0**	**0.94**	**0.46**	**0.61**	**0.01**	**2.96**	**1**	**0.96**	**1.51**	**0.41**	**0.96**	**0.44**	**2.56**	**1.28**	**23.46**
January	1	0.01	0	0	0	0	0	0.28	0	0	0	0	0	0.08	0	0	0	0	0	0.06	0	0	0	0	0	0.38	0	0	0	0	0	0.02	0.83
Feburary	2	0	0.27	0	0	0.44	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0	0.15	0.21	0	0	0	0	0	0	0				1.08
March	3	0	0	1.49	0.93	0	0	0	0	0	0.01	0.26	0	0	0	0.28	0.2	0	0	0	0.01	0	0.01	0	0.05	0	0.51	0.16	0.01	0.36	0	0	4.28
April	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.71	0.29	0	0	0	0.18	0.13	0	0.06	0	0	0		1.37
May	5	0.01	0	0	0	0.03	0.2	0	0	0	0	0	0	0.6	0.06	0.32	0	0.04	0	0	0	0	0	0	0	0	0	0.04	0.11	0.02	1.78	0.69	3.9
June	6	0	0	0	0.04	0.1	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0	0	0	0	1.52	0.65	0	0	0	0	0	0		2.32
July	7	0	0.33	0	0	0	0	0.25	0	0	0	0	0	0	0	0	0	0	0	0	0	0.4	0	0	0	0	0.05	0	0.68	0	0	0.57	2.28
August	8	0	0	0	0	0.21	0.04	0	0	0	0	0	0	0	0.75	0.01	0	0	0	0	0	0	0	0	0	0.26	0	0	0	0	0	0	1.27
September	9	0	0	0	0	0	0	0	0.02	0.26	0	0	0	0	0	0	0	0	0	0	0	0	0	0.03	0	0.17	0.29	0.13	0	0	0		0.9
October	10	0	0	0	0.08	0.77	0	0	0	0	0	0	0	0	0	0	0	0	0	0.17	0.01	0	0	1.38	0.12	0	0	0	0	0.06	0.78	0	3.37
November	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.03	0	0.02	0.66	0.02	0	0	0		0.73
December	12	0	0	0	0	0	0.89	0.01	0.02	0	0.05	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.16	0	0	0	1.13
1977 Totals	**1977**	**0.75**	**0.44**	**0.18**	**1.34**	**2.22**	**0.97**	**2.38**	**1.77**	**1.34**	**1.98**	**2.52**	**1.38**	**1.9**	**0.7**	**1.46**	**0.05**	**0.2**	**0.93**	**1.19**	**0.34**	**3.25**	**0.08**	**3.08**	**2.43**	**1.54**	**2.34**	**1.95**	**3.09**	**0.07**	**1.27**	**0.27**	**43.41**
January	1	0	0.22	0.01	0.61	0.01	0.14	0	0	0.39	0.03	0	0	0.33	0.02	0.09	0	0	0.01	0.12	0	0	0	0.32	0	0.02	0	0.03	0.03	0	0	0	2.38
Feburary	2	0	0	0	0	0	0	0	0	0	0	0	0.38	0	0.01	0	0	0	0	0.11	0	0	0	0.74	0	0	1.01	0.05	0.17				2.47
March	3	0.01	0.1	0.02	0	0	0	0	0	0	0	2.26	0.26	0	0	0	0	0.17	0.02	0.02	0	0.17	0	0	0	0	0	0.87	2.38	0	0	0	6.28
April	4	0.2	0.02	0	0.05	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0	0.3	0.01	0.33	0	0	0	0	0	0	0	0	0.07		0.99
May	5	0.21	0	0.01	0.38	0.08	0.69	0.02	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.56	0	0	0	0	0.18	0	2.13
June	6	0	0	0	0	0	0	0	0.1	0	0	0	0	0.73	0	0	0	0	0	0	0	1.24	0.08	0.4	0.85	0.01	1.28	0.68	0.04	0	0.06		5.47
July	7	0	0	0	0	0	0	0	0.07	0	1.31	0.23	0.11	0	0	0	0	0	0	0	0	1.49	0	0	0.31	0.76	0	0	0	0	0	0	4.28
August	8	0	0	0	0	0	0	0.63	1.2	0.77	0.6	0.02	0	0	0	0	0	0	0	0	0	0	0	1.58	0	0	0	0	0.47	0.07	0	0	5.34
September	9	0	0	0.07	0.01	0.58	0	0	0	0	0	0	0.63	0.14	0.66	0.15	0	0	0.9	0	0	0	0	0	0.32	0.18	0	0	0	0	0		3.64
October	10	0.04	0	0	0.13	0.68	0	1.65	0	0	0.04	0.01	0	0	0	0.02	0	0	0	0	0	0	0	0	0.95	0.01	0	0	0	0	0	0.23	3.76
November	11	0.21	0.1	0.06	0.02	0	0.14	0.06	0	0.18	0	0	0	0	0	1.2	0.02	0	0	0.64	0.33	0	0	0.04	0	0	0.05	0.32	0	0	0.96		4.33
December	12	0.08	0	0.01	0.14	0.86	0	0.02	0.4	0	0	0	0	0.7	0.01	0	0.03	0.03	0	0	0	0.02	0	0	0	0	0	0	0	0	0	0.04	2.34
1978 Totals	**1978**	**0.25**	**1.84**	**0.56**	**0.53**	**0.02**	**0.71**	**2.71**	**0.58**	**0.38**	**0.88**	**0.76**	**2.47**	**2.64**	**2.75**	**0.81**	**4.55**	**1.44**	**1.09**	**0.14**	**0.34**	**0.13**	**1.03**	**1.59**	**3.34**	**1.58**	**1.93**	**0.36**	**0.57**	**0.45**	**0.65**	**0.63**	**37.71**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0	0	0	0	0	0	0.04	0	0	0	0	0.11	0.02	0.01	0.05	0.84	0.16	0	0	0.01	0	0	0	0.23	0.2	0	0	0	0	0.02	0.01	1.7
Feburary	2	0	0	0	0.08	0	0	0	0	0	0	0	0.24	0.78	0.01	0	0	0	0	0	0.01	0	0.08	0.02	0	0	0	0.22	0.16				1.6
March	3	0	0.34	0.02	0	0	0.02	1.8	0.5	0	0	0.06	0.01	0.75	0	0	0	0.08	0	0	0.28	0	0	0.5	1.9	0.35	0.05	0	0	0.01	0	0	6.67
April	4	0	0.07	0	0.03	0	0.31	0	0	0	0.39	0	0	0	0	0.29	0.33	0.98	0.14	0.14	0	0	0.21	0.08	0.08	0.02	0	0	0	0.01	0.13		3.21
May	5	0	0	0.09	0.42	0	0.06	0.59	0.01	0	0	0.65	0.54	0.31	0	0	0	0	0	0	0.04	0	0.44	0.1	0	0.07	0	0	0.37	0	0	0	3.69
June	6	0.16	0	0	0	0	0.14	0.09	0	0	0	0	0	0	0	0	0	0	0.95	0	0	0	0.06	0.45	0.54	0	0	0	0	0	0		2.39
July	7	0	1.14	0	0	0	0	0	0	0.21	0.24	0	0.1	0.02	2.5	0	0	0	0	0	0	0	0	0.36	0.59	0	0.87	0	0	0	0	0	6.03
August	8	0.09	0.06	0	0	0	0	0	0	0	0.16	0.05	0	0	0	0.02	0	0	0	0	0	0	0	0	0	0.02	0	0.14	0.02	0	0.2	0	0.76
September	9	0	0	0	0	0	0	0	0	0	0	0	0.15	0	0.04	0	2.58	0	0	0	0	0.13	0	0	0	0	0	0	0	0	0.2		3.1
October	10	0	0.16	0.14	0	0.02	0	0	0	0.17	0.09	0	1.32	0.12	0.01	0	0	0	0	0	0	0	0	0.07	0	0.18	0	0	0	0	0	0	2.28
November	11	0	0	0	0	0	0.16	0	0	0	0	0	0	0.64	0.18	0.45	0.8	0.22	0	0	0	0	0.24	0.01	0	0.74	1.01	0	0	0.02	0		4.47
December	12	0	0.07	0.31	0	0	0.02	0.19	0.07	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.02	0.41	0.1	0.62	1.81
1979 Totals	**1979**	**0.59**	**0.59**	**0.92**	**0.39**	**0.14**	**0.07**	**0.27**	**0.71**	**0.55**	**0.18**	**5.04**	**0.12**	**0.57**	**0.11**	**0.92**	**0.11**	**0.24**	**0.15**	**0.6**	**0.73**	**1.64**	**2.01**	**2.55**	**1.53**	**2.06**	**0.93**	**1.63**	**1.64**	**1.17**	**0.79**	**0.53**	**29.48**
January	1	0.03	0	0	0	0.12	0.06	0.13	0	0	0	0.06	0.02	0.22	0	0	0	0	0.07	0.31	0	0	0	0.4	0	0	0.07	0.35	0	0	0.11	0	1.95
Feburary	2	0	0.05	0.01	0	0	0	0	0.14	0	0	0	0	0	0	0.03	0.01	0	0.02	0	0.44	0.01	0.5	0.12	0	0	0	0	0.15				1.48
March	3	0	0	0.69	0.11	0	0.01	0.01	0	0.19	0	0	0	0.01	0	0	0	0.04	0.06	0.21	0.14	0	0.79	0.7	0.06	0.07	0.03	0.07	0.03	0.22	0.19	0	3.63
April	4	0.23	0.02	0	0.25	0	0	0	0.34	0	0.12	4.79	0	0	0	0	0.04	0.08	0	0.03	0.05	0.1	0	0.4	0.48	0.13	0.41	0	0	0	0		7.47
May	5	0	0.48	0.15	0.03	0	0	0	0	0	0	0.19	0.1	0.01	0	0	0	0	0	0.01	0.05	0	0	0	0.02	0	0.26	0	0	0	0.2	0.12	1.62
June	6	0	0	0	0	0	0	0.06	0.19	0	0.06	0	0	0.01	0	0	0	0	0	0	0.01	0	0	0.29	0	0	0	0	1.05	0	0		1.67
July	7	0	0.04	0.02	0	0.02	0	0	0	0	0	0	0	0.32	0	0	0	0	0	0	0	0	0	0.04	0	0.99	0.13	1.12	0.38	0.28	0.25	0.08	3.67
August	8	0.33	0	0	0	0	0	0	0	0	0	0	0	0	0.11	0	0	0	0	0	0.04	0.96	0.15	0	0	0	0	0	0.01	0.66	0	0	2.26
September	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		0
October	10	0	0	0.05	0	0	0	0	0	0.01	0	0	0	0	0	0.89	0.06	0.12	0	0.04	0	0	0.46	0	0	0	0	0	0	0	0	0.18	1.81
November	11	0	0	0	0	0	0	0.07	0.04	0.35	0	0	0	0	0	0	0	0	0	0	0	0.57	0.02	0	0	0.87	0.03	0.09	0.02	0.01	0		2.07
December	12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.09	0.6	0.97	0	0	0	0	0	0.04	0.15	1.85
1980 Totals	**1980**	**0.49**	**0.21**	**1.94**	**0.97**	**0.4**	**0.21**	**0.61**	**0.77**	**0.18**	**0.77**	**0.03**	**0.88**	**0.55**	**0.74**	**1.22**	**4.56**	**1.96**	**0.01**	**0.04**	**0.43**	**1.33**	**0.14**	**2.13**	**0.56**	**0.06**	**0.21**	**1.82**	**1.08**	**0.22**	**2.02**	**0.94**	**27.48**
January	1	0	0	0.02	0	0.06	0.1	0	0	0	0.05	0.01	0	0	0	0	0.08	0	0	0.01	0.01	0	0	0	0	0	0	0	0	0	0.28	0.01	0.63
Feburary	2	0	0	0	0	0.13	0	0	0.26	0.01	0	0	0	0	0.16	0.71	0	0	0	0	0	0.04	0	0	0	0.06	0	0	0	0.17			1.54
March	3	0.18	0	0	0.02	0.02	0	0.01	0	0	0	0	0.59	0.07	0	0	0.12	0.53	0	0	0.42	0	0	0.2	0.25	0	0	0	0.29	0	1.28	0	3.98
April	4	0	0	0.11	0	0	0	0.6	0.09	0.04	0	0.02	0	0.17	0.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0		1.54
May	5	0	0	0	0	0	0	0	0	0	0.25	0	0.29	0	0	0	0.81	0.07	0.01	0	0	0	0.12	0.68	0	0	0	0	0	0	0.46	0.71	3.4
June	6	0	0	0	0.47	0	0.02	0	0	0	0	0	0	0	0	0	0	0	0	0.03	0	0	0	0.88	0	0	0	0	0.79	0	0		2.19
July	7	0	0.13	1.8	0	0	0	0	0	0	0.37	0	0	0	0	0	0	0	0	0	0	1.18	0	0	0	0	0.02	0.06	0	0	0	0	3.56
August	8	0.03	0	0	0.14	0.19	0	0	0	0	0.1	0	0	0.04	0.03	0.37	1.36	0.09	0	0	0	0.11	0	0	0	0	0	0	0	0.04	0	0.22	2.72
September	9	0.25	0.08	0	0.32	0	0.09	0	0	0	0	0	0	0.27	0	0	2.08	0.01	0	0	0	0	0.02	0	0	0	0	0	0	0	0		3.12
October	10	0.03	0	0.01	0.02	0	0	0	0	0	0	0	0	0	0	0.08	0.11	1.23	0	0	0	0	0	0	0.15	0	0	1.26	0	0	0	0	2.89
November	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0.05	0.06	0	0.03	0	0	0	0	0	0.37	0.05	0	0.19	0.5	0	0	0		1.25
December	12	0	0	0	0	0	0	0	0.42	0.13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.11	0	0	0	0	0	0	0	0.66
1981 Totals	**1981**	**1.58**	**0.45**	**0.63**	**1.54**	**2.32**	**0.02**	**0.5**	**0.09**	**0.98**	**2.71**	**0.53**	**0.04**	**0.34**	**1.22**	**1.86**	**1.35**	**1.34**	**2.25**	**4.22**	**2.83**	**2.37**	**3.26**	**2.03**	**0.85**	**0.37**	**1.54**	**2.62**	**1.1**	**1.95**	**1.17**	**1.46**	**45.52**
January	1	0.01	0	0	0	0	0.02	0	0	0	0	0	0	0	0	0	0	0	0	0	0.28	0.01	0	0	0	0	0	0	0	0.04	0	0.28	0.64
Feburary	2	0.27	0.01	0	0	0	0	0	0	0.54	0.61	0	0	0	0	0	0	0	0	0	0	0.02	0.55	0.07	0	0	0	0.11	0				2.18
March	3	0	0	0.1	0.89	0.1	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0	0	0	0	0	0	0.01	0	0	0	1.86	0	0	2.97
April	4	0	0	0.18	0.01	0	0	0	0.01	0	0	0.26	0.01	0	0.52	0	0	0	0.22	0.95	0	0	0.43	0	0	0	0	0.76	0.05	0			3.4
May	5	0.03	0	0	0	1.04	0	0	0	0.04	1.41	0.02	0	0.17	0.06	0	0	0.79	2.03	0.32	0	0	0	0.15	0.47	0	0.14	0	0	0	0.12	0	6.79
June	6	0.61	0.03	0	0	0.25	0	0	0.05	0	0.06	0.25	0.01	0.02	0	0.34	0.06	0	0	0.29	1.45	2.32	0	0	0	0.08	0	0	0	0	0		5.82
July	7	0	0.12	0.3	0.59	0.06	0	0	0	0.01	0.63	0	0	0	0	0.31	0.03	0	0	2.59	1.1	0	0	1.74	0.38	0.05	0.23	2.43	0.14	0	0	0	10.71
August	8	0	0.18	0.02	0	0.05	0	0	0	0	0	0	0	0	0	0.75	0	0	0	0	0	0	0	0	0	0.19	0.85	0.05	0	0	0.04	1.18	3.31
September	9	0.13	0	0	0	0	0	0.5	0	0	0	0	0	0	0.2	0.1	0.1	0	0	0	0	0	0	0	0	0	0.14	0	0	0	0		1.17
October	10	0	0	0	0.01	0.77	0	0	0	0.14	0	0	0.02	0.15	0.44	0.01	0.81	0.44	0	0	0	0.01	0.97	0	0	0.04	0	0	0	0	0	0	3.81
November	11	0.53	0.11	0.03	0.04	0.05	0	0	0.03	0.25	0	0	0	0	0	0.34	0	0	0	0.07	0	0	0	0.07	0	0	0.18	0	0	0	1.01		2.71
December	12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.35	0.11	0	0	0	0.01	1.31	0	0	0	0	0.03	0.2	0	0	0	2.01
1982 Totals	**1982**	**0.37**	**4.94**	**4.48**	**4.67**	**1.11**	**1.17**	**0.85**	**4.84**	**0.36**	**4.09**	**0.09**	**1.26**	**0.82**	**2.44**	**1.32**	**1.15**	**1.25**	**0.92**	**0.83**	**1.14**	**0.25**	**0.63**	**1.79**	**1.36**	**0.73**	**3.2**	**1.85**	**1.86**	**1.01**	**2.87**	**1.32**	**54.97**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0	0.82	0.45	0	0	0	0	0	0.04	0	0	0.16	0.02	0.01	0.01	0	0	0	0	0.03	0	0.59	0	0	0	0	0	0	0.21	1.92	0.64	4.9
Feburary	2	0	0	0.23	0	0.02	0	0	0.43	0	0	0	0.09	0	0	0	0.56	0	0.03	0	0.01	0	0	0	0	0	0	0	0				1.37
March	3	0	0	0.06	0.2	0	0.04	0	0	0.1	0	0	0.46	0	0.88	0	0	0	0.02	0	0	0	0	0	0.19	0.64	0	0	0	0	0.29	0	2.88
April	4	0	0.4	0	0	0.31	0	0.24	0.14	0	0	0	0	0	0	0.27	0.47	0	0	0.24	0	0	0	0	0	0.07	0.41	0	0	0	0		2.55
May	5	0	0	0	0	0	0.35	0.09	0	0	0	0	0	0	0.16	0	0	0	0	0	0.04	0.11	0	0	0	0	0.04	1.02	1.4	0.8	0.54	0.3	4.85
June	6	0	0	0	1.32	0	0	0.44	1.66	0.22	0	0.01	0	0	0	0.51	0.12	0	0.77	0.03	0.04	0	0.03	0	0	0	0.81	0	0	0	0		5.96
July	7	0.12	0.82	0.51	3.03	0	0	0.02	0	0	3.37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0.03	0	0	0	0	7.91
August	8	0	0	0	0	0	0.33	0.04	2.2	0	0.48	0	0	0	0	0.49	0	0	0	0	0	0	0	0.14	0.05	0	1.1	0.02	0	0	0.12	0.3	5.27
September	9	0.25	1.41	0	0	0	0	0.02	0	0	0	0	0.02	0.8	1.39	0.04	0	1.25	0	0	0	0	0	0.09	0	0	0	0	0	0	0		5.27
October	10	0	0	0.5	0	0	0.45	0	0.41	0	0	0	0	0	0	0	0	0	0	0.53	0	0	0	0	0	0	0	0	0.33	0	0	0.08	2.3
November	11	0	0.02	0	0	0	0	0	0	0	0	0.08	0.53	0	0	0	0	0	0	0.1	0.03	1.02	0.14	0.01	0.6	0	0.02	0.77	0.44	0.13	0	0	3.89
December	12	0	1.47	2.73	0.12	0.78	0	0	0	0	0.24	0	0	0	0	0	0	0	0	0	0	0	0	0	0.96	1.12	0	0.06	0.34	0	0	0	7.82
1983 Totals	**1983**	**3.02**	**3.74**	**2.53**	**0.32**	**1.56**	**0.5**	**0.31**	**0.66**	**0.95**	**1.59**	**0.84**	**1.12**	**2.23**	**0.71**	**0.16**	**0.04**	**0.78**	**1.17**	**3.66**	**3.37**	**3**	**3.14**	**1.57**	**0.3**	**1.13**	**0.73**	**3.19**	**1.09**	**0.66**	**0.73**	**0**	**44.8**
January	1	0	0	0	0	0	0	0.09	0.05	0	0.02	0	0	0	0	0	0	0	0	0	0	0.21	0.21	0.02	0	0	0	0	0	0.12	0	0	0.72
Feburary	2	0.4	0.51	0	0	0	0.03	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0	0	0	0	0	0	0	0	0				0.95
March	3	0	0	0	0	0.64	0.19	0.16	0	0.04	0	0	0	0	0	0	0	0.06	0.91	0.21	0.64	0.02	0	0	0	0	0.48	0.04	0	0.04	0.11	0	3.54
April	4	1.19	0.29	0.01	0.02	0.5	0.07	0	0.61	0.24	0.11	0	0.16	0.92	0	0	0	0.21	0.03	0	0	0	0.14	0	0	0	0	0.91	0.8	0.5	0.59		7.3
May	5	1.43	0	0.01	0	0	0	0.06	0	0	0	0.04	0.17	1.15	0.5	0	0	0	0.2	0	0	1.82	0.67	0	0	0	0	0.22	0.02	0	0.03	0	6.32
June	6	0	1.81	1.04	0	0.41	0	0	0	0	0	0	0	0	0.07	0	0	0	0	0.5	0.15	0	0	0	0	0	0.25	0.05	0.04	0	0		4.32
July	7	0	0	0	0.16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.3	0.77	0	0	0	0	0	0	1.23
August	8	0	0	0	0	0	0.2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.01	0.03	0	0	0	0	0	0	0	0	2.24
September	9	0	0	0	0	0	0	0	0	0	0	0.07	0.43	0	0	0.13	0	0	0	0	0.25	0	0	0	0	0.36	0	0	0	0	0		1.24
October	10	0	0	0	0.13	0	0	0	0	0	0	0.28	0.32	0	0	0	0.03	0.51	0	1.49	2.08	0.54	0	0.02	0	0	0	0	0	0	0	0	5.4
November	11	0	0.92	0.74	0	0	0	0	0	0.67	0.14	0	0.04	0	0	0	0	0	0	1.46	0.24	0	0.11	1.5	0	0	0	1.94	0.03	0	0		7.79
December	12	0	0.21	0.73	0.01	0.01	0.01	0	0	0	1.32	0.45	0	0.16	0.14	0.03	0	0	0.03	0	0.01	0.41	0	0	0	0	0	0.03	0.2	0	0	0	3.75
1984 Totals	**1984**	**1.72**	**1.89**	**2.39**	**1.47**	**0.79**	**0.7**	**0.74**	**5.47**	**1.56**	**3.46**	**0.6**	**1.11**	**1.34**	**0.45**	**1.11**	**0.46**	**0.88**	**2.38**	**1.32**	**2.92**	**2.09**	**1.98**	**2.27**	**0.96**	**2.14**	**2.54**	**2.35**	**0.66**	**2.09**	**0.12**	**1.69**	**51.65**
January	1	0	0	0	0	0	0	0	0	0.46	0	0	0	0	0	0.08	0.01	0.04	0.09	0	0	0	0	0.14	0	0	0	0	0.01	0	0.01	0	0.84
Feburary	2	0	0.07	0	0	0.11	0	0	0	0.34	0.22	0	0.45	0	0	0	0.16	0	0.35	0	0	0	0	0	0	0.16	1.2	0.35	0.02	0			3.43
March	3	0	0	0	0.76	0	0	0.04	0.05	0.01	0.02	0	0.51	0	0	0.47	0	0.28	0.4	0.86	0	0	0	0	0.91	0.01	0.35	0.08	0.62	0	0	0	5.37
April	4	0	0.5	2.08	0	0	0	0.26	0.49	0.03	0	0	0.08	0	0.08	0.05	0.06	0	0	0	0.35	1.75	0.07	0.01	0	0	0	0	0	0.48	0		6.29
May	5	0	0	0	0.11	0.38	0.18	0.25	0	0	0	0	0	0.46	0	0	0	0	0	0.25	0.85	0.09	0.22	0	0	1.4	0	0.99	0.01	0	0	0	5.19
June	6	0	0	0	0.07	0	0.15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.06	0.07	2.11	0	0	0	0.28	0	0	0		2.74
July	7	0	0	0.04	0.47	0	0	0	0.01	0	0	0.08	0	0	0	0.12	0	0	0	0	0	0	0	0	0	0	0.04	0	0	0	0	0	0.76
August	8	0	0	0.27	0.06	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0.2	0	0	0	0.1	0	0	0	0	0	0	0	0	0	0.64
September	9	0	1.24	0	0	0.12	0.03	0	2.58	0	2.89	0.1	0	0.04	0.21	0	0	0	0	0	0	0	1.52	0.01	0	0.05	0	0.09	0	0	0		8.88
October	10	0	0	0	0	0	0.34	0.19	2.16	0	0.06	0.33	0.07	0.38	0.15	0.27	0.15	0	0.95	0.01	1.22	0.01	0	0	0.05	0.52	0	0	0	0.18	0.08	0	7.12
November	11	1.72	0	0	0	0	0	0	0.18	0.72	0.27	0.02	0	0	0.01	0.12	0	0.55	0.39	0.01	0	0	0	0	0	0	0.95	0.56	0	0	0		5.5
December	12	0	0.08	0	0	0.18	0	0	0	0	0	0.07	0	0.46	0	0	0.08	0	0	0.19	0.5	0.18	0	0	0	0	0	0	0	1.43	0.03	1.69	4.89
1985 Totals	**1985**	**2.57**	**1.02**	**0.51**	**3.19**	**1.59**	**1.39**	**0.52**	**0.01**	**0.88**	**3.62**	**3.5**	**0.3**	**3.13**	**1.75**	**1.67**	**0.06**	**0.85**	**3.47**	**2.14**	**0.21**	**1.77**	**1.33**	**3.05**	**1.05**	**2.9**	**0.45**	**1.15**	**0.01**	**2.47**	**1.2**	**2.97**	**50.73**
January	1	0.05	0	0	0	0	0	0	0	0.11	0.06	0	0	0	0	0	0.06	0	0	0.04	0	0	0	0	0	0	0	0	0	0.09	0.11	0.01	0.53
Feburary	2	0	0	0	0.02	0.06	0	0	0	0	0.49	0.04	0	0	0	0	0	0	0	0	0	1.16	0.25	1.52	0.07	0	0.16	0	0				3.77
March	3	0.11	0	0.1	0.66	0	0	0.32	0.01	0	0.13	0.22	0	0.43	0	0	0	0	0	0	0.12	0.03	0	0	0	0	0	0.25	0	1.93	0.82	0.05	5.18
April	4	0	0	0	0.03	1.31	0.09	0.2	0	0	0.5	0	0	0.19	0.27	0	0	0	0	0	0	0	0.04	0.95	0.02	0	0	0	0	0	0		3.6
May	5	1.29	0.07	0	0	0	0.02	0	0	0	0	0	0	1.7	0.16	0	0	0.02	0	0	0	0	0	0	0	0	0	0.03	0	0	0.01	0	3.3
June	6	0.08	0.95	0.32	2.07	0.22	1.02	0	0	0.03	0.73	1.83	0.15	0	0.15	0.12	0	0.83	0	0	0	0.05	0.19	0.15	0.36	0	0	0	0	0	0.18		9.43
July	7	0	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0	0	0	0	0	0	0	0.22	0.28	0	0	2.63	0	0	0	0	0	2.09	5.23
August	8	0.06	0	0.09	0.37	0	0.06	0	0	0	0.09	0	0	0.53	0.25	0.12	0	0	0	0.79	0	0.13	0.48	0.21	0.44	0	0	0	0	0	0.04	0	0	3.66
September	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.09	0.17	0	0.09	0	0	0	0	0.07	0.01		0.43
October	10	0	0	0	0.04	0	0	0	0	0	0	0.29	0.03	0.03	0.01	0	0	0	0.32	0	0.08	0	0	0	0	0	0	0	0	0	0.34	0	0.82	1.96
November	11	0.6	0	0	0	0	0.2	0	0	0.02	0.47	0	0.12	0.06	0.91	1.43	0	0	3.15	1.18	0	0.18	0	0.05	0.16	0.18	0.29	0.87	0.01	0	0.07		9.95
December	12	0.38	0	0	0	0	0	0	0	0.72	1.15	1.11	0	0.19	0	0	0	0	0	0	0.13	0.01	0	0	0	0	0	0	0	0	0	0	0	3.69
1986 Totals	**1986**	**4.33**	**1.49**	**4.28**	**0.5**	**1.32**	**1.95**	**0.94**	**1.12**	**0.86**	**0.29**	**1.85**	**0.64**	**0.27**	**1.31**	**1.07**	**0.45**	**0.45**	**1.42**	**0.17**	**0.47**	**0.19**	**0.28**	**0.37**	**1**	**1.47**	**0.65**	**1.3**	**0.42**	**1.22**	**2.76**	**0.04**	**34.88**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0	0.09	0	0	0	0.1
Feburary	2	1.3	1.02	1.57	0.04	0	0.26	0	0	0	0	0	0	0	0.46	0	0	0	0	0	0	0.01	0	0.02	0	0	0	0	0				4.68
March	3	0	0	0	0	0.1	0	0.01	0	0	0.02	0.24	0.39	0	0	0	0	0	0.39	0	0	0	0	0	0	0	0.07	0	0	0	0	0	1.22
April	4	0.07	0	0.01	0	0	0.01	0.11	0	0	0	0	0	0	0.15	0.04	0.02	0	0.01	0	0.45	0.18	0	0	0	0	0	0.02	0.11	0	0.05		1.23
May	5	0.16	0	0	0	0	0	0	0.11	0.01	0.02	0.07	0	0.01	0.12	0.4	0.41	0.01	0.01	0	0	0	0	0	0.51	0.36	0	0	0.22	0	0	0	2.42
June	6	0.04	0	0	0.1	1.1	0.55	0	0.82	0.73	0	0.06	0.01	0	0.2	0.26	0	0	0	0	0	0	0.02	0	0	0	0	0.18	0	0	0.36		4.43
July	7	1.4	0.12	0	0	0	0	0	0	0	0.08	0.23	0.07	0.2	0.38	0.01	0	0	0	0	0	0	0	0	0	0	0.01	0	0	0.07	0	0.04	2.61
August	8	0	0	0	0	0.04	1.13	0.25	0	0.03	0.13	0	0	0	0	0.36	0.02	0	0	0	0	0	0	0	0	0	0.18	0.08	0	0	0	0	2.22
September	9	0	0	0.01	0.06	0	0	0.09	0	0	0	1.22	0	0	0	0	0	0.41	1.01	0	0	0	0.25	0.2	0.02	0	0.2	1.02	0	1.15	2.35		7.99
October	10	0.7	0.3	2.67	0	0	0	0	0	0	0	0	0.17	0.06	0	0	0	0	0	0	0	0	0.01	0.15	0.47	0.63	0.18	0	0	0	0	0	5.34
November	11	0	0	0.02	0.3	0.08	0	0.36	0.08	0	0.04	0.03	0	0	0	0	0	0	0	0.17	0.02	0	0	0	0	0.48	0	0	0	0	0	0	1.58
December	12	0.66	0.05	0	0	0	0	0.12	0.11	0.09	0	0	0	0	0	0	0	0.03	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.06
1987 Totals	**1987**	**0.74**	**1.02**	**3.03**	**0.39**	**0.44**	**3.36**	**1.24**	**2.13**	**1.14**	**1.19**	**0.04**	**0.2**	**2.15**	**1.88**	**0.35**	**2.01**	**0.6**	**1.08**	**3.35**	**0.91**	**0.13**	**0.48**	**0.13**	**2.92**	**0.96**	**1.12**	**2.4**	**1.92**	**0.84**	**0.23**	**0**	**38.38**
January	1	0.14	0	0	0	0	0	0	0	0.88	0.03	0	0	0	0	0	0	0.31	0.06	0.46	0	0	0.03	0.07	0	0	0	0	0	0	0	0	1.98
Feburary	2	0.08	0	0	0	0	0	0	0	0	0	0	0	0	0	0.42	0	0	0	0	0	0	0	0	0	0	0.24	0.03	0.63				1.4
March	3	0.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0.06	0	0.23	0.95	0	0	0	0.33	0	0.33	0	0	0	0.01	0.15	0	0	2.16
April	4	0	0	0	0	0	0	0	0	0	0.31	0	0	1.2	0.09	0.03	0	0	0	0	0	0.07	0.01	0.03	0	0	0	0	0	0	0		1.74
May	5	0	0	1.64	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0.05	0	0.22	0	0.06	0	0	0	0	0	0	0	0	0.02	0	2
June	6	0	1.02	0	0	0	0	0	0	0.07	0.02	0.03	0.17	0	0	0	0.09	0	0	1.09	0.43	0	0.11	0	0	0	0	0	0	0.35	0.21		3.59
July	7	0.4	0	0	0.36	0.44	3.1	0.32	0	0	0	0	0.03	0.39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5.04
August	8	0	0	1.38	0.02	0	0	0	1.84	0.18	0	0	0	0.56	0	0.01	0.02	0	0	0	0.47	0	0	0	0	0	0.77	0.31	0	0	0	0	5.56
September	9	0	0	0	0	0	0	0.05	0.11	0	0.02	0	0	0	0.01	0	0.29	0	0.02	0	0	0	0	0	0	0	0	0	0.89	0.23	0		1.62
October	10	0	0	0	0	0	0.03	0	0	0.01	0.81	0	0	0	0	0	0.27	0	0	0.21	0.01	0	0	0.03	0.34	0	0.03	0	0	0	0	0	1.74
November	11	0.01	0	0	0	0	0.06	0.06	0.14	0	0	0	0	0	0	0.01	0.92	0.01	0	0	0	0	0	0	1.73	0.2	0.08	0.4	0.36	0.11	0		4.09
December	12	0.01	0	0.01	0	0	0.17	0.81	0.04	0	0	0.01	0	0	1.78	0.24	0	0	0.05	1.37	0	0	0	0	0.52	0.76	0	1.66	0.03	0	0	0	7.46
1988 Totals	**1988**	**1.44**	**1.07**	**1.3**	**0.87**	**0.4**	**0.13**	**0.12**	**1.92**	**0.76**	**0.26**	**0.46**	**0.95**	**0.03**	**0.15**	**1.18**	**0.14**	**1**	**0.93**	**4.12**	**3.25**	**0.05**	**2.62**	**1.59**	**0.43**	**1.14**	**1.37**	**1.08**	**0**	**2.13**	**1.31**	**1.73**	**33.93**
January	1	0	0	0	0	0	0	0.06	0	0	0	0	0	0	0	0	0.01	0.24	0	1.36	0	0	0	0	0	0.01	0	0	0	0	0	1.62	3.3
Feburary	2	0.89	0.02	0.2	0	0	0	0	0	0	0.26	0.06	0.04	0	0.13	0	0	0	0.11	0.56	0	0	0	0	0	0	0	0	0	0			2.27
March	3	0	0.89	1.06	0.15	0	0	0	0.11	0	0	0.35	0	0	0	0	0	0.07	0.07	0	0	0	0	0	0.38	0	0.07	0	0	1.58	0	0	4.73
April	4	0.07	0.16	0	0	0.33	0.13	0	0	0	0	0	0	0	0	0	0	0.23	0.23	0	0	0	0	0	0	0	0	0	0	0	0		1.15
May	5	0	0	0.04	0.07	0	0	0	0.55	0	0	0	0	0	0	0	0	0	0	0	0	0	0.17	0.61	0	0	0	0	0	0	0	0	1.44
June	6	0	0	0	0	0	0	0	1.26	0	0	0	0	0	0	0	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0.5	0.2		1.97
July	7	0	0	0	0	0	0	0	0	0	0	0.05	0	0	0	0	0	0	0.26	0.02	1.75	0	0	0	0	0.8	0	0	0	0.05	0.09	0	3.02
August	8	0	0	0	0	0	0	0	0	0	0	0	0.18	0.03	0.02	0	0	0	0.01	0.65	0.02	0	0.86	0.5	0	0	0	0.04	0	0	0	0	2.31
September	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0	0.07	0.83	0	0	0	0.05	0.01	0	0	0	0	0	1.02		1.99
October	10	0.48	0	0	0	0	0	0	0	0.02	0	0	0	0	0	0	0.11	0.46	0	0	0.18	0.05	0.13	0.32	0	0	0	0.11	0	0	0	0	1.86
November	11	0	0	0	0.65	0.07	0	0	0	0.74	0	0	0.73	0	0	1.18	0	0	0	0.18	0.7	1.3	0	0	0	0	0.33	0.77	0	0	0	0	6.65
December	12	0	0	0	0	0	0	0.06	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.46	0.11	0.04	0	0.53	0.93	0	0	0	0.11	3.24
1989 Totals	**1989**	**1.03**	**1.29**	**0.78**	**0.61**	**1.84**	**0.97**	**0.57**	**0.25**	**0.36**	**0**	**0.18**	**0.14**	**0.8**	**0.58**	**0.75**	**0.64**	**0.54**	**1.07**	**1.01**	**4.04**	**0.39**	**0.42**	**1.37**	**0.84**	**1.11**	**0.66**	**0.71**	**2.55**	**1.64**	**1.46**	**0**	**28.6**
January	1	0	0	0	0	1.27	0.01	0.41	0	0	0	0.05	0	0	0.06	0	0	0	0	0	0	0	0	0	0	0.44	0.24	0	0.08	0.02	0	0	2.58
Feburary	2	0	0.3	0.07	0.08	0.04	0.04	0	0	0	0	0	0.05	0.14	0.18	0.2	0	0	0	0	0.29	0.04	0	0	0	0	0	0	0				1.43
March	3	0	0	0.04	0.14	0.23	0.56	0	0	0	0	0	0	0.04	0	0	0	0.46	0	0.23	2.02	0	0	0	0	0	0	0	0.2	0.01	0.6	0	4.53
April	4	0	0.95	0.67	0	0	0	0.14	0	0	0	0	0	0	0.01	0.01	0	0	0.02	0	0	0	0	0	0	0	0	0	0.26	0.03	0.01		2.1
May	5	0	0	0	0.13	0	0	0	0.04	0.22	0	0	0	0	0	0	0	0	0.01	0.73	0	0.05	0.34	0	0	0.61	0.03	0	1.95	0	0	0	4.11
June	6	0.04	0	0	0.26	0.04	0	0	0	0	0	0.13	0.08	0	0	0	0	0.05	0.97	0	0	0	0	0	0	0	0.39	0.38	0	0	0		2.34
July	7	0.34	0.04	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.02	0.03	1.62	0.06	0.08	0.28	0.17	0.01	0	0	0	1.43	0.51	0	4.59
August	8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.59	0	0	0.01	0.11	0.23	0	1.09	0.67	0.01	0	0.23	0.06	0	0	0	3
September	9	0.65	0	0	0	0	0	0	0.1	0.14	0	0	0.01	0.58	0.13	0.08	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		1.69
October	10	0	0	0	0	0.26	0.26	0	0	0	0	0	0	0	0	0	0.05	0.03	0	0	0	0	0	0	0	0.04	0	0	0	0	0.31	0	0.95
November	11	0	0	0	0	0	0.02	0.02	0.11	0	0	0	0	0	0.05	0.39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		0.59
December	12	0	0	0	0	0	0.08	0	0	0	0	0	0	0.04	0.15	0.07	0	0	0.05	0.01	0	0.01	0	0	0	0	0	0.1	0	0.15	0.03	0	0.69
1990 Totals	**1990**	**1.27**	**0.85**	**4**	**2.39**	**0.23**	**1.03**	**3.15**	**1.21**	**1.01**	**1.02**	**1.36**	**1.43**	**0.63**	**1.03**	**2.6**	**3.32**	**1.52**	**0.58**	**1.19**	**2.42**	**2.54**	**1.78**	**0.48**	**0.45**	**0.85**	**0.72**	**2.3**	**0.98**	**1.78**	**0.97**	**0**	**45.09**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0.01	0	0.16	0	0	0	0	0	0	0	0	0	0	0	0	0	0.33	0	0.59	0.04	0	0	0	0.06	0.23	0	0	0	0	0	0	1.42
Feburary	2	0.95	0.01	0.13	0.42	0	0.07	0	0	0.07	0	0	0	0	0.51	0.42	0	0	0	0	0	0.11	0.73	0.04	0	0	0	0.07	0				3.53
March	3	0	0	0	0	0	0.09	0.14	0.19	0	0	0.17	0.01	0	0.44	0.07	0	0	0	0	0	0	0.18	0.32	0.33	0	0	0	0.39	0.12	0.21	0	2.66
April	4	0.31	0	0	0	0	0	0	0	0.01	0.83	0	0	0.59	0	0.03	0.01	0.04	0	0.04	0.46	0	0	0.02	0	0	0	0.54	0.19	0	0		3.07
May	5	0	0	1.11	0.13	0	0.02	0	0	0.17	0	0.26	1.21	0	0	1.91	2.8	0	0	0.53	0	0	0	0	0.06	0.62	0.3	0.08	0.39	0	0	0	9.59
June	6	0	0.1	0	0	0	0.84	1.27	0	0.06	0	0	0	0	0.01	0	0	0.05	0	0	0.58	0	0.09	0	0	0	0	0	0	0.01	0.01		3.02
July	7	0	0	0	0	0.14	0	0	0	0	0.09	0.93	0.03	0.04	0.03	0.03	0	0	0	0.03	1.11	0.54	0.37	0	0	0	0	0	0	0	0	0	3.34
August	8	0	0	1.3	0.49	0	0	0	0	0	0	0	0.18	0	0	0.13	0.51	0	0	0	0.23	0	0	0	0	0	0	0	0	0	0	0	2.84
September	9	0	0	0	0	0	0	0	0.01	0	0	0	0	0	0	0	0	0	0.45	0	0	0.32	0	0	0	0	0	0	0	0	0		0.78
October	10	0	0	0.93	0	0	0.01	1.74	1.01	0.69	0.1	0	0	0	0	0.01	0	0.44	0	0	0	0.03	0	0	0	0	0	0	0	0	0	0	4.96
November	11	0	0	0	1.35	0.09	0	0	0	0.01	0	0	0	0	0	0	0	0	0.03	0	0	0.2	0	0	0	0	0.42	1.26	0	0	0		3.36
December	12	0	0.74	0.37	0	0	0	0	0	0	0	0	0	0	0.04	0	0	0.66	0.1	0	0	1.34	0.41	0.1	0	0	0	0.35	0.01	1.65	0.75	0	6.52
1991 Totals	**1991**	**1.38**	**1.62**	**1.62**	**2.01**	**1.08**	**0.36**	**0.36**	**0.11**	**0.94**	**1.11**	**2.88**	**1.63**	**1.1**	**0.65**	**0.78**	**1.12**	**2.05**	**1.38**	**0.87**	**1.08**	**0.86**	**1.63**	**1.37**	**0.23**	**0.55**	**0.71**	**0.07**	**0.77**	**2.74**	**0.4**	**0.02**	**33.48**
January	1	0	0	0	0	0.32	0.03	0	0	0	0.36	0.3	0	0	0	0.22	0.04	0	0	0	0.04	0	0	0	0	0.02	0.01	0	0	0.17	0.01	0	1.52
Feburary	2	0	0	0	0	0	0.05	0.01	0	0	0	0	0	0.47	0	0	0	0.01	0.44	0	0	0	0	0	0	0	0	0	0				0.98
March	3	0.32	0	0	0	0	0.05	0	0	0	0	0	0.5	0.07	0.1	0	0	1.14	0	0	0	0.84	0.16	0	0	0	0	0.02	0	0	0	0	3.2
April	4	0	0	0.05	0.36	0	0	0.26	0	0	0	0.03	0.69	0.56	0.51	0.07	0	0	0.23	0.28	0.01	0	0	0.01	0	0.03	0	0	0.18	0	0		3.27
May	5	0.27	0	0.54	0	0.69	0	0	0	0	0.01	0.08	0	0	0	0	0.22	0	0.32	0	0	0	0	0	0	0.5	0.02	0	0	1.22	0	0	3.87
June	6	0	0	0	0.01	0	0	0	0	0	0	0	0	0	0	0.39	0.02	0	0	0	0	0.01	0	0	0	0	0	0	0	0.01	0		0.44
July	7	0	0.82	0.1	0	0	0	0	0	0.94	0.74	2.47	0	0	0	0	0	0	0	0	0	0	0	0	0.02	0	0	0	0.02	0.07	0	0	5.18
August	8	0	0	0	0.13	0.05	0.03	0	0.11	0	0	0	0	0	0	0	0	0.36	0	0	0	0	0	0	0	0	0	0	0.08	0.22	0	0	0.98
September	9	0	0.01	0.74	0	0	0	0	0	0	0	0	0	0	0	0	0.82	0	0.23	0	0	0.01	1.12	0	0.05	0	0	0	0	0	0		2.98
October	10	0	0.32	0.19	1.51	0.02	0	0	0	0	0	0	0	0	0	0	0	0	0.16	0	0	0	0	1.28	0.16	0	0.64	0	0.4	0.61	0.39	0.02	5.7
November	11	0.76	0	0	0	0	0.2	0.09	0	0	0	0	0.06	0	0.04	0.1	0.02	0.54	0	0.59	0.34	0	0	0	0	0	0.04	0.05	0	0.43	0		3.26
December	12	0.03	0.47	0	0	0	0	0	0	0	0	0	0.38	0	0	0	0	0	0	0	0.69	0	0.35	0.08	0	0	0	0	0.09	0.01	0	0	2.1
1992 Totals	**1992**	**0.49**	**2.26**	**1.03**	**0**	**0.09**	**0.09**	**1.25**	**0.51**	**1.65**	**0.88**	**1.8**	**1.49**	**0.49**	**1.61**	**3.59**	**0.11**	**0.89**	**1.5**	**1.44**	**3**	**0.26**	**1.5**	**1.02**	**0.23**	**0.34**	**2.12**	**1.12**	**0.07**	**1.22**	**0.96**	**0.48**	**33.49**
January	1	0	0.02	0	0	0	0	0.03	0.47	0	0	0	0.03	0.38	0.04	0.03	0	0	0	0	0	0	0.1	0.02	0	0	0	0	0	0	0	0	1.12
Feburary	2	0	0	0	0	0	0	0	0	0	0	0	0.37	0	0.79	0	0	0.45	0	0	0	0	0	0.06	0.22	0	0	0	0				1.89
March	3	0	0	0	0	0.04	0.07	0	0	0.07	0.1	0	0	0.11	0	0	0	0	0.94	0.34	0	0.13	0.02	0	0	0.18	0	0	0.02	0.83	0.56	0.04	3.45
April	4	0	0	0	0	0	0	0	0	0.12	0.06	0	0	0	0	0.23	0.05	0.28	0.42	0.76	0.4	0	0	0.03	0	0.04	0	0	0	0.07	0		2.46
May	5	0	0	0	0	0	0	0	0	0	0	0.27	0.19	0	0.12	0	0.02	0.02	0.09	0	0.49	0.01	0.19	0.01	0	0	0.04	0	0	0	0	0	1.45
June	6	0	0	0.32	0	0	0	0	0	0	0	0	0	0	0	0.24	0	0	0	0.08	0.05	0	0	0.5	0	0	0	0	0	0	0		1.19
July	7	0	2.09	0.16	0	0.05	0	0.03	0	0	0.04	0	0	0	0.62	0	0.04	0.12	0	0	0.66	0.06	0	0.4	0	0	0	0	0	0	0.04	0	4.31
August	8	0	0	0	0	0	0	0.24	0	0	0.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.76	1.12	0	0	0	0.23	3.45
September	9	0.11	0.11	0	0	0	0	0.95	0.02	1.02	0	0	0	0	0	0	0	0	0.04	0	0.34	0.06	0	0	0	0.01	0.32	0	0	0	0		2.98
October	10	0	0	0	0	0	0	0	0.01	0	0	0	0	0	0	0.33	0	0	0	0.09	0.15	0	0	0	0	0	0	0	0	0.16	0.33	0.14	1.21
November	11	0.37	0.04	0.55	0	0	0	0	0.01	0.09	0.58	1.53	0.9	0	0	0	0	0.02	0.01	0	0.91	0	1.19	0	0.01	0.11	0	0	0	0	0		6.32
December	12	0.01	0	0	0	0	0.02	0	0	0.35	0	0	0	0	0.04	2.76	0	0	0	0.17	0	0	0	0	0	0	0	0	0.05	0.16	0.03	0.07	3.66
1993 Totals	**1993**	**0.35**	**2.74**	**1.78**	**1.62**	**0.22**	**2.88**	**0.47**	**0.32**	**0.57**	**1.49**	**4.46**	**4.3**	**2.88**	**4.71**	**2.22**	**2.75**	**0.55**	**0.5**	**2.16**	**2.58**	**0.27**	**3.61**	**1.81**	**2.86**	**3.33**	**0.74**	**0.06**	**1.12**	**0.2**	**0.65**	**0.56**	**54.76**
January	1	0	0.04	0.51	1.29	0	0	0	0	0.39	0.02	0	0.18	0	0	0	0	0	0.03	0	0.95	0.08	0	0.05	0	0	0	0	0	0	0	0	3.54
Feburary	2	0	0	0	0	0	0	0	0	0	0	0.55	0.05	0.01	0	0.5	0.16	0	0	0	0.13	0.19	0	0	0.17	0.99	0	0	0				2.75
March	3	0	0.34	0.58	0.24	0	0	0	0	0	0	0	0.04	0.01	0	0.04	0.19	0	0	0.47	0	0	0.94	0	0	0.01	0	0	0	0	0.29	0.16	3.31
April	4	0.1	0	0.08	0.02	0	0	0.05	0.11	0	0	0	1.18	0.78	0.66	0.54	0.06	0	0	0.65	0.03	0	0	0	1.36	0.34	0	0	0	0.2	0		6.16
May	5	0.08	0.11	0.08	0.02	0	0.89	0	0	0	0.46	0.17	1.04	0	0	0	0.14	0.3	0.45	0	0	0	0.09	0	0	0	0	0	0	0	0.11	0	3.94
June	6	0	0.07	0.01	0.02	0	1.47	0	0.13	0	0.26	1.51	0	0	0	0	0	0	0	0.33	0	0	0	0	1.05	0.9	0	0	1.12	0	0.25		7.12
July	7	0.16	0	0	0	0.02	0.52	0.42	0	0.16	0	0	0	0.71	0.04	1.14	0.1	0	0	0	0.37	0	0.8	0.16	0.03	0.03	0	0	0	0	0	0.4	5.06
August	8	0	0	0.05	0	0.2	0	0	0	0	0.75	2.16	1.01	0	0	0	0	0	0	0	0	0	0.01	0.51	0.09	0	0	0	0	0	0	0	4.78
September	9	0	1.56	0.24	0	0	0	0	0.01	0	0	0	0	0.76	1.8	0	0	0	0	0.71	0	0	1.77	1.09	0.04	0.73	0.45	0	0	0	0		9.16
October	10	0	0	0	0	0	0	0	0.07	0.02	0	0.07	0	0	0	0	1.33	0	0.02	0	1.1	0	0	0	0	0	0	0	0	0	0	0	2.61
November	11	0	0.07	0	0	0	0	0	0	0	0	0	0.8	0.41	1.86	0	0.77	0.24	0	0	0	0	0	0	0.02	0.33	0.29	0.06	0	0	0		4.85
December	12	0.01	0.55	0.23	0.03	0	0	0	0	0	0	0	0	0.2	0.35	0	0	0.01	0	0	0	0	0	0	0.1	0	0	0	0	0	0	0	1.48
1994 Totals	**1994**	**0.84**	**0.79**	**0.45**	**1.45**	**1.59**	**0.53**	**0.78**	**2.09**	**0.99**	**1.76**	**2.53**	**0.62**	**1.09**	**1**	**0.74**	**1.1**	**0.05**	**0.81**	**0.42**	**2.2**	**0.59**	**1.07**	**0.76**	**0.4**	**1.14**	**1.6**	**1.38**	**3.34**	**0.18**	**1.71**	**0.7**	**34.7**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0.06	0	0.08	0.02	0	0.06	0	0	0	0.18	0	0	0.04	0	0	0.6	0	0	0	0	0	0	0	0.01	0.31	0.07	0.65	0	0	0	0.01	2.09
Feburary	2	0	0	0.04	0	0	0	0	0.12	0	0	0	0	0	0	0	0	0	0	0.2	0.12	0	0.79	0.13	0	0	0	0	0.11				1.51
March	3	0.08	0	0	0	0	0	0.22	0	0	0	0	0	0.15	0	0	0	0	0.02	0	0	0	0	0.01	0	0	0.75	0	0	0.04	0	0	1.27
April	4	0	0.13	0.08	0	0.34	0.19	0	0	0.46	1.58	2.1	0.5	0	0	0.74	0	0	0	0	0	0.09	0	0	0	0	0.29	0.19	2.96	0.14	0.53		10.32
May	5	0	0	0	0	0	0.2	0.5	0	0	0	0.43	0	0	0.23	0	0	0	0	0	0	0	0	0	0.09	0.13	0	0	0	0	0.14	0	1.72
June	6	0	0.63	0.13	0	0	0	0.01	0	0	0	0	0.05	0	0	0	0	0	0	0	0	0	0	0.56	0.02	0.58	0.18	0	0	0	0		2.16
July	7	0	0.01	0	0	0	0	0.02	0.84	0	0	0	0	0	0.02	0	0.01	0	0	0	0.52	0	0	0	0	0	0	0	0	0	0	0	1.42
August	8	0.7	0.02	0	0.53	0	0	0	0.06	0	0	0	0	0.66	0.2	0	0	0	0	0	0.25	0	0	0	0	0	0	0	0.27	0	1.04	0.03	3.76
September	9	0	0	0	0.06	0.18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0.28	0	0.22	0.12	0.31	0	0	0	0		1.18
October	10	0	0	0	0	0	0	0	0.98	0	0	0	0.07	0.24	0.01	0	0	0.05	0.79	0	0	0.01	0	0.06	0.06	0	0	0	0	0	0	0.58	2.85
November	11	0	0	0.05	0.84	1.07	0	0	0	0.5	0	0	0	0	0.54	0	0	0	0	0.22	1.09	0.05	0	0	0	0	0	0.54	0	0	0		4.9
December	12	0	0	0.07	0	0	0.08	0.03	0.09	0.03	0	0	0	0	0	0	0.49	0	0	0	0.22	0.43	0	0	0	0	0	0	0	0	0	0.08	1.52
1995 Totals	**1995**	**2.31**	**1.75**	**1.35**	**0.54**	**0.13**	**2.38**	**1.95**	**1.04**	**0.08**	**1.37**	**0.43**	**0.23**	**2.33**	**0.67**	**0.15**	**6.24**	**4.5**	**1.73**	**3.25**	**1.52**	**0.04**	**0.2**	**0.86**	**0.44**	**1.13**	**2.55**	**1.3**	**0.25**	**0.58**	**0.35**	**0.03**	**41.68**
January	1	0.08	0	0	0	0	0.35	0	0	0	0	0	0.1	2.12	0.12	0	0	0.01	0.44	0.54	0	0	0	0.03	0	0	0	0.5	0.1	0	0	0	4.39
Feburary	2	0.02	0.08	0.74	0	0	0.02	0.04	0	0	0	0	0	0	0.05	0	0	0	0	0	0	0	0	0	0	0	0.34	0.02	0.02				1.33
March	3	0	0.04	0	0.08	0.12	0.47	1.67	0	0	0	0	0	0	0	0	0	0	0	0	0	0.16	0	0	0	0	0	0.65	0	0	0	0	3.19
April	4	0.12	0	0.12	0	0	0	0	0	0.02	0.02	0.33	0.02	0	0	0	0.46	0.08	0.1	0.05	0.73	0	0	0.6	0.01	0	0.09	0	0	0.58	0		3.33
May	5	0.7	0	0.21	0.13	0	0.01	0.02	0.71	0	0.06	0	0.1	0.19	0	0	5.59	3.95	0.24	0	0	0	0	0.15	0.38	0.18	0.01	0.29	0	0	0	0	12.92
June	6	0.6	0.09	0	0	0	0.06	0	0.17	0.06	0.28	0.05	0	0	0	0	0	0	0	0	0.05	0	0	0	0	0.07	0.91	0.49	0.13	0	0		2.96
July	7	0	0	0.15	0.12	0	0.13	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0.56	0	0.19	0.01	0.05	0.88	0.06	0	0	0	0	0	2.16
August	8	0.56	1.13	0	0.21	0	1.28	0.05	0	0	0	0	0	0	0.5	0.1	0.02	0	0	0.66	0	0	0	0	0	0	0	0	0	0	0	0.01	4.52
September	9	0	0	0	0	0	0	0.17	0.03	0	0	0	0	0	0	0	0.16	0	0	0.17	0	0.04	0	0	0	0	0	0	0	0	0.17		0.74
October	10	0	0.39	0.13	0	0	0	0	0	0	0.07	0	0	0.02	0	0	0	0	0	0.72	0.02	0	0	0.07	0	0	0.49	0	0	0	0.08	0.02	2.01
November	11	0.23	0.02	0	0	0.01	0.02	0	0	0	0.94	0.05	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		1.28
December	12	0	0	0	0	0	0.04	0	0.13	0	0	0	0	0	0	0.05	0	0.46	0.95	1.11	0	0	0.01	0	0	0	0	0	0	0	0.1	0	2.85
1996 Totals	**1996**	**2.04**	**0.88**	**0.01**	**1.03**	**1.09**	**2.96**	**1.55**	**0.46**	**1.12**	**0.44**	**0.25**	**0.07**	**0.37**	**1.85**	**0.85**	**0.51**	**1.29**	**1.26**	**0.85**	**0.34**	**1.46**	**2.7**	**4.15**	**1.97**	**1.51**	**1.27**	**2.06**	**6.53**	**1.37**	**0.48**	**0.95**	**43.67**
January	1	0.02	0.84	0	0.03	0.09	0.06	0	0	0	0	0.13	0	0	0	0	0	0.03	1.08	0	0.12	0	0.11	0.68	0.01	0	0.06	0	0	0	0.01	0	3.27
Feburary	2	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0.03	0.1	0	0	0	0	0	0	0	0	0	0	0.25	0.13	0	0			0.52
March	3	0	0	0	0	0.5	0.02	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0	0.06	0	0	0.46	0.9	0	0	0	0.04	0	0.12	0.95	3.06
April	4	0	0	0	0	0	0	0.01	0	0	0	0	0.01	0	0.48	0.03	0	0	0.01	0	0	0.49	1.77	0	0	0	0	0.11	4.46	0.35	0.25		7.97
May	5	0	0.04	0.01	0.79	0.17	0.03	0.39	0.04	0	0.04	0	0.04	0.01	0.73	0	0	0	0	0	0.11	0.16	0	0	0	0.45	0	1.33	0	0	0	0	4.34
June	6	0.44	0	0	0	0.11	0.58	0	0	1.11	0.4	0.12	0	0.36	0	0.44	0	0.16	0	0	0	0	0	0	0	0	0	0	0	0	0		3.72
July	7	1.48	0	0	0	0	0	0	0.24	0	0	0	0	0	0.61	0	0	0	0	0.85	0.02	0.21	0	0	0	0	0	0.22	2.03	0.66	0.01	0	6.33
August	8	0	0	0	0.01	0	0	0	0	0	0	0	0	0	0	0.02	0.06	0	0.17	0	0	0	0	1.3	0.01	0	0	0	0	0	0	0	1.57
September	9	0	0	0	0	0	0.02	0.03	0	0	0	0	0	0	0	0.25	0.27	0	0	0	0	0	0	1.23	0	0	0.94	0.12	0	0	0		2.86
October	10	0	0	0	0	0	0	0	0.16	0.01	0	0	0	0	0	0	0	0.81	0	0	0	0.54	0.82	0.12	0	0	0	0.15	0	0.06	0	0	2.67
November	11	0	0	0	0.05	0	2.25	1.11	0.02	0	0	0	0	0	0	0	0.18	0.29	0	0	0.03	0.06	0	0.01	1.05	1.06	0	0	0	0.3	0.09		6.5
December	12	0.09	0	0	0.15	0.22	0	0	0	0	0	0	0.02	0	0	0.01	0	0	0	0	0	0	0	0.35	0	0	0.02	0	0	0	0	0	0.86
1997 Totals	**1997**	**0.29**	**1.71**	**0.83**	**0.53**	**1.76**	**0.15**	**0.04**	**0.62**	**1.2**	**0.37**	**0.17**	**0.11**	**2.27**	**0.11**	**1.46**	**0.92**	**1.38**	**1.04**	**2.6**	**1.71**	**0.89**	**0.19**	**0.27**	**2.49**	**1.44**	**3.07**	**1.29**	**0.33**	**0.58**	**1.41**	**0**	**31.23**
January	1	0	0	0	0	0	0	0	0.05	0.3	0	0	0	0	0	0.55	0	0	0	0	0	0.07	0.12	0	0.63	0	0.06	0.96	0	0	0	0	2.74
Feburary	2	0	0	0.44	0	0	0	0.04	0	0	0	0	0	0	0	0	0.01	0	0	0	0.96	0.39	0	0	0	0	2.19	0	0.11				4.14
March	3	0.12	0	0	0	0.02	0	0	0	0.47	0	0	0	0.87	0.02	0	0	0.05	0.45	0	0	0	0	0	0	0.32	0	0.1	0.16	0	0.27	0	2.85
April	4	0	0	0	0.32	0.52	0	0	0	0	0.34	0.07	0	0	0	0	0.03	0	0.48	0	0.64	0.02	0	0	0.05	0	0	0.19	0	0	0		2.66
May	5	0	0.41	0.05	0	0.03	0	0	0.28	0	0	0.06	0.02	0	0.03	0	0	0	0.11	0	0	0	0	0	0.1	0.63	0.6	0.04	0.02	0	0.67	0	3.05
June	6	0.04	0	0.01	0	0	0.09	0	0.02	0	0	0	0	0.7	0	0	0.88	0.02	0	0	0	0	0	0	0	0.23	0	0	0.01	0	0		2
July	7	0	0	0.08	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.36	0	0	0	0	0	0	0	0	0	0	0	0	1.44
August	8	0	0	0	0.11	0	0	0	0.03	0.19	0	0	0.04	0	0.06	0.9	0	0.35	0	1.24	0	0	0	0	0	0	0.06	0	0	0	0.38	0	3.36
September	9	0	1.27	0	0	0	0	0	0.2	0	0	0	0	0	0	0	0	0.96	0	0	0	0	0	0.27	0.03	0	0	0	0	0	0		2.73
October	10	0	0	0	0	0	0	0	0	0.02	0	0	0.05	0.47	0	0	0	0	0	0	0	0	0	0	1.09	0.26	0.16	0	0	0	0	0	2.05
November	11	0.13	0.03	0.03	0	1.19	0.06	0	0	0	0.03	0	0	0.23	0	0.01	0	0	0	0	0.11	0	0	0	0	0	0	0	0.03	0.46	0.05		2.36
December	12	0	0	0.22	0.1	0	0	0	0.04	0.22	0	0.04	0	0	0	0	0	0	0	0	0	0.41	0.07	0	0.59	0	0	0	0	0.12	0.04	0	1.85
1998 Totals	**1998**	**1.33**	**2.02**	**1.31**	**4.35**	**0.81**	**1.65**	**2.05**	**2.63**	**0.33**	**0.59**	**1.85**	**0.13**	**0.99**	**1.1**	**1.44**	**1.53**	**2.48**	**1.35**	**1.28**	**1.5**	**1.3**	**1.07**	**0.45**	**0.05**	**0.53**	**1.21**	**1.17**	**1**	**2.74**	**2.57**	**0.81**	**43.62**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0	0	0	0.37	0.13	0.33	0.69	0.88	0	0	0	0	0	0.29	0	0	0.04	0	0	0	0	0.08	0	0.03	0	0.04	0	0	0	0	0	2.88
Feburary	2	0	0	0	0	0.03	0	0	0	0	0.26	0.78	0	0	0	0	0.49	0.6	0.05	0.02	0	0	0	0	0	0	0.69	0.01	0				2.93
March	3	0	0.01	0.02	0	0.01	0.01	0.32	0.9	0.11	0	0.05	0	0	0	0	0.26	0.95	0	0.91	0.89	0	0	0	0	0	0	0.73	0.31	0	0	0.52	6
April	4	0	0	0.72	0	0	0	0	0	0.02	0	0	0	0.74	0	1.22	0.02	0	0	0	0	0	0.12	0	0	0.1	0	0.43	0.68	0.57	0.01		4.63
May	5	0.76	0.08	0	0	0	0.7	0.07	0	0	0	0	0.13	0	0	0	0	0	0	0	0.03	0.7	0.28	0.45	0	0.36	0.05	0	0	0	0	0.01	3.62
June	6	0	0	0.05	2.47	0.05	0	0	0.85	0	0	1.01	0	0.03	0.55	0.19	0.29	0	0.03	0	0.45	0.3	0.02	0	0	0	0	0	0.01	0.6	0		6.9
July	7	0	0	0.47	1.11	0	0	0.4	0	0	0.14	0	0	0	0	0	0	0	0	0	0	0	0.57	0	0	0	0.43	0	0	0.94	2.33	0	6.39
August	8	0.06	0	0	0.38	0.29	0	0.46	0	0	0	0.01	0	0	0	0	0.06	0	0.81	0	0	0	0	0	0	0	0	0	0	0	0	0.28	2.35
September	9	0.51	0	0	0	0	0	0	0	0	0	0	0	0.22	0.26	0.03	0.09	0.49	0	0	0	0.2	0	0	0.02	0.04	0	0	0	0	0		1.86
October	10	0	0.09	0.01	0	0.3	0.35	0	0	0	0	0	0	0	0	0	0.32	0.4	0.41	0	0	0	0	0	0	0	0	0	0	0.63	0	0	2.51
November	11	0	1.84	0.04	0	0	0	0.11	0	0.2	0.19	0	0	0	0	0	0	0	0	0.18	0	0	0	0	0	0.03	0	0	0	0	0.13		2.72
December	12	0	0	0	0.02	0	0.26	0	0	0	0	0	0	0	0	0	0	0	0.05	0.17	0.13	0.1	0	0	0	0	0	0	0	0	0.1	0	0.83
1999 Totals	**1999**	**3.38**	**1.01**	**1.59**	**0.98**	**0.71**	**1.54**	**2.74**	**3.15**	**2.64**	**0.36**	**0.9**	**4.41**	**0.23**	**0.24**	**0.73**	**0.37**	**0.31**	**0.02**	**0.17**	**0.01**	**0.34**	**0.45**	**2.71**	**0.2**	**0.27**	**0.28**	**0.68**	**0.93**	**0.25**	**1.02**	**1.44**	**34.06**
January	1	0.7	0.54	0	0	0	0.03	0.09	0.01	0	0	0	0.04	0.21	0	0	0	0.27	0	0	0	0.01	0.15	0.87	0	0	0	0	0.07	0	0.68	1.43	5.1
Feburary	2	0.02	0.01	0	0	0	0.81	1.79	0	0	0	0.41	0	0	0	0	0.26	0	0.02	0	0	0	0	0.12	0	0	0	0.08	0				3.52
March	3	0	0.19	0	0	0.27	0	0	0.85	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0.3	0.64	0	0	0	0	0.14	0	0	0	2.4
April	4	0	0	1.17	0	0.01	0	0	0.2	0	0	0	0	0	0.23	0.52	0.06	0	0	0	0	0.18	0	0.17	0	0.27	0.13	0.6	0.18	0	0		3.72
May	5	0	0	0.01	0.72	0	0.05	0	0	0	0	0.05	0.71	0.01	0.01	0.19	0	0	0	0	0	0.1	0	0	0	0	0	0	0	0	0.34	0.01	2.2
June	6	0.43	0	0	0	0	0	0	0.58	0	0.29	0.37	3.04	0	0	0	0	0	0	0	0	0.05	0	0.11	0.2	0	0.15	0	0.04	0	0		5.26
July	7	2.21	0.12	0	0	0	0.65	0	0	1.23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0	0	0	4.22
August	8	0	0	0	0	0	0	0.86	0.58	0	0	0	0.22	0.01	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0	0.18	0	0	1.95
September	9	0	0	0	0	0	0	0	0	0	0	0	0.35	0	0	0	0	0	0	0.17	0.01	0	0	0	0	0	0	0	0.49	0.07	0		1.09
October	10	0	0.15	0.27	0	0	0	0	0.93	0.6	0	0	0	0	0	0	0.05	0.04	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2.04
November	11	0.02	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.7	0	0	0	0	0	0	0		0.72
December	12	0	0	0.14	0.26	0.43	0	0	0	0.8	0.07	0.07	0.05	0	0	0.02	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.84
2000 Totals	**2000**	**0.02**	**0.37**	**0.82**	**0.98**	**1.07**	**1.29**	**3.36**	**0.63**	**0.86**	**0.03**	**1.72**	**1.37**	**0.71**	**0.45**	**0.4**	**1.37**	**1.93**	**3.01**	**0.57**	**1.46**	**0.05**	**1.54**	**1.17**	**4.52**	**1.85**	**2.45**	**1.63**	**1.29**	**0.36**	**0.07**	**0.02**	**37.37**
January	1	0	0	0.52	0	0	0	0	0.16	0.02	0.01	0	0	0	0	0	0	0.21	0	0.01	0	0	0.01	0.01	0	0	0	0	0.02	0.23	0.03	0	1.23
Feburary	2	0	0	0	0	0	0	0	0	0	0	0	0	0.18	0	0	0	0.36	2.24	0	0	0	0	0	0	0.2	0.13	0	0	0			3.11
March	3	0	0	0.24	0	0	0	0	0	0	0	0.34	0	0	0	0	0	0	0.19	0.39	0.23	0	0	0	0.01	0	0.48	0	0	0	0	0	1.88
April	4	0	0	0	0	0.03	0.02	0.83	0	0	0	0.02	0	0	0	0	0.18	0	0	0.04	0	0.01	0	0.33	0.24	0	0	0.1	0.04	0	0		1.84
May	5	0	0	0	0	0	0.46	2.02	0	0.07	0	0	0.18	0	0	0	0	0	0.02	0	0	0	1.31	0	0	0	0.68	1.1	0	0	0	0	5.84
June	6	0	0	0	0.6	0	0	0	0	0	0	0.59	0.58	0	0.19	0	0.52	0.13	0	0	0.82	0.04	0	0.65	2.94	0	1.12	0	0	0.04			8.22
July	7	0	0.12	0.06	0	0	0	0	0	0	0	0	0	0	0	0	0	0.22	0.52	0	0	0	0	0	0	0	0	0.01	1.22	0.09	0	0.01	2.25
August	8	0	0	0	0	0	0.07	0.51	0.45	0	0	0	0	0	0	0	0	1.01	0	0.13	0.35	0	0	0.07	0.63	0	0	0.42	0	0	0	0	3.64
September	9	0	0	0	0	0	0	0	0	0	0.02	0.41	0.24	0	0.03	0	0	0	0	0	0.06	0	0.11	0.11	0.48	1.16	0	0	0	0	0		2.62
October	10	0	0	0	0.38	1.04	0	0	0	0	0	0	0	0	0.23	0.24	0.6	0	0	0	0	0	0.11	0	0	0	0	0	0	0	0	0	2.6
November	11	0	0.2	0	0	0	0.72	0	0.02	0.77	0	0	0.37	0	0	0	0	0	0	0	0	0	0	0	0.22	0.49	0	0	0	0	0		2.79
December	12	0.02	0.05	0	0	0	0.02	0	0	0	0	0.36	0	0.53	0	0.16	0.07	0	0.04	0	0	0	0	0	0	0	0.04	0	0.01	0.04	0	0.01	1.35
2001 Totals	**2001**	**0.05**	**0.72**	**0.9**	**0.92**	**1.57**	**0.41**	**0**	**1.41**	**1.28**	**2.32**	**1.43**	**1.07**	**0.54**	**1.36**	**2.46**	**1.31**	**1.01**	**2.96**	**0.46**	**0.81**	**0.43**	**0.31**	**2.1**	**4.18**	**0.13**	**0.24**	**1.23**	**0.81**	**1.14**	**1.32**	**0.41**	**35.29**
January	1	0	0	0	0	0	0	0	0	0	0	0.02	0.01	0.19	0.01	0	0	0	0	0.01	0	0	0	0	0	0	0.09	0	0.11	0.59	0.08	0.01	1.12
Feburary	2	0	0	0	0	0	0	0	0.01	0.55	0	0	0	0.1	0.08	0	0	0	0	0	0	0.03	0.03	0.12	1.49	0	0	0.07	0				2.48
March	3	0.01	0	0	0	0	0	0	0	0	0	0	0.02	0	0.02	1.1	0.14	0	0	0	0	0	0.07	0	0.04	0	0	0	0	0	0	0.05	1.45
April	4	0	0.27	0.48	0	0	0	0	0	0.38	1.02	0.14	0	0	0.01	0.36	0	0	0	0	0	0	0	0.08	0	0	0	0	0	0	0.27		3.01
May	5	0	0	0	0	0.04	0.01	0	0	0	0	0	0	0	0	0	0	0.43	0.52	0	0.24	0.19	0.05	0.04	0	0.05	0	0	0	0.13	0.76	0.35	2.81
June	6	0.04	0	0.42	0.41	0	0.4	0	0	0	0	0	0	0	0.73	0.01	0	0	0	0	0.21	0.21	0	0	0	0	0	1.16	0.01	0	0		3.6
July	7	0	0.05	0	0.51	0.55	0	0	0	0	0	0	0.24	0	0	0	0	0.04	1.29	0.42	0.15	0	0	0.53	0.22	0	0	0	0	0	0	0	4
August	8	0	0.26	0	0	0	0	0	0	0.2	0.03	0	0	0	0	0.08	0.01	0.08	0	0	0	0	0	0.8	0.43	0.08	0	0	0	0	0.02	0	1.99
September	9	0	0	0	0	0	0	0	1.4	0.15	0	0	0	0	0	0	0	0.01	1.04	0	0.21	0	0	0	0	0	0	0	0	0	0		2.81
October	10	0	0	0	0	0.9	0	0	0	0	1.27	1.27	0	0.22	0	0.64	0	0	0	0	0	0	0	0.49	0.71	0	0	0	0	0	0	0	5.5
November	11	0	0.14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.11	0.03	0	0	0	0.04	1.29	0	0.15	0	0.69	0.42	0.19		3.06
December	12	0	0	0	0	0.08	0	0	0	0	0	0	0.8	0.03	0.51	0.27	1.16	0.45	0	0	0	0	0.16	0	0	0	0	0	0	0	0	0	0	3.46
2002 Totals	**2002**	**0.02**	**3.12**	**0.59**	**1**	**1.02**	**3.51**	**1.53**	**1.43**	**0.96**	**0.6**	**1.57**	**3.34**	**0.62**	**0.64**	**0.67**	**0.83**	**1.14**	**2.82**	**4.32**	**0.99**	**0.03**	**0.09**	**0.69**	**2.12**	**1.48**	**0.5**	**1.03**	**0.63**	**1.1**	**1.49**	**1.07**	**40.95**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0	0	0	0	0.09	0.04	0	0	0	0	0	0	0	0	0	0	0	0.11	0.06	0	0	0	0.24	0	0	0	0	0	0.28	1.37	0.97	3.16
Feburary	2	0.01	0	0	0	0	0	0	0	0.01	0.14	0	0	0	0	0	0	0	0	0.4	0.04	0	0	0	0	0.2	0.03	0	0				0.83
March	3	0	0.95	0	0	0	0	0	0.03	0.59	0	0.03	0	0	0	0.6	0.01	0	0.04	0.36	0.06	0	0	0	0.32	0.41	0.22	0	0.01	0.04	0	0	3.67
April	4	0	0.01	0	0	0	0	0.13	0.54	0	0	0	0.07	0	0.02	0	0.06	0	0	1.76	0.53	0.03	0	0	0.07	0	0	1.03	0	0	0		4.25
May	5	0.01	0.13	0	0.03	0	0.56	1.4	0.86	0.19	0	0.01	2.18	0.48	0	0	0.47	0.72	0	0	0	0	0	0	0.19	0	0	0	0.57	0	0.01	0	7.81
June	6	0	0	0	0.56	0.58	0	0	0	0.15	0.44	1.53	0.96	0	0	0	0	0	0	0	0	0	0	0	1.01	0.03	0	0	0	0	0		5.26
July	7	0	0	0.47	0	0	0	0	0	0	0.02	0	0.02	0	0	0	0.26	0	0.14	0	0	0	0.09	0.25	0	0	0.22	0	0	0	0	0	1.47
August	8	0	0	0	0	0	2.68	0	0	0	0	0	0	0.11	0.21	0	0.03	0	0.85	0.02	0.02	0	0	0.2	0	0	0	0	0	0	0	0	4.12
September	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0.05	0	0	0.41	0	1.64	0.34	0	0	0	0	0	0	0	0	0	0		2.44
October	10	0	1.82	0.05	0.24	0	0.23	0	0	0	0	0	0.11	0	0	0	0	0	0.5	0.07	0	0	0	0	0	0.84	0.03	0	0.05	0.78	0.05	0.01	4.78
November	11	0	0.21	0.07	0	0.35	0	0	0	0.02	0	0	0	0	0.36	0.07	0	0	0	0	0	0	0	0	0.06	0	0	0	0	0	0		1.14
December	12	0	0	0	0.17	0	0	0	0	0	0	0	0	0.03	0	0	0	0.01	1.18	0.01	0	0	0	0	0.47	0	0	0	0	0	0.06	0.09	2.02
2003 Totals	**2003**	**2.93**	**2.09**	**0.14**	**1.02**	**0.79**	**1.79**	**0.08**	**0.07**	**1.69**	**5.03**	**0.66**	**2.39**	**1.78**	**1.03**	**0.49**	**2.28**	**1.57**	**2.73**	**1.65**	**0.66**	**0.05**	**1.12**	**1.01**	**1.41**	**4.23**	**1.82**	**0.55**	**1.17**	**0.49**	**1.94**	**1.4**	**46.06**
January	1	0.19	0.43	0	0	0	0	0	0	0	0	0	0	0	0	0	0.03	0	0.02	0	0	0	0.07	0	0	0	0	0	0	0.01	0	0.21	0.96
Feburary	2	0	0	0.01	0	0	0.11	0	0	0.04	0	0	0	0	0.51	0.41	0.16	0	0.03	0.18	0	0	0.15	0.2	0	0	0	0.14	0.06				2
March	3	0.01	0	0	0	0.05	0	0	0	0	0	0.41	0.07	0.69	0	0	0	0	0.05	0.99	0.19	0.01	0	0	0	0.03	0	0	0.3	0	0	0	2.8
April	4	0	0	0	0.1	0	0.59	0	0.07	0	0	0	0	0	0	0	1.2	0.12	0	0.03	0.38	0	0	0	0.83	0.4	0	0	0.39	0.18	0		4.29
May	5	0.06	0	0	0.78	0.21	0.51	0	0	0	1.02	0	0	0	0	0.04	0.08	0.06	0.01	0.01	0.09	0	0	0	0.55	0.29	0	0	0	0	0.26	0	3.97
June	6	0	0.55	0	0	0	0.29	0	0	0	2.68	0.18	2.09	0.86	0	0	0	0	0	0.44	0	0	0	0	0	3.31	0.47	0	0	0	1.48		12.35
July	7	0	0.39	0	0	0	0	0	0	0.22	0.96	0	0	0	0	0	0	0	0.74	0	0	0	0.12	0	0	0	0	0	0.08	0	0	0	2.51
August	8	0.06	0.45	0	0	0	0.15	0.08	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.37	0	0.24	0	1.19	2.54
September	9	1.98	0.27	0	0	0	0	0	0	0	0	0	0.23	0.02	0.01	0	0	0	0	0	0	0.04	0.01	0	0.03	0	1.35	0.01	0	0	0.2		4.15
October	10	0	0	0.03	0	0	0	0	0	1.13	0	0.07	0	0.08	0.25	0	0.8	0.04	0	0	0	0	0	0	0	0.2	0	0.03	0.18	0	0	0	2.81
November	11	0.63	0	0	0.06	0.43	0.14	0	0	0	0	0	0	0	0.26	0.04	0	1.35	1.85	0	0	0	0	0.58	0	0	0	0	0	0	0		5.34
December	12	0	0	0.1	0.08	0.1	0	0	0	0.3	0.37	0	0	0.13	0	0	0.01	0	0.03	0	0	0	0.77	0.23	0	0	0	0	0.16	0.06	0	0	2.34
2004 Totals	**2004**	**1.72**	**0.92**	**1.08**	**4.66**	**1.9**	**1.02**	**0.48**	**0.18**	**0.32**	**0.32**	**1.66**	**0.87**	**1.65**	**1.2**	**0.24**	**0.44**	**1.07**	**1.51**	**1.32**	**0.56**	**0.09**	**0.59**	**0.8**	**2.83**	**3.45**	**3.05**	**2.54**	**0.33**	**0.53**	**4.6**	**0.34**	**42.27**
January	1	0.03	0	0.12	2.2	0	0	0	0	0	0	0	0	0	0	0	0.1	1.02	0	0	0	0	0	0	0	0.45	0.02	0.03	0	0	0	0	3.97
Feburary	2	0.06	0.64	0	0	0.06	0.02	0	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0	0	0.03	0	0	0	0	0	0.03			0.85
March	3	0	0	0.25	1.26	0.09	0	0	0	0.01	0	0	0	0.06	0.05	0.02	0.07	0.05	0	0	0	0	0	0.06	0	0.46	1.57	0.07	0.31	0.02	0	0.01	4.36
April	4	0	0	0	0	0	0	0	0	0	0.18	0	0	0	0	0	0	0	0	0	0.06	0	0.21	0	0.75	0	0	0	0	0.03	0.71		1.94
May	5	0.69	0.05	0	0	0	0	0	0	0	0.03	0	0.05	1.53	0.62	0	0	0	0.36	1.1	0	0	0	0.02	0.17	0.76	0.95	2.09	0	0	1.18	0.15	9.75
June	6	0	0	0	0	0	0	0	0	0.31	0.02	0	0.01	0.03	0	0	0.23	0	0.11	0	0	0.09	0.01	0	0	0	0	0	0.02	0	0		0.83
July	7	0.03	0.22	0.41	0	1.51	0.19	0	0	0	0	0.1	0	0	0	0	0.02	0	0	0	0	0	0.09	0	0.15	0.48	0	0	0	0.07	2.25	0	5.52
August	8	0	0	0.07	1.18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.05	0.49	0	0	0.45	0.37	1.3	0.08	0.09	0	0.02	0	0	4.1
September	9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.22	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0	0		0.23
October	10	0.09	0	0	0	0	0	0	0.18	0	0	0.2	0.81	0.03	0.53	0	0	0	0.65	0.03	0	0	0	0.19	0	0	0.43	0.01	0	0	0	0.06	3.21
November	11	0.82	0.01	0.23	0.02	0	0	0	0	0	0	1.33	0	0	0	0	0.01	0	0.39	0.14	0	0	0.28	0.05	1.39	0	0	0.25	0	0.36	0.46		5.74
December	12	0	0	0	0	0.24	0.81	0.48	0	0	0.09	0.03	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.12	1.77
2005 Totals	**2005**	**0.14**	**0.54**	**1.86**	**2.13**	**2.16**	**0.26**	**0.51**	**0.78**	**1.23**	**0**	**3.35**	**2.52**	**4.21**	**1.17**	**3.01**	**0.05**	**0**	**0.8**	**1.82**	**0.3**	**0.29**	**1.48**	**0.25**	**0.3**	**3**	**0.85**	**1.61**	**1.65**	**0.32**	**0.2**	**1.06**	**37.85**
January	1	0.14	0.47	1.83	1.83	1.58	0	0.05	0	0	0	0.08	1.67	1.11	0	0.02	0.01	0	0	0	0	0	0	0	0	0	0	0	0.05	0.17	0	0	9.01
Feburary	2	0	0.07	0	0	0	0.18	0.35	0.14	0.12	0	0	0.05	0.76	0	0	0	0	0	0	0.01	0	0	0.03	0.02	0	0	0	0.11				1.84
March	3	0	0	0	0	0	0	0.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.05	0.1	0.12	0.1	0	0	0	0	0	0	1.47
April	4	0	0	0	0	0	0.02	0.01	0	0	0	0.27	0.4	0.13	0	0	0	0	0	0	0.07	0.28	0.3	0.12	0	0.21	0.12	0	0.14	0.1	0		2.17
May	5	0	0	0	0	0	0	0	0	0.01	0	0	0	0	0.24	0	0	0	0	0.31	0	0.01	0.1	0	0	0	0	0.06	0	0.05	0	0	0.78
June	6	0	0	0	0	0	0.03	0	0.48	1.1	0	2.02	0	0.59	0	0	0	0	0	0	0	0	0	0	0	0.88	0	0	0	0	0		5.1
July	7	0	0	0	0.06	0	0	0	0	0	0	0.91	0.35	0.04	0.04	0.03	0	0	0.35	0	0	0	0	0	0	0	0.38	0.06	0	0	0	0	2.22
August	8	0	0	0	0.24	0.1	0	0	0	0	0	0.06	0.05	1.09	0.11	1.14	0.04	0	0.23	0	0	0	0	0	0.02	0.44	0.35	0	0	0	0	0	3.87
September	9	0	0	0	0	0	0	0	0	0	0	0	0	0.49	0.17	1.03	0	0	0.21	1.42	0	0	0	0	0.01	1.04	0	0	0.93	0	0		5.3
October	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.09	0.22	0	0.03	0	0	0	0	0	0	0	0.12	1.06	1.52
November	11	0	0	0	0	0.48	0.03	0	0	0	0	0	0	0	0.27	0.79	0	0	0	0	0	0	0	0	0	0	0	1.49	0.29	0	0		3.35
December	12	0	0	0.03	0	0	0	0	0.16	0	0	0.01	0	0	0.34	0	0	0	0.01	0	0	0	0	0	0.13	0.33	0	0	0.13	0	0.08	0	1.22
2006 Totals	**2006**	**2.22**	**0.68**	**0.13**	**0.09**	**0.26**	**0.71**	**0.02**	**0.67**	**1.02**	**2.59**	**1.59**	**0.26**	**1.1**	**0.23**	**1.55**	**2.34**	**0.66**	**0.84**	**0.24**	**1.09**	**2.06**	**0.1**	**0.03**	**0.05**	**0.3**	**1.38**	**1.67**	**0.75**	**1.25**	**3.44**	**0.61**	**29.93**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0	0.18	0	0	0	0	0	0	0	0.43	0	0	0.24	0	0	0.08	0	0	0	0.1	0	0	0	0	0	0	0	0.58	0.02	0	0	1.63
Feburary	2	0	0	0	0	0	0	0	0.19	0	0	0	0	0	0	0.01	0.26	0	0	0	0	0	0	0	0	0	0	0	0				0.46
March	3	0	0	0	0	0.19	0	0	0.48	0.79	0	0.41	0.23	0.09	0	0	0	0	0	0	0.43	0.2	0	0	0	0	0	0.31	0	0	0	0.13	3.26
April	4	0	0.5	0	0	0.03	0.55	0	0	0	0	0	0	0	0	0.03	0	0	0.17	0	0	0	0	0.01	0	0.01	0	0	0	0.48	0.32		2.1
May	5	0.56	0	0.13	0	0	0	0	0	0.23	1.18	0.16	0	0	0.08	0.08	0.36	0	0	0	0	0	0	0	0.05	0	0	0	0	0	0	0.05	2.88
June	6	1.23	0	0	0	0	0	0	0	0	0.61	0.32	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0.01	0	0	0.1	0		2.37
July	7	0	0	0	0	0	0	0	0	0	0	0.08	0.01	0.74	0	0	0	0	0	0.12	0	1.35	0	0	0	0	0	0.1	0	0.33	0	0	2.73
August	8	0	0	0	0	0	0	0	0	0	0.14	0	0	0	0.01	0	0	0	0.67	0.12	0	0	0	0	0	0.06	1.03	0.07	0.17	0	0	0	2.27
September	9	0.05	0	0	0.09	0.03	0	0	0	0	0	0.39	0.02	0	0	0	0	0.66	0	0	0	0	0	0.02	0	0	0	0	0	0	0.02		1.28
October	10	0	0	0	0	0	0	0	0	0	0	0.09	0	0	0	0	1.64	0	0	0	0	0.16	0	0	0	0.23	0.34	1.19	0	0	0.01	0	3.66
November	11	0	0	0	0	0.01	0.16	0.01	0	0	0.23	0	0	0.03	0.14	1.43	0	0	0	0	0	0	0	0	0	0	0	0	0	0.32	2.92		5.25
December	12	0.38	0	0	0	0	0	0.01	0	0	0	0.14	0	0	0	0	0	0	0	0	0.56	0.35	0	0	0	0	0	0	0	0	0.17	0.43	2.04
2007 Totals	**2007**	**1.41**	**1.4**	**1.53**	**2.09**	**0.63**	**0.66**	**0.68**	**0.21**	**0.56**	**1.01**	**0.44**	**2.37**	**1.32**	**2.22**	**1.14**	**0.04**	**0.5**	**0.51**	**2.13**	**0.42**	**0.42**	**0.62**	**0.59**	**1.55**	**0.53**	**1.05**	**1.52**	**0.64**	**0.49**	**0.93**	**0.96**	**30.57**
January	1	0	0	0	0.25	0	0	0.06	0	0.01	0	0	1.43	0.29	0.8	0.02	0	0	0	0	0.1	0.11	0	0	0	0	0	0	0.01	0	0	0.03	3.11
Feburary	2	0.01	0	0	0	0.03	0	0	0	0	0	0	0.5	0.44	0	0	0.01	0.04	0	0	0	0	0	0	0.82	0.12	0	0	0.01				1.98
March	3	0	0	0	0	0	0	0	0	0.06	0	0	0	0	0.84	0.01	0	0	0	0	0.05	0	0.18	0.21	0	0	0	0.03	0.03	0	0.84	0.55	2.8
April	4	0	0	1.02	0	0	0	0	0	0	0.65	0.1	0	0.35	0.58	0	0	0	0	0	0	0	0	0	0.1	0.19	0.19	0	0	0	0		3.18
May	5	0.58	0.17	0.15	1.42	0	0	0	0	0	0.07	0.03	0	0	0	0.43	0	0	0	0	0	0	0	0	0	0	0.21	0.72	0.01	0	0.09	0.38	4.26
June	6	0.82	0.11	0	0.01	0.06	0	0	0.01	0	0	0	0	0	0	0	0	0	0.21	0	0	0	0	0.34	0	0	0	0.68	0.52	0.12	0		2.88
July	7	0	0	0	0.41	0.07	0	0	0	0	0.1	0	0	0	0	0	0	0.1	0	2.12	0	0	0	0	0	0	0	0.08	0	0.23	0	0	3.11
August	8	0	0	0.34	0	0	0	0	0	0	0	0	0	0.23	0	0	0	0	0.02	0.01	0.18	0.02	0	0	0.63	0	0	0	0	0.14	0	0	1.57
September	9	0	0	0	0	0.47	0.51	0.62	0.05	0	0.04	0	0	0	0	0.01	0	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0		1.71
October	10	0	0.86	0.02	0	0	0	0	0	0	0	0	0	0	0	0	0	0.36	0.28	0	0	0	0.17	0.04	0	0.05	0.19	0	0	0	0	0	1.97
November	11	0	0	0	0	0	0	0	0	0	0	0.02	0.44	0.01	0	0	0	0	0	0	0	0.29	0	0	0	0.17	0.32	0	0	0	0		1.25
December	12	0	0.26	0	0	0	0.15	0	0.15	0.49	0.15	0.29	0	0	0	0.67	0.03	0	0	0	0.09	0	0.27	0	0	0	0.13	0.01	0.06	0	0	0	2.75
2008 Totals	**2008**	**0.36**	**0.92**	**2.68**	**3.99**	**2.36**	**0.48**	**1.71**	**2.78**	**0.91**	**2.49**	**0.8**	**1.76**	**0.66**	**5.7**	**0.98**	**0.5**	**1.48**	**3.44**	**0.63**	**0.64**	**1.49**	**1.44**	**1.86**	**0.99**	**2.77**	**3.47**	**4.19**	**0.42**	**0.33**	**3.99**	**1.74**	**57.96**
January	1	0	0	0	0	0	0	0	1.56	0	0.11	0	0	0	0	0	0	0	0	0	0	0.01	0	0	0	0	0	0	0	0	0	0.3	1.98
Feburary	2	0.32	0	0.14	0	2.36	0.06	0	0.01	0	0	0.04	0	0	0	0	0.46	0.63	0	0	0	0.34	0.02	0	0.1	0.05	0.03	0	0.04	0			4.6
March	3	0	0	0.74	0.73	0	0	0	0	0	0	0	0	0.04	0	0.21	0	0.85	2.46	0.31	0	0	0	0.04	0	0	1.24	0.22	0	0	0.33	1.22	8.39
April	4	0	0	0.82	0	0	0	0	0.12	0	1.45	0	0	0.03	0	0	0	0	0.64	0.03	0	0	0.06	0	0.14	0.35	0	0.07	0.05	0	0		3.76
May	5	0	0.23	0	0	0	0	1.24	0.72	0.21	0.93	0.28	0	0.41	0.04	0.22	0	0	0	0	0	0	0.16	0.25	0.03	1.61	2.19	0.62	0	0	1.48	0.22	10.84
June	6	0	0	0.24	0.2	0	0.2	0.01	0	0.06	0	0	0	0.18	0	0	0	0	0	0	0.58	0	0.01	0	0.28	0	0.01	0.12	0	0	0		1.89
July	7	0	0.69	0.3	0	0	0	0	0.33	0.28	0	0.02	0.01	0	0	0	0	0	0	0.01	0	0.42	1.19	0	0.14	0.76	0	1.34	0.19	0	1.82	0	7.5
August	8	0	0	0.33	0	0	0.18	0.16	0	0	0	0	0	0	0	0	0	0	0	0	0.06	0.72	0	0	0	0	0	0	0.14	0	0	0	1.59
September	9	0	0	0.04	3.06	0	0	0.08	0	0	0	0.01	1.71	0	4.58	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.29	0		9.77
October	10	0	0	0	0	0	0	0.22	0	0	0	0	0	0	0	0.37	0	0	0	0	0	0	0	0.54	0.1	0	0	0	0	0	0	0	1.23
November	11	0	0	0	0	0	0.03	0	0	0	0	0.45	0.04	0	0.81	0.1	0	0	0	0	0	0	0	0.03	0	0	0	0	0	0.04	0.36		1.86
December	12	0.04	0	0.07	0	0	0.01	0	0.04	0.36	0	0	0	0	0.27	0.08	0.04	0	0.34	0.28	0	0	0	1	0.2	0	0	1.82	0	0	0	0	4.55
2009 Totals	**2009**	**1.3**	**1.43**	**0.13**	**1.78**	**1.67**	**0.59**	**0.15**	**4.11**	**1.96**	**2.67**	**1.36**	**1.54**	**2**	**0.78**	**3.55**	**4.19**	**1.48**	**0.65**	**0.77**	**1.7**	**0.46**	**2**	**1.21**	**1.88**	**2.46**	**1.11**	**1.84**	**1.92**	**2.28**	**1.85**	**0.1**	**50.92**
January	1	0	0	0	0	0	0.01	0	0	0	0.02	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.07	0.17	0.42	0.08	0	0	0	0.77
Feburary	2	0	0	0	0	0	0	0	0	0.1	0.44	1.22	0	0.01	0	0	0	0	0	0	0	0.03	0	0	0	0	0.53	0	0				2.33
March	3	0	0	0	0	0	0	0	0	0.07	0.49	0	0	0	0	0	0	0	0.29	0	0	0.04	0	0	0.54	0	0	0	1.14	0.37	0	0.1	3.04
April	4	0	0.24	0	0	0.09	0.04	0	0	1.11	0.33	0	0.13	0.5	0	0	0	0	0.23	0.45	0.01	0	0	0	0	0	0.45	0.01	0.42	0.05			4.06
May	5	0.16	0.01	0	0	0.02	0.1	0.14	0.67	0	0	0	0	0.13	0	0.47	0.03	0	0	0	0	0	0	0.03	0.03	2.01	0.07	0.4	0.24	0	0.21	0	4.72
June	6	0	0.92	0.13	0	0	0	0.01	0.21	0.02	1.14	0.14	0	0	0	1.86	1.59	0	0	0.21	0.07	0	0	0	0	0	0	0.02	0.1	0	0		6.42
July	7	0	0	0	1.78	0.08	0	0	0	0	0	0	0.9	0	0	0.36	0.74	0	0	0	0	0	0	0	0	0	0	0	0.25	0.08	0.01	0	4.2
August	8	0.09	0	0	0	0	0	0	0	0	0.25	0	0	0	0	0	0.11	1.18	0	0.06	0.67	0.02	0	0	0	0	0	0	0.1	0	0	0	2.48
September	9	0	0	0	0	1.48	0.01	0	0	0	0	0	0	0	0	0	0	0	0	0	0.95	0.37	0.03	0	0.1	0	0.22	0	0	0	0		3.16
October	10	1.05	0	0	0	0	0.42	0	2.66	0.64	0	0	0.05	0.8	0.78	0.16	0	0	0	0	0	0	1.91	0.08	0	0.29	0.12	0.51	0	1.41	1.5	0	12.38
November	11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.7	1.72	0.3	0.09	0.03	0	0	0	0	0.26	0.01	0	0	0	0	0		3.11
December	12	0	0.26	0	0	0	0.01	0	0.57	0.02	0	0	0.46	0.56	0	0	0	0	0.04	0.02	0	0	0.06	1.1	0.95	0.08	0	0.04	0	0	0.08	0	4.25
2010 Totals	**2010**	**0.11**	**1.15**	**0.4**	**0.53**	**1.33**	**0.2**	**0.21**	**1.75**	**0.82**	**0.94**	**1.23**	**1.93**	**0.74**	**2.41**	**0.96**	**1.01**	**0.71**	**0.74**	**0.97**	**3.18**	**2.88**	**1.32**	**0.56**	**6.15**	**2.1**	**0.74**	**1.43**	**0.26**	**0.57**	**1.2**	**0.54**	**39.07**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0.03	0	0	0	0	0.12	0.07	0	0	0	0	0	0	0	0	0	0	0	0	0.11	0.29	0	0.43	0.09	0	0.01	0.05	0	0	0	0	1.2
Feburary	2	0	0	0	0.12	0.67	0	0	0.12	0.04	0	0	0	0	0.19	0.01	0	0	0	0.01	0	0.86	0.07	0	0	0	0	0	0				2.09
March	3	0	0	0	0	0	0	0	0	0.13	0	0.4	0.23	0.21	0.03	0	0	0	0	0	0.03	0.28	0.03	0	0	0.74	0	0.01	0.26	0	0	0	2.35
April	4	0	0.1	0.32	0.25	0.27	0	0	0	0	0	0	0	0	0	0	0.02	0	0	0	0	0	0.37	0.13	0.78	0.33	0.03	0.12	0	0	0.29		3.01
May	5	0.01	0.13	0.02	0	0	0	0	0	0	0.27	0.01	1.29	0.09	0.3	0.5	0.99	0.02	0	0	0.35	0.27	0	0	0	0	0.38	0	0	0	0	0.01	4.64
June	6	0	0.58	0.05	0	0	0	0	0.68	0.03	0	0	0.26	0.34	0.25	0.38	0	0.41	0	0.07	0	0	0.01	0	0.03	0	0	0.95	0	0	0		4.04
July	7	0	0	0	0.13	0	0.08	0.14	0.95	0.36	0	0.01	0.02	0.08	0	0	0	0.14	0.25	0.02	1.97	0.74	0	0	0.97	0	0	0.3	0	0.01	0.52	0	6.69
August	8	0	0	0	0	0.39	0	0	0	0	0.04	0	0	0	1.64	0	0	0	0	0	0.72	0.44	0	0	0	0	0	0	0	0	0.39	0	3.62
September	9	0.07	0.33	0.01	0	0	0	0	0	0.26	0.63	0.54	0	0	0	0.06	0	0	0.46	0.86	0	0	0.07	0	0.16	0.2	0.08	0	0	0	0		3.73
October	10	0	0.01	0	0	0	0	0	0	0	0	0.01	0	0.01	0	0	0	0	0	0	0	0	0	0	0.79	0	0.24	0	0	0	0	0	1.06
November	11	0	0	0	0.03	0	0	0	0	0	0	0	0	0.01	0	0	0	0.14	0.03	0	0	0	0.77	0	3.08	0.78	0	0	0	0.5	0		5.34
December	12	0	0	0	0	0	0	0	0	0	0	0.26	0.13	0	0	0.01	0	0	0	0.01	0	0	0	0	0.25	0.05	0	0	0	0.06	0	0.53	1.3
2011 Totals	**2011**	**1.18**	**0.06**	**2.88**	**2.28**	**1.18**	**0.02**	**1.84**	**0.85**	**0.89**	**1.66**	**0.34**	**0.45**	**0.79**	**4.44**	**1.3**	**0.03**	**1.72**	**2**	**3.52**	**0.76**	**0.61**	**3.18**	**1.59**	**1.09**	**5.53**	**3.53**	**2.46**	**0.42**	**0.01**	**0.22**	**0.34**	**47.17**
January	1	0	0	0	0	0	0	0.03	0	0	0.1	0.13	0	0	0	0	0	0.01	0.08	0.21	0.37	0	0	0.05	0.01	0	0	0	0	0	0	0.34	1.33
Feburary	2	0.9	0	0	0	0.2	0	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0	0.43	0	0.08	0.8	0.4	0	0.39	0.16				3.37
March	3	0	0	0	1.36	0.37	0	0	0.47	0	0	0	0	0.27	1.21	0	0	0	0.03	0.31	0	0	0	0	0.02	0.27	0.39	0	0	0	0.04	0	4.74
April	4	0	0	0	0.67	0	0	0	0.01	0.69	0.18	0.17	0	0	0	0.81	0.01	0	0.01	1.66	0	0.09	1.29	0.64	0.26	0.66	0.05	0.65	0.03	0	0		7.88
May	5	0.28	0.01	0	0	0.05	0	0.05	0	0	0.26	0	0	0.03	0.53	0.35	0	0	0	0.04	0.01	0.03	0.5	0.25	0	1.4	0.31	0.04	0.02	0	0	0	4.16
June	6	0	0	0	0	0	0	0	0	0	1.06	0.04	0.01	0	0.54	0.14	0	1.12	0.34	0.33	0	0.05	0	0	0	2.8	1.65	1.02	0	0	0		9.1
July	7	0	0	1.59	0.06	0	0	0.56	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.53	0	0	0	0	0	0	0.17	0	2.91
August	8	0	0	0	0	0.56	0.02	0	0	0	0.04	0	0.1	0.09	0	0	0	0	0	0.11	0.07	0	0.05	0	0	0	0	0	0	0	0	0	1.04
September	9	0	0	0.16	0	0	0	0	0	0.18	0.02	0	0	0	1.78	0	0.02	0.02	0.93	0	0	0	0.03	0.04	0	0	0	0	0	0	0		3.18
October	10	0	0	0	0	0	0	0	0	0	0	0	0.34	0.01	0	0	0	0.57	0.61	0.05	0	0	0	0	0	0	0.08	0	0	0	0	0	1.66
November	11	0	0.05	0.96	0	0	0	1.2	0.37	0.02	0	0	0	0.03	0	0	0	0	0	0	0.06	0	1.31	0	0	0	0.45	0.02	0.21	0	0		4.68
December	12	0	0	0.17	0.19	0	0	0	0	0	0	0	0	0.36	0.38	0	0	0	0	0.8	0.25	0.01	0	0	0	0	0.6	0.34	0	0.01	0.01	0	3.12
2012 Totals	**2012**	**1.14**	**0.35**	**1.77**	**1.47**	**1.51**	**0.03**	**1.55**	**1.18**	**0.31**	**0.05**	**2.5**	**0.18**	**1.46**	**2.46**	**2.17**	**1.74**	**2.82**	**0.02**	**0.09**	**0.54**	**0**	**0.5**	**0.41**	**0**	**2.26**	**1.36**	**0.14**	**1.61**	**0.83**	**0.05**	**1.8**	**32.3**
January	1	0	0	0	0	0	0	0	0	0	0	0.04	0.15	0	0	0	0	0.85	0	0	0	0	0	0	0	0.77	0.34	0.12	0.07	0	0	0	2.34
Feburary	2	0	0	1.05	0.23	0.04	0	0.09	0.04	0	0.04	0.01	0	0.13	0	0.16	0.14	0	0	0	0.03	0	0	0.03	0	0	0	0	0	0.02			2.01
March	3	0	0.2	0	0	0	0	0.01	0.2	0	0	0.19	0	0	0	0.74	0.22	1.34	0.01	0	0	0	0.19	0.13	0	0	0	0	0	0.1	0	0	3.33
April	4	0	0	0.72	0.31	0.72	0	0	0	0	0	0	0	1.12	1.3	0.92	0	0	0	0	0.1	0	0.14	0	0	0	0	0	1.4	0.52	0.05		7.3
May	5	0.57	0	0	0.1	0	0.01	0.82	0	0	0	0	0	0	0	0	0	0	0	0	0.1	0	0	0	0	0	0	0	0	0	0	0.1	1.7
June	6	0	0	0	0.04	0	0	0	0	0	0	1.06	0	0	0	0	0.87	0	0	0	0	0	0	0	0	0	0	0	0	0	0		1.97
July	7	0	0	0	0	0	0	0.01	0.24	0.03	0	0	0	0	0.25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.19	0	0	0.72
August	8	0	0.01	0	0.48	0	0	0	0.46	0.01	0	0	0.03	0.09	0	0	0.51	0	0	0	0	0	0	0	0	0.08	0.83	0.02	0	0	0	1.48	4
September	9	0.57	0.11	0	0.01	0.13	0	0.57	0	0	0	0	0	0	0.1	0	0	0.29	0.01	0	0	0	0	0	0	0.97	0.19	0	0.08	0	0		3.03
October	10	0	0	0	0	0.54	0	0	0	0.01	0.01	0	0	0.12	0.77	0	0	0.27	0	0.01	0	0	0.08	0.25	0	0.44	0	0	0	0	0	0	2.5
November	11	0	0	0	0	0.08	0.02	0	0	0	0	1.2	0	0	0	0	0	0	0	0.01	0	0	0.09	0	0	0	0	0	0	0	0		1.4
December	12	0	0.03	0	0.3	0	0	0.05	0.24	0.26	0	0	0	0	0.04	0.35	0	0.07	0	0.07	0.31	0	0	0	0	0	0	0	0.06	0	0	0.22	2
2013 Totals	**2013**	**2.15**	**1.65**	**2.24**	**0.02**	**1**	**0.31**	**0.25**	**0.88**	**1.2**	**4.06**	**0.17**	**0.84**	**0.37**	**0.69**	**2.07**	**0.86**	**1.84**	**3.21**	**0.17**	**1.62**	**2.22**	**0.25**	**2.36**	**1.26**	**0.3**	**2.35**	**1.18**	**0.11**	**1.97**	**2.42**	**2.66**	**42.68**
January	1	0	0	0	0	0	0	0	0	0	0.62	0	0.65	0	0	0	0	0	0	0	0	0	0.02	0	0	0	0	0.24	0	1.44	0.15	0	3.12
Feburary	2	0	0.14	0.12	0	0	0	0.23	0	0.09	0.46	0	0	0	0	0	0	0	0.16	0	0	0.94	0.01	0	0	0.19	0.84	0.06	0.03				3.27
March	3	0.08	0	0	0.02	0.25	0	0	0	0.44	1.35	0.01	0	0.01	0	0	0.09	1.19	0.02	0	0	0	0	0.06	1.25	0.03	0	0	0	0	0.15	0	4.95
April	4	0	0	0	0	0	0	0.02	0	0	1.02	0.1	0	0	0	0.45	0.45	0	2.48	0	0	0	0	0.72	0.01	0	0	0.41	0.01	0	0		5.67
May	5	0	0.37	1.99	0	0.15	0	0	0	0.18	0	0	0	0	0	0	0	0.27	0	0	1.22	0.01	0	0.02	0	0.08	0.02	0.47	0.05	0	0.56	1.74	7.13
June	6	0.26	0	0	0	0.05	0	0	0	0.49	0.06	0	0	0	0	1.13	0.24	0.28	0	0	0	0	0.02	1.54	0	0	1.44	0	0.01	0.4	0.01		5.93
July	7	0	0.54	0	0	0	0.07	0	0	0	0.55	0	0	0	0.28	0	0	0.05	0.28	0	0	0	0	0	0	0	0.05	0	0	0	1.53	0	3.35
August	8	0	0.42	0	0	0	0	0	0.42	0	0	0	0.17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.18	1.19
September	9	1.81	0	0	0	0	0	0	0.41	0	0	0	0	0	0	0.01	0	0.03	0.17	0	0.3	0	0	0	0	0	0	0	0.01	0	0		2.74
October	10	0	0.18	0.13	0	0.23	0.01	0	0	0	0	0	0.02	0	0	0.48	0	0.02	0.1	0.17	0	0	0.1	0.02	0	0	0	0	0	0.13	0.02	0.74	2.35
November	11	0	0	0	0	0.21	0.23	0	0	0	0	0.06	0	0	0	0	0.08	0	0	0	0.07	0.37	0	0	0	0	0	0	0	0	0		1.02
December	12	0	0	0	0	0.11	0	0	0.05	0	0	0	0	0.36	0.41	0	0	0	0	0	0.03	0.9	0.1	0	0	0	0	0	0	0	0	0	1.96
2014 Totals	**2014**	**3.27**	**4.38**	**2.5**	**1.85**	**2.34**	**1.16**	**3.25**	**0.4**	**2.26**	**3.24**	**0.87**	**0.73**	**1.59**	**2**	**0.88**	**1.14**	**0.36**	**0.08**	**0**	**0.25**	**1.08**	**0.78**	**0.91**	**1.5**	**1.5**	**0.93**	**2.03**	**1.84**	**0**	**0.17**	**0.14**	**43.43**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0.11	0.09	0	0	0.64	0	0	0	0.07	0.55	0.02	0	0	0.01	0	0.03	0	0.06	0	0	0.09	0	0	0	0	0	0	0	0	0	0	1.67
Feburary	2	0.53	0	0	0.37	0.11	0	0	0.04	0.02	0	0	0	0	0.09	0	0	0.09	0	0	0.23	0	0	0	0	0	0	0	0				1.48
March	3	0	0.32	0	0	0	0	0	0	0	0	0.68	0.34	0	0	0	0	0	0.01	0	0	0	0	0	0	0	0.02	0.17	0.01	0	0	0	1.55
April	4	0.07	2.53	2.23	0	0	0	0.66	0	0	0	0	0	0.49	0.07	0	0	0	0	0	0	0.09	0	0	0.5	0	0	0.59	1.15	0	0		8.38
May	5	0	0	0	0	0	0	0	0.02	0	0.32	0.17	0.17	0.15	0.53	0.35	0	0	0	0	0	0.13	0	0	0	1.48	0.52	0	0	0	0	0.14	3.98
June	6	0	0	0	0.87	0	0	0.66	0	0.9	0.43	0	0.15	0	0	0	0	0	0	0	0	0.73	0	0.06	0.51	0	0	0.95	0	0	0		5.26
July	7	0.02	0	0	0	0	0	0	0.33	0	0	0	0	0.11	1.11	0	0	0	0	0	0	0	0	0	0	0.02	0	0	0	0	0	0	1.59
August	8	0	0	0	0	0.23	1.14	1.79	0.01	0.01	0	0	0	0	0	0.09	0.98	0.19	0	0	0.02	0	0	0	0	0	0.07	0.18	0.19	0	0.16	0	5.06
September	9	2.15	0.21	0	0	0.01	0.02	0	0	0.56	1.13	0	0.01	0	0	0.03	0	0.08	0	0	0	0	0	0	0	0	0	0	0	0	0		4.2
October	10	0.31	1.23	0.27	0	0	0	0.14	0	0.7	0.81	0	0.06	0.84	0.19	0.04	0	0	0	0	0	0	0	0	0	0	0	0	0.49	0	0	0	5.08
November	11	0	0	0	0.58	0	0	0	0	0	0	0	0	0	0	0.04	0.13	0	0	0	0	0.04	0.1	0.85	0.47	0	0.24	0	0	0	0.01		2.46
December	12	0.08	0	0	0.03	1.35	0	0	0	0	0	0	0	0	0	0.33	0	0	0.01	0	0	0	0.68	0	0.02	0	0.08	0.14	0	0	0	0	2.72
2015 Totals	**2015**	**1.58**	**0.69**	**1.03**	**0.19**	**6.52**	**0.17**	**1.89**	**4.46**	**3.06**	**1.89**	**1.31**	**0.12**	**1.92**	**3.02**	**0.6**	**2.27**	**2.16**	**1.4**	**3.01**	**0.97**	**1.26**	**0.91**	**1.16**	**0.83**	**2.58**	**6.46**	**3.71**	**3.95**	**1.24**	**0.66**	**0.22**	**61.24**
January	1	0.02	0.03	0.61	0.01	0	0.02	0.01	0	0	0	0.29	0.03	0	0	0	0	0	0	0	0	0	0	0	0	0.19	0	0	0	0	0	0	1.21
Feburary	2	0.66	0	0	0.06	0	0	0	0	0	0	0	0	0.01	0.14	0.25	0.02	0.01	0	0.14	0.09	0	0	0	0	0	0.05	0	0.31				1.74
March	3	0.04	0	0.12	0.01	0	0	0	0	0	0.2	0	0.02	1.1	0.15	0	0	0	0.03	0	0	0	0	0.13	0.59	0.52	0.07	0	0	0.02	0	0	3
April	4	0	0.61	0.3	0	0	0.01	1.76	0.48	1.14	0	0	0	0.06	0	0	0	0	0	0	0.77	0	0	0	0	0	0.29	0	0	0	0	0		5.42
May	5	0	0	0	0.01	0	0	0	0.3	0.32	0.55	0.55	0	0	0.05	0.35	0.09	0.15	0	0	0.24	0	0	0	0	0.24	0	0.15	0	0	0.08	0.54	0	3.62
June	6	0	0	0	0.1	1.9	0	0.06	1.32	0	0	0	0.07	0.02	2.43	0.11	0.75	0.08	0.87	1.33	0	0.38	0	0	0	1.57	1.11	0	1.02	0.02	0		13.14
July	7	0.86	0.04	0	0	0	0.14	0.06	1.01	0	0.77	0	0	0	0	0	0	0	0	0.45	0.56	0	0	0	0	0	0.21	0.03	0	0	0	0	4.13
August	8	0	0	0	0	3.25	0	0	0	1.49	0.05	0	0	0	0	0	0	0.06	0.45	0.46	0	0	0.91	0	0	0	0	0	0	0	0	0	6.67
September	9	0	0	0	0	0	0	0	1.35	0.11	0.32	0.3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1.03	0		3.11
October	10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.01	0	0.01	0	0	0	0.72	0.02	0	0	0.22	0.98
November	11	0	0	0	0	1.37	0	0	0	0	0	0.17	0	0	0	0	1.04	1.85	0.04	0	0.02	0.52	0	0	0	0.01	0	1.24	0.01	0.09	0.12		6.48
December	12	0	0.01	0	0	0	0	0	0	0	0	0	0	0.74	0.38	0	0.14	0	0	0	0.01	0.26	0	1.02	0	0	4.87	1.72	2.59	0	0	0	11.74
2016 Totals	**2016**	**0.44**	**2.57**	**2.83**	**0.62**	**0.17**	**1.08**	**0.64**	**0.65**	**2.24**	**3.89**	**2.59**	**0.91**	**0.95**	**0.67**	**2.62**	**1.75**	**0.58**	**0.31**	**3.35**	**1.97**	**0**	**0.16**	**0.37**	**0.63**	**1.92**	**2.27**	**1.49**	**0.3**	**0.73**	**2.13**	**0.61**	**41.44**
January	1	0	0	0	0	0	0	0.06	0.01	0.45	0	0	0	0	0	0.09	0	0.01	0	0.17	0.01	0	0	0	0	0	0	0	0	0	0	0	0.8
Feburary	2	0	0.15	0	0	0	0	0	0	0.01	0.06	0	0.03	0	0.16	0	0.06	0	0	0	0.02	0	0	0	0.31	0	0	0	0	0			0.8
March	3	0	0	0.05	0	0	0.01	0.04	0.07	0.05	0.19	0	0.05	0.12	0.14	0	0	0	0.1	0	0.12	0	0	0	0.16	0	0	0.23	0	0	0.41	0.55	2.29
April	4	0.04	0	0	0	0	0.36	0	0	0	0.18	0.99	0	0	0	0	0	0	0	0	0.22	0	0	0	0	0	1.07	0.14	0	0.37	1.12		4.49
May	5	0	0	0	0	0	0	0.05	0	0.29	0.14	1.59	0.04	0.12	0	0	0.37	0.51	0	0	0.01	0	0	0	0	0.01	0.53	1.01	0	0	0	0	4.67
June	6	0.09	0	0	0.24	0	0	0	0	0	0	0	0	0.12	0	0.01	0	0	0	0	0.03	0	0	0	0	0.42	0	0	0	0.38			1.29
July	7	0	0.15	1.11	0.11	0	0.52	0.49	0.18	0	1.91	0	0	0.57	0.01	0	0	0	0	0.7	0.97	0	0.07	0	0.16	1.21	0.15	0	0	0	0	0.06	8.37
August	8	0.31	0.16	0.96	0	0.17	0	0	0	0	0	0	0.73	0	0.36	2.52	0	0	0	0	0	0	0	0.03	0	0	0	0	0	0.35	0.18	0	5.77
September	9	0	0	0	0	0	0.19	0	0.32	1.44	1.41	0	0	0	0	0	1.32	0	0	0	0	0	0	0	0	0.14	0.08	0	0	0.01	0.04		4.95
October	10	0	0	0	0	0	0	0	0	0	0	0	0.06	0	0	0	0	0	0	2.48	0.59	0	0	0	0	0	0.02	0	0	0	0	0	3.15
November	11	0	2.11	0.71	0	0	0	0	0.07	0	0	0	0	0	0	0	0	0	0.21	0	0	0	0.09	0.15	0	0	0	0.11	0.28	0	0		3.73
December	12	0	0	0	0.27	0	0	0	0	0	0	0.01	0	0.02	0	0	0	0.06	0	0	0	0	0	0.19	0	0.14	0.42	0	0.02	0	0	0	1.13
2017 Totals	**2017**	**0.57**	**0.23**	**2.34**	**1.36**	**3.08**	**0.29**	**0.58**	**0.02**	**1.87**	**0.9**	**0.12**	**0.02**	**0.4**	**1.52**	**1.26**	**2.28**	**0.38**	**1.5**	**0.89**	**1.32**	**0.5**	**1.07**	**1.02**	**0.26**	**0.91**	**1.51**	**1.53**	**1.75**	**3.65**	**3.5**	**0.02**	**36.65**
January	1	0	0.22	0.04	0	0.04	0	0	0	0	0.01	0	0	0.16	0.64	0.21	0.11	0	0	0.37	0	0	0	0	0	0	0	0	0	0	0	0	1.8
Feburary	2	0	0	0	0	0	0.01	0.01	0.02	0	0	0	0	0	0	0	0	0	0	0	0	0.43	0	0	0	0	0	0.02	0				0.49
March	3	0.54	0	0	0	0	0	0.44	0	0.15	0	0.04	0	0.18	0	0	0	0.08	0	0	0	0	0	0.11	0.18	0.91	0	0.33	0	0.09	1.17	0.02	4.24
April	4	0	0.01	0.34	0.02	2.01	0.03	0	0	0	0.03	0	0	0	0.04	0	0.24	0.01	0	0	0	0.06	0.07	0	0	0	1.44	0.05	0.88	3.15	1.99		10.37
May	5	0.02	0	1.84	0.9	0	0	0	0	0	0.38	0.04	0	0	0	0	0	0	0	0.52	1.32	0	0	0.18	0	0	0	0.41	0	0.39	0	0	6
June	6	0	0	0	0.25	0	0	0	0	0	0	0	0	0	0.63	0.29	0	0.21	1.06	0	0	0	0	0	0	0	0	0	0	0.02	0.26		2.72
July	7	0	0	0	0	0.07	0.01	0	0	0	0	0	0	0.01	0.17	0	0.01	0	0	0	0	0	0.02	0.32	0	0	0.05	0.72	0	0	0	0	1.38
August	8	0	0	0	0	0.01	0.09	0	0	0	0	0.04	0	0	0.04	0	1.92	0.08	0	0	0	0	0.25	0	0	0	0	0	0.87	0	0	0	3.3
September	9	0	0	0	0.01	0	0	0	0	0	0	0	0.01	0.05	0	0	0	0	0.2	0	0	0	0	0	0	0	0	0	0	0	0		0.27
October	10	0	0	0.12	0.03	0.04	0.01	0.13	0	1.72	0.48	0	0	0	0	0.61	0	0	0	0	0	0.01	0.5	0.05	0	0	0	0	0	0	0.01	0	3.71
November	11	0.01	0	0	0	0.91	0.14	0	0	0	0	0	0.01	0	0	0.15	0	0	0.24	0	0	0	0	0	0	0	0	0	0	0	0.07		1.53
December	12	0	0	0	0.15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0.23	0.36	0.08	0	0.02	0	0	0	0	0	0.84
2018 Totals	**2018**	**2.64**	**1.06**	**1.26**	**0.56**	**1.01**	**0.84**	**1.97**	**0.98**	**0.91**	**1.11**	**0.31**	**0.31**	**1.47**	**1.51**	**1.21**	**0.34**	**0.1**	**1.69**	**2.45**	**3.17**	**0.49**	**1.41**	**1.03**	**3.66**	**0.58**	**2.44**	**3.06**	**0.42**	**1.6**	**0.2**	**2.81**	**42.6**

APPENDIX J. LAMBERT FIELD PRECIPITION
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	Grand Total
January	1	0	0	0	0	0	0	0.35	0	0	0	0.04	0	0	0.01	0.06	0	0	0	0	0	0	0.76	0.01	0	0	0	0	0	0	0	0	1.23
Feburary	2	0	0	0	0.01	0	0	0	0	0	0.03	0	0	0	0.13	0.26	0	0.1	0	0.89	1.04	0.29	0.26	0.31	1.73	0	0	0	0.2				5.25
March	3	0.27	0	0	0	0.62	0.04	0	0	0	0	0.27	0	0	0	0	0.34	0	0	1.43	0	0	0	0.26	0.81	0	1.01	1.12	0.02	0.79	0	0.14	7.12
April	4	0.28	0.45	0.19	0	0	0	0	0.01	0	0	0	0	0.97	0.28	0.01	0	0	0	0	0	0	0.02	0.07	0	0	0	0	0	0	0		2.28
May	5	0	0	1.02	0	0	0.01	0	0	0.17	0	0	0	0	0.15	0.03	0	0	1.61	0.07	0.37	0.12	0	0	0	0.13	0	1.33	0	0	0.04	0	5.05
June	6	0	0.31	0	0	0	0	0	0	0.43	0	0	0	0	0	0	0	0	0	0.03	0.92	0.01	0.37	0	0	0	0.82	0	0.2	0	0		3.09
July	7	0.59	0	0.05	0	0	0	0	0	0.25	0	0	0	0	0.28	0	0	0	0	0.02	0	0	0	0	0	0	0	0	0	0.2	0.01	0.6	2
August	8	0	0.19	0	0	0	0	0.46	0	0	0.98	0	0	0	0.05	0.45	0	0	0	0.01	0.75	0.02	0	0	1.12	0	0	0	0	0.61	0	0.02	4.66
September	9	0	0	0	0	0	0	0.66	0.92	0.02	0	0	0	0	0	0	0	0	0	0	0	0.05	0	0	0	0	0.35	0	0	0	0		2
October	10	0	0	0	0.07	0	0.68	0.5	0	0	0.1	0	0.22	0	0.1	0.02	0	0	0	0	0	0	0	0	0	0.22	0.24	0	0	0	0	1.05	3.2
November	11	0.72	0.11	0	0.35	0.39	0	0	0.05	0.04	0	0	0.09	0	0.09	0.21	0	0	0.08	0	0	0	0	0.38	0	0.23	0	0	0	0	0		2.74
December	12	0.78	0	0	0.13	0	0.11	0	0	0	0	0	0	0.5	0.42	0.17	0	0	0	0	0.09	0	0	0	0	0	0.02	0.61	0	0	0.15	1	3.98
2019 Totals	**2019**	**0**	**0**	**0.22**	**0**	**0.05**	**1.18**	**1.05**	**0**	**1.28**	**0.16**	**0.97**	**0.6**	**0.96**	**0**	**0.13**	**0**	**0.04**	**0.19**	**0.59**	**0.23**	**0**	**0.76**	**0.59**	**0.55**	**0.01**	**0**	**0**	**0.11**	**0**	**0.03**	**0**	**9.7**
January	1	0	0	0	0	0	0	0.1	0	0	0	0.65	0.45	0.03	0	0	0	0.03	0.19	0.24	0.05	0	0.76	0.33	0	0	0	0	0.07	0	0.03	0	2.93
Feburary	2	0	0	0	0	0.05	1.18	0.95	0	0	0.16	0.32	0.01	0	0	0.13	0	0.01	0	0.35	0.16	0	0	0.2	0	0	0	0	0.04				3.56
March	3	0	0	0.22	0	0	0	0	0	1.28	0	0	0.14	0.93	0	0	0	0	0	0	0.02	0	0	0.06	0.55	0.01	0	0					3.21
Grand Total		**91.25**	**97.21**	**107.39**	**103.61**	**109.25**	**83.31**	**82.72**	**95.99**	**100.64**	**121.2**	**114.64**	**94.32**	**95.47**	**110.49**	**104.07**	**100.38**	**91.45**	**98.44**	**117.29**	**104.24**	**90.72**	**93.86**	**103.87**	**101.88**	**114.3**	**113.3**	**106.45**	**96.03**	**81.88**	**102.44**	**63.78**	**3091.87**

APPENDIX K

SURFACE WATER FLOW

DRAFT

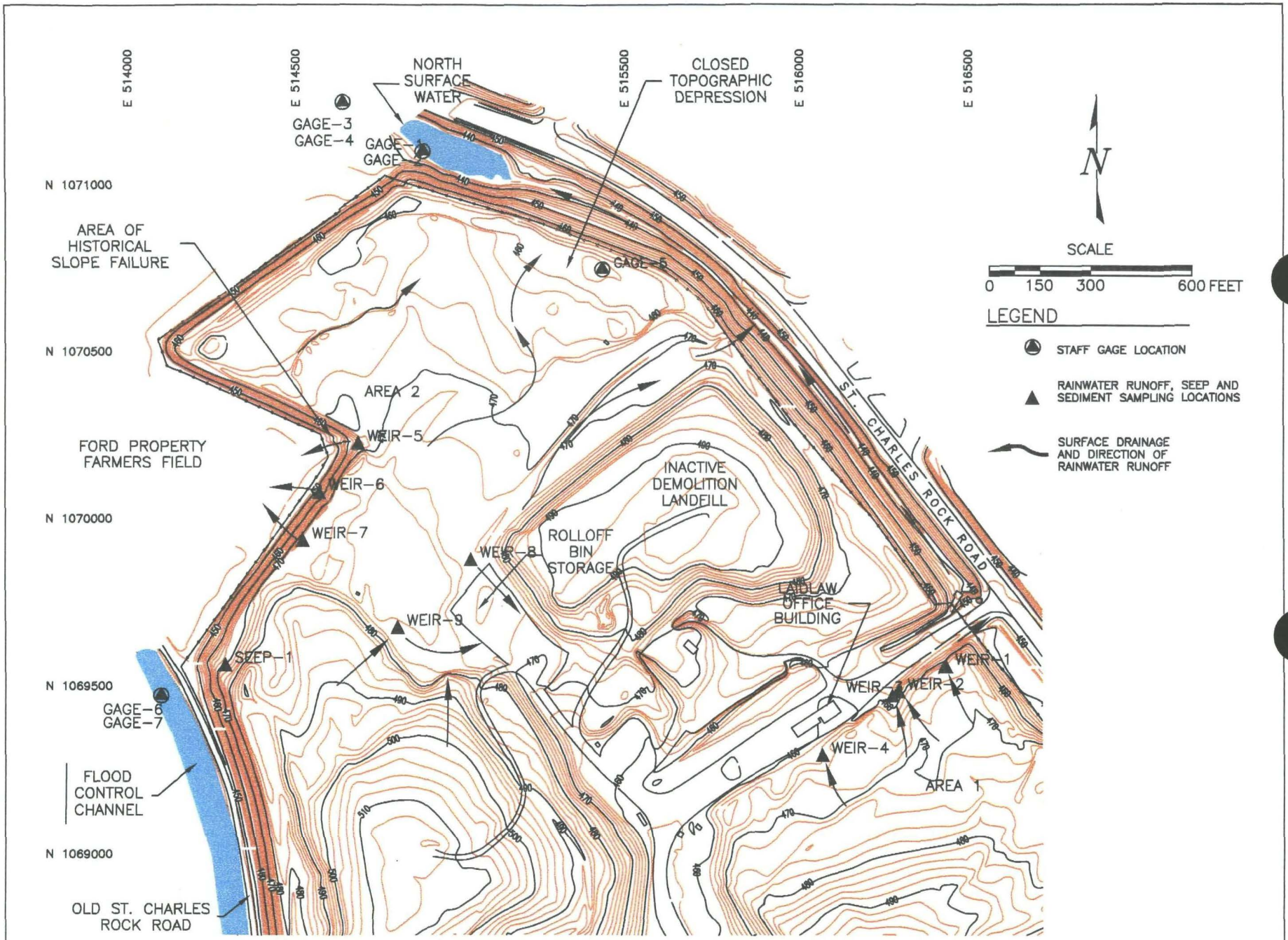


Figure 3-6: Area 1 and 2 Drainage Patterns and Runoff Locations

NORTH

0 100 200 425 850

Scale in Feet
Graphic Scale: 1 inch = 425 feet

EXPLANATION

→ Generalized Surface Water Flow Directions

BRIDGETON ACTIVE SANITARY LANDFILL BOUNDARY

BRIDGETON ACTIVE SANITARY LANDFILL BOUNDARY

ACTIVE SANITARY LANDFILL PERMIT No.118912

ST. CHARLES ROCK ROAD

ENTRANCE STATION

CLOSED DEMOLITION LANDFILL

CONCRETE PLANT

ASPHALT PLANT

BORROW AREA

LEACHATE LAGOONS (ABANDONED)

AUTO REPAIR FACILITY

APPROXIMATE LOCATION OF EDGE OF ALLUVIAL VALLEY

INACTIVE LANDFILL

CLOSED LEACHATE RETENTION POND

EARTH CITY INDUSTRIAL PARK STORM WATER RETENTION POND

EARTH CITY INDUSTRIAL PARK

NOTE: TOPOGRAPHY PROVIDED BY SURDEX, JANUARY 1995

© Allied Waste Industries (2005)

4630 South Highway 94
North Outer Road
St. Charles, Missouri 63304
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Fax (636) 939-9757

HERST & ASSOCIATES, INC.®

West Lake Landfill OU-2
Bridgeton, Missouri

Figure 2-1
Surface Water Drainage

APPENDIX K-2. SURFACE WATER ELEVATIONS
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

Location	Date	MPE (ft msl)	Reading (ft)	Comments	Elevation (ft msl)
SG-1	11/22/1994	438.57	-		-
SG-1	12/29/1994	438.57	-		-
SG-1	1/30/1995	438.57	-		-
SG-1	3/3/1995	438.57	-		-
SG-1	3/30/1995	438.57	-		-
SG-1	4/28/1995	438.57	-		-
SG-1	5/26/1995	438.57	-		-
SG-1	6/30/1995	438.57	4.2		437.27
SG-1	7/28/1995	438.57	3.25		436.32
SG-1	8/31/1995	438.57	2.35		435.42
SG-1	10/2/1995	438.57	-		-
SG-1	10/31/1995	438.57	1.5		434.57
SG-1	11/30/1995	438.57	-		-
SG-1	1/5/1996	438.57	-		-
SG-1	2/5/1996	438.57	dry		dry
SG-1	3/4/1996	438.57	dry		dry
SG-1	4/2/1996	438.57	dry		dry
SG-1	4/2/1996	438.57			-
SG-1	4/30/1996	438.57	0.5		433.57
SG-1	5/3/1996	438.57	dry		dry
SG-1	6/13/1996	438.57	3.1		436.17
SG-1	7/5/1996	438.57			435.37
SG-1	7/12/1996	438.57	2		435.07
SG-1	8/8/1996	438.57	1.4		434.47
SG-1	9/6/1996	438.57	dry		dry
SG-1	2/3/1997	438.57	dry		dry
SG-1	5/9/1997	438.57	2		435.07
SG-1	5/22/2000	438.57	dry		dry
SG-2	11/22/1994	438.84	-		-
SG-2	12/29/1994	438.84	-		-
SG-2	1/30/1995	438.84	-		-
SG-2	3/3/1995	438.84	-		-
SG-2	3/30/1995	438.84	-		-
SG-2	4/28/1995	438.84	-		-
SG-2	5/26/1995	438.84	-		-
SG-2	6/30/1995	438.84	3.95		437.29
SG-2	7/28/1995	438.84	3.05		436.39
SG-2	8/31/1995	438.84	2.1		435.44
SG-2	10/2/1995	438.84	-		-
SG-2	10/31/1995	438.84	1.25		434.59
SG-2	11/30/1995	438.84	-		-
SG-2	1/5/1996	438.84	-		-
SG-2	2/5/1996	438.84	dry		dry
SG-2	3/4/1996	438.84	dry		dry
SG-2	4/2/1996	438.84	dry		dry
SG-2	4/2/1996	438.84	-		-

APPENDIX K-2. SURFACE WATER ELEVATIONS
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

Location	Date	MPE (ft msl)	Reading (ft)	Comments	Elevation (ft msl)
SG-2	5/3/1996	438.84	dry		dry
SG-2	6/13/1996	438.84	2.9		436.24
SG-2	7/5/1996	438.84	2.25		435.59
SG-2	7/12/1996	438.84	1.8		435.14
SG-2	8/8/1996	438.84	1.2		434.54
SG-2	9/6/1996	438.84	dry		dry
SG-2	2/3/1997	438.84	dry		dry
SG-2	5/9/1997	438.84	1.85		435.19
SG-2	5/22/2000	438.84	dry		dry
SG-3	11/22/1994	440.73	-		-
SG-3	12/29/1994	440.73	-		-
SG-3	1/30/1995	440.73	-		-
SG-3	3/3/1995	440.73	-		-
SG-3	3/30/1995	440.73	-		-
SG-3	4/28/1995	440.73	-		-
SG-3	5/26/1995	440.73	-		-
SG-3	6/30/1995	440.73			437.21
SG-3	7/28/1995	440.73	1.05		436.28
SG-3	8/31/1995	440.73	-		-
SG-3	10/2/1995	440.73	-		-
SG-3	10/31/1995	440.73	3.2		438.43
SG-3	11/30/1995	440.73	-		-
SG-3	1/5/1996	440.73	-		-
SG-3	2/5/1996	440.73	dry		dry
SG-3	3/4/1996	440.73	dry		dry
SG-3	4/2/1996	440.73	dry		dry
SG-3	4/2/1996	440.73	-		-
SG-3	4/30/1996	440.73	dry		dry
SG-3	6/13/1996	440.73	1.9		437.13
SG-3	7/5/1996	440.73	-		-
SG-3	7/12/1996	440.73	-0.1		435.13
SG-3	8/8/1996	440.73	-0.7		434.53
SG-3	9/6/1996	440.73	dry		dry
SG-3	2/3/1997	440.73	dry		dry
SG-3	5/9/1997	440.73	dry		dry
SG-4	11/22/1994	441.05	-		-
SG-4	12/29/1994	441.05	-		-
SG-4	1/30/1995	441.05	-		-
SG-4	3/3/1995	441.05	-		-
SG-4	3/30/1995	441.05	-		-
SG-4	4/28/1995	441.05	-		-
SG-4	5/26/1995	441.05	-		-
SG-4	6/30/1995	441.05	1.7		437.25
SG-4	7/28/1995	441.05	0.8		436.35
SG-4	8/31/1995	441.05	-		-
SG-4	10/2/1995	441.05	-		-

APPENDIX K-2. SURFACE WATER ELEVATIONS
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

Location	Date	MPE (ft msl)	Reading (ft)	Comments	Elevation (ft msl)
SG-4	10/31/1995	441.05	2.95		438.5
SG-4	11/30/1995	441.05	-		-
SG-4	1/5/1996	441.05	-		-
SG-4	2/5/1996	441.05	dry		dry
SG-4	3/4/1996	441.05	dry		dry
SG-4	4/2/1996	441.05	dry		dry
SG-4	4/2/1996	441.05	-		-
SG-4	4/30/1996	441.05	-2.5		433.05
SG-4	5/3/1996	441.05	-3.5		432.05
SG-4	6/13/1996	441.05	1.7		437.25
SG-4	7/5/1996	441.05	-		-
SG-4	7/12/1996	441.05	-0.3		435.25
SG-4	8/8/1996	441.05	-0.9		434.65
SG-4	9/6/1996	441.05	dry		dry
SG-4	2/3/1997	441.05	dry		dry
SG-4	5/9/1997	441.05	dry		dry
SG-5	11/22/1994	460.94	-		-
SG-5	12/29/1994	460.94	-		-
SG-5	1/30/1995	460.94	-		-
SG-5	3/3/1995	460.94	-		-
SG-5	3/30/1995	460.94	-		-
SG-5	4/28/1995	460.94	-		-
SG-5	5/26/1995	460.94	-		-
SG-5	6/30/1995	460.94	-		-
SG-5	7/28/1995	460.94	-		-
SG-5	8/31/1995	460.94	-		-
SG-5	10/2/1995	460.94	-		-
SG-5	10/31/1995	460.94	-		-
SG-5	11/30/1995	460.94	-		-
SG-5	1/5/1996	460.94	-		-
SG-5	2/5/1996	460.94	dry		dry
SG-5	3/4/1996	460.94	dry		dry
SG-5	4/2/1996	460.94	dry		dry
SG-5	4/2/1996	460.94	-		-
SG-5	4/30/1996	460.94		0.02 below top of gauge	455.44
SG-5	5/3/1996	460.94		0.05 below top of gauge	455.44
SG-5	6/13/1996	460.94	2.4		457.84
SG-5	7/5/1996	460.94			-
SG-5	7/12/1996	460.94	dry		dry
SG-5	8/8/1996	460.94	dry		dry
SG-5	9/6/1996	460.94	dry		dry
SG-5	2/3/1997	460.94	dry		dry
SG-5	5/9/1997	460.94	dry		dry
SG-5	5/22/2000	460.94	dry		dry
SG-6	11/22/1994	437.28	-		-
SG-6	12/29/1994	437.28	-		-

APPENDIX K-2. SURFACE WATER ELEVATIONS
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

Location	Date	MPE (ft msl)	Reading (ft)	Comments	Elevation (ft msl)
SG-6	1/30/1995	437.28	-		-
SG-6	3/3/1995	437.28	-		-
SG-6	3/30/1995	437.28	-		-
SG-6	4/28/1995	437.28	-		-
SG-6	5/26/1995	437.28	-		-
SG-6	6/30/1995	437.28	2.18		433.96
SG-6	7/28/1995	437.28	2.63		434.41
SG-6	8/31/1995	437.28	1.55		433.33
SG-6	10/2/1995	437.28	-		-
SG-6	10/31/1995	437.28	0.25		432.03
SG-6	11/30/1995	437.28	0.7		432.48
SG-6	1/5/1996	437.28	-		-
SG-6	2/5/1996	437.28	dry		dry
SG-6	3/4/1996	437.28	dry		dry
SG-6	4/2/1996	437.28	dry		dry
SG-6	4/2/1996	437.28	-		-
SG-6	4/30/1996	437.28	0.9		432.68
SG-6	5/1/1996	437.28	1		432.78
SG-6	5/2/1996	437.28	1		432.78
SG-6	5/3/1996	437.28	1		432.78
SG-6	6/13/1996	437.28	1.7		433.48
SG-6	7/5/1996	437.28	1.75		433.53
SG-6	7/12/1996	437.28	1.8		433.58
SG-6	8/8/1996	437.28	1		432.78
SG-6	9/6/1996	437.28	dry		dry
SG-6	2/3/1997	437.28	0.6		432.38
SG-6	5/9/1997	437.28	1.65		433.43
SG-6	5/22/2000	437.28	dry		dry
SG-7	11/22/1994	437.01	-		-
SG-7	12/29/1994	437.01	-		-
SG-7	1/30/1995	437.01	-		-
SG-7	3/3/1995	437.01	-		-
SG-7	3/30/1995	437.01	-		-
SG-7	4/28/1995	437.01	-		-
SG-7	5/26/1995	437.01	-		-
SG-7	6/30/1995	437.01	2.45		433.96
SG-7	7/28/1995	437.01	2.95		434.46
SG-7	8/31/1995	437.01	1.8		433.31
SG-7	10/2/1995	437.01	0.3		431.81
SG-7	10/31/1995	437.01	-		-
SG-7	11/30/1995	437.01	1		432.51
SG-7	1/5/1996	437.01	-		-
SG-7	2/5/1996	437.01	dry		dry
SG-7	3/4/1996	437.01	dry		dry
SG-7	4/2/1996	437.01	dry		dry
SG-7	4/2/1996	437.01	-		-

APPENDIX K-2. SURFACE WATER ELEVATIONS
WEST LAKE LANDFILL OU-3
REMEDIAL INVESTIGATION/FEASIBILITY STUDY WORK PLAN

Location	Date	MPE (ft msl)	Reading (ft)	Comments	Elevation (ft msl)
SG-7	4/30/1996	437.01	1.1		432.61
SG-7	5/1/1996	437.01	1.2		432.71
SG-7	5/2/1996	437.01	1.2		432.71
SG-7	5/3/1996	437.01	1.2		432.71
SG-7	6/13/1996	437.01	1.9		433.41
SG-7	7/5/1996	437.01	2		433.51
SG-7	7/12/1996	437.01	2		433.51
SG-7	8/8/1996	437.01	1.2		432.71
SG-7	9/6/1996	437.01	0.4		431.91
SG-7	2/3/1997	437.01	0.8		432.31
SG-7	5/9/1997	437.01	2	gauge not secure	433.51
SG-7	5/22/2000	437.01	dry		dry
SG-8	2/5/1996		1.98	No survey data	
SG-8	3/4/1996		dry	No survey data	dry
SG-8	3/5/1996		1.6	No survey data	
SG-8	4/2/1996	435.38	3.52	Angled gauge	433.9893
SG-8	4/30/1996	435.38	2.5	Angled gauge	433.0308
SG-8	5/1/1996	435.38	2.57	Angled gauge	433.0965
SG-8	5/2/1996	435.38	2.57	Angled gauge	433.0965
SG-8	5/3/1996	435.38	2.54	Angled gauge	433.0684
SG-8	6/13/1996	435.38	3.38	Angled gauge	433.8577
SG-8	7/12/1996	435.38	3.39	Angled gauge	433.8671
SG-8	8/8/1996	435.38	2.64	Angled gauge	433.1623
SG-8	9/6/1996	435.38	dry	Angled gauge	dry
SG-8	2/3/1997	435.38	dry at 2.10	Angled gauge	dry
SG-8	5/9/1997	435.38	4.4	Angled gauge	434.8162
SG-9	4/2/1996	435.49	3.48		433.97
SG-9	4/30/1996	435.49	2.49		432.98
SG-9	5/1/1996	435.49	2.56		433.05
SG-9	5/2/1996	435.49	2.56		433.05
SG-9	5/3/1996	435.49	2.53		433.02
SG-9	6/13/1996	435.49	3.35		433.84
SG-9	7/12/1996	435.49	3.37		433.86
SG-9	8/8/1996	435.49	2.62		433.11
SG-9	9/6/1996	435.49	dry at 1.8		dry
SG-9	2/3/1997	435.49	dry at 2.08		dry
SG-9	5/9/1997	435.49	4.35		434.84

Notes:
MPE - measuring point elevation
ft msl - feet above mean sea level
ft - feet

APPENDIX L

AQUIFER TESTING SUMMARY

L-1. SLUG TESTING SUMMARY

L-2. PACKER TESTING SUMMARY

L-3. LABORATORY TESTING SUMMARY

DRAFT

APPENDIX L-1

SLUG TESTING SUMMARY

DRAFT

Aquifer Testing Results

Aquifer Test Results

West Lake Landfill, Bridgeton, Missouri

Monitoring Well	Hydraulic Conductivity K (cm/s) *		
Shallow Depth Wells			
S-1	3.78E-03		
S-5	8.76E-04	Max	3.43E-02
S-8	3.43E-02	Min	8.76E-04
S-84	2.32E-03	Avg	8.22E-03
MW-101	4.17E-03		
MW-F3	3.83E-03		
Intermediate Depth Wells			
I-2	3.27E-02		
I-4	5.41E-02	Max	6.68E-02
I-7	6.68E-02	Min	1.22E-02
I-9	5.47E-02	Avg	4.45E-02
I-11	4.63E-02		
I-68	1.22E-02		
Deep Depth Wells			
D-3	3.15E-02		
D-6	4.29E-02	Max	8.85E-02
D-12	4.14E-02	Min	4.50E-03
D-13	8.85E-02	Avg	4.28E-02
D-85	4.50E-03		
D-93	4.78E-02		

* All Hydraulic Conductivities were determined using the computer software program AQTESOLV ™ (Geraghty & Miller, Inc. 1989). A graph of the data points was assigned a best fit line that was visually positioned on the graph.

Equations for Determining Hydraulic Conductivity (K)
using the Bouwer and Rice method

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_o}{y_t}$$

where r_c = radius of well casing
L_e = length of well screen
y_o = displacement at time 0
y_t = displacement at time t

$$\ln\frac{R_e}{r_w} = \left[\left(\frac{1.1}{\ln\frac{L_w}{r_w}}\right) + \left(\frac{A + B\ln\left[\frac{(H-L_w)}{r_w}\right]}{\frac{L_e}{r_w}}\right)\right]^{-1}$$

where L_w = depth from potentiometric surface to bottom of well screen
r_w = radial distance from center of well to native aquifer sediments
H = saturated thickness of the aquifer
A and B = constants taken from a plot in article entitled "the Bouwer and Rice Slug Test - An Update" by Herman Bouwer from Ground Water May-June 1989 Vol. 27, No. 3.

A semi-logarithmic plot of y and t with a best fit line drawn through the data will be plotted. The straight line drawn through the data will allow for selection of y_o and y_t to be substituted into equation 1. See next page for this plot for well S-8. Note this is where the "double straight line effect" will skew the value of K if the wrong part of the double line is chosen.
The use of the Hermit Data recorder will allow for collection of data in more frequent steps and will allow for data to be taken at quicker intervals. This increase in data will help in the decision of which of the double lines is correct for the aquifer conditions.

RISING HEAD SLUG TEST
DATA RECORDED WITH THE TELOG WLS-2109E DATA RECORDER

DATE	TIME	MIN	AVG	MAX
12/12/95"	9:56:48	15.42	15.42	15.42
12/12/95"	9:56:49	14.96	14.96	14.96
12/12/95"	9:56:50	14.81	14.81	14.81
12/12/95"	9:56:51	14.96	14.96	14.96
12/12/95"	9:56:52	15.02	15.02	15.02
12/12/95"	9:56:53	15.33	15.33	15.33
12/12/95"	9:56:54	15.42	15.42	15.42
12/12/95"	9:56:55	15.39	15.39	15.39
12/12/95"	9:56:56	15.36	15.36	15.36
12/12/95"	9:56:57	15.37	15.37	15.37
12/12/95"	9:56:58	15.39	15.39	15.39

BOUWER AND RICE CALCUATION DATA

STATIC WATER LEVEL	13.02'
SCREEN LENGTH	20'
TOP OF SCREEN DEPTH	6.3'
BOTTOM OF SCREEN DEPTH	26.3'
BOTTOM OF AQUIFER DEPTH	109'
WELL DIAMETER	2"
DIAMETER OF FILTER PACK	4.25"

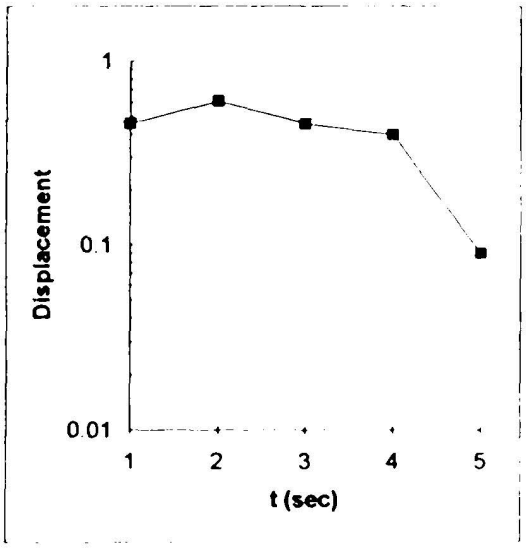
ASSUMPTIONS

Filter pack sand was placed through the middle of the auger flites as the augers were pulled from the ground.
Assume the borehole collapsed around the filter pack (see boring logs for the lithology of the native material) therefore the radial distance from the center of the well to the normal conductivity of the aquifer is 2.125"

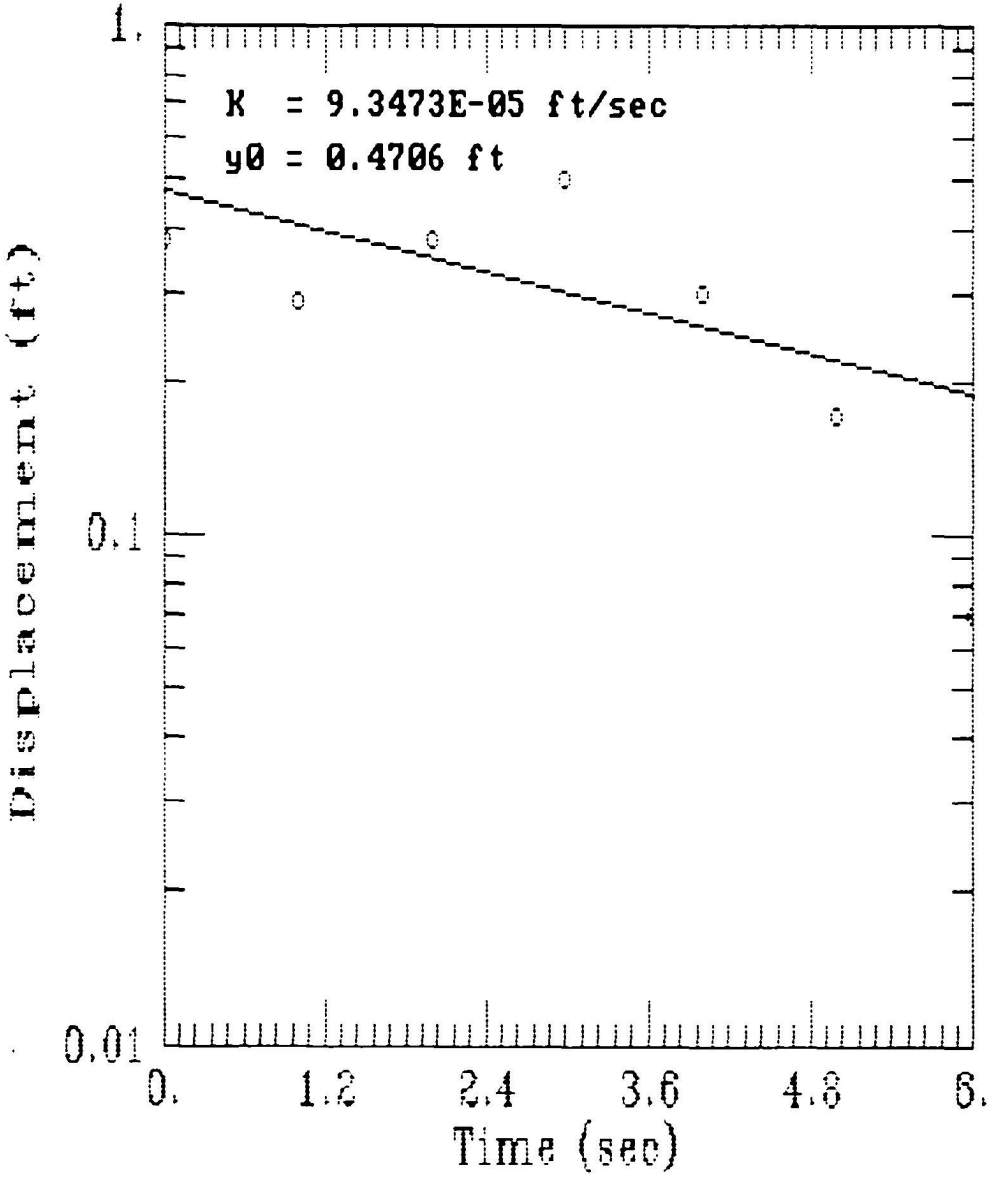
Notice the "double straight line effect" from time 2 to 4 seconds and again from 4 to 5 seconds. The data is too coarse to get the points in between these two intervals for correct best fit line interpretation. Without the best fit line, the correct value of K cannot be arrived at.

DATA USED IN PLOT

TIME	DISPACEMENT
1	0.46
2	0.61
3	0.46
4	0.4
5	0.09
6	0
7	0.03
8	0.03
9	0.02
10	0



S-8 SLUG TEST DATA W/TELOG RECORDER



AQTESOLV

GERAGHTY & MILLER, INC.

Modeling Group

APPENDIX C-2

SLUG TEST DATA

RISING HEAD TEST PZ-100-SS

WELL NO. PZ-100-SS

DATE	7/17/95	
INITIAL DEPTH TO WATER	69.61	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	72.8	FEET (btoc)
BOTTOM OF OPEN INTERVAL	96.0	FEET (btoc)
SATURATED THICKNESS	170	FEET
WATER TABLE TO BOTTOM OF SCREEN	26.39	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	23.2	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.30	FEET
MAX. HEAD IN SCREEN?	Y	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1025	0	72.91	0.0	3.30	1.00
1	1026	0	72.9	1.0	3.29	1.00
1	1031	0	72.89	6.0	3.28	0.99
1	1036	0	72.87	11.0	3.26	0.99
1	1041	0	72.85	16.0	3.24	0.98
1	1046	0	72.83	21.0	3.22	0.98
1	1051	0	72.82	26.0	3.21	0.97
1	1056	0	72.81	31.0	3.20	0.97
1	1131	0	72.78	66.0	3.17	0.96
1	1256	0	72.66	151.0	3.05	0.92
1	1405	0	72.58	220.0	2.97	0.90
1	1652	0	72.36	387.0	2.75	0.83
1	1825	0	72.44	480.0	2.83	0.86
2	647	45	71.81	1222.0	2.20	0.67

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-100-SS

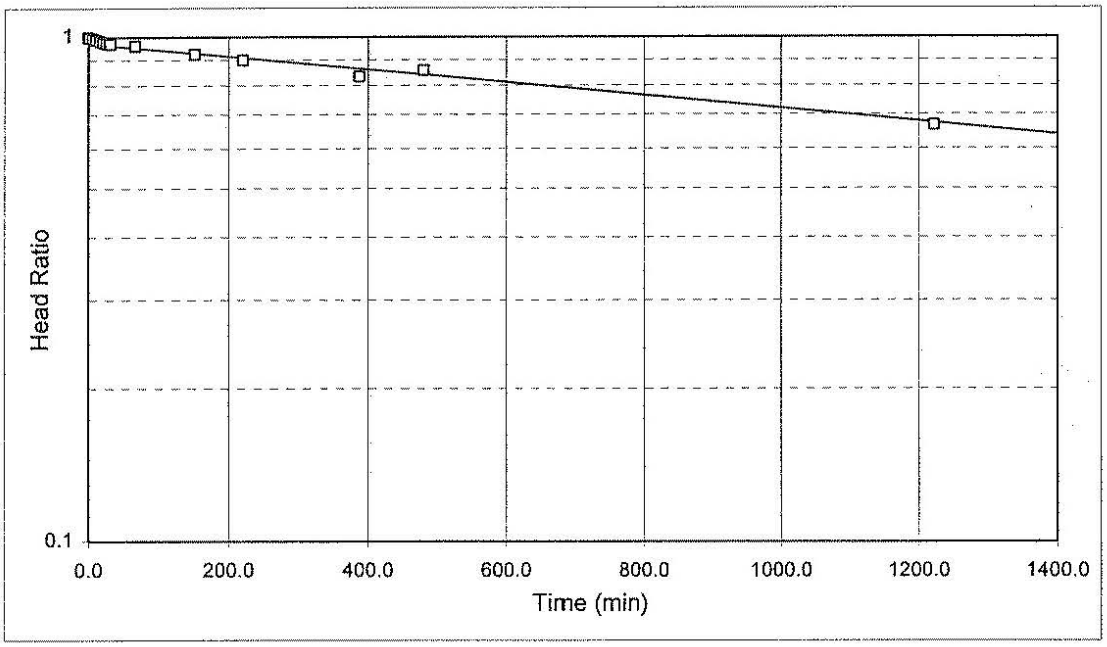
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	23.2
t_1 (min) =	0
t_2 (min) =	1400
h_1/h_0 =	0.97
h_2/h_0 =	0.64

RESULTS

K=	1.02E-07	cm/sec
K=	2.90E-04	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/17/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-100-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

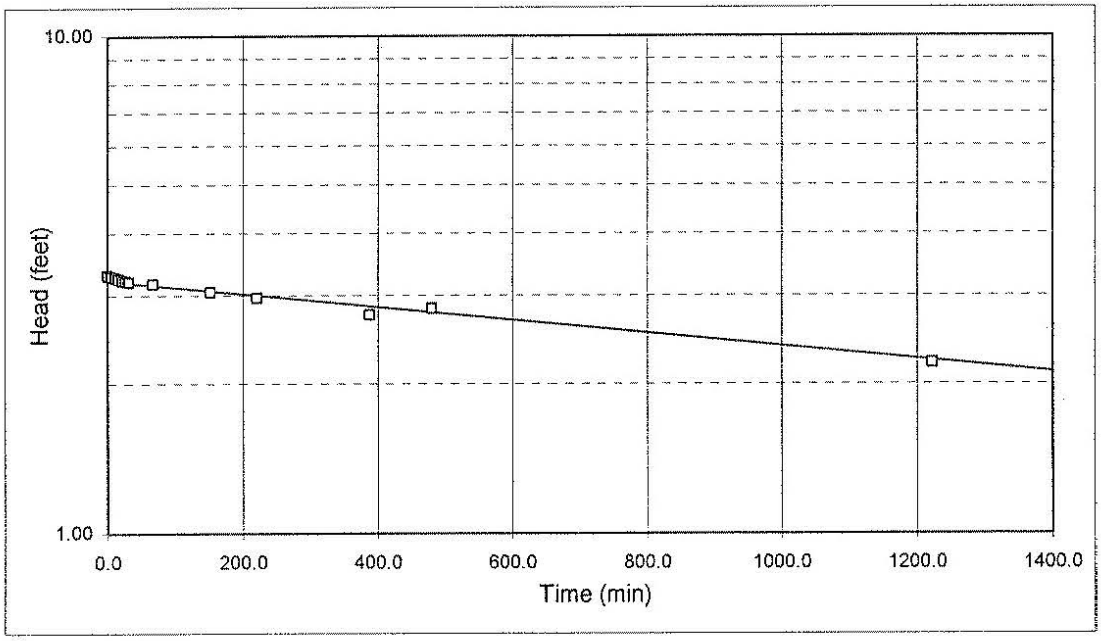
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.25
L_e =	23.2
$\ln(R_e/r_w)$	3.04
y_0 =	3.21
y_t =	2.11
t =	1400.0

RESULTS

K=	5.65E-08	cm/sec
K=	1.60E-04	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/17/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-100-SD

WELL NO. PZ-100-SD

DATE	7/31/95	
INITIAL DEPTH TO WATER	88.62	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	232.0	FEET (btoc)
BOTTOM OF OPEN INTERVAL	247.5	FEET (btoc)
SATURATED THICKNESS	160	FEET
WATER TABLE TO BOTTOM OF SCREEN	158.88	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	15.5	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	1.95	FEET
MAX. HEAD IN SCREEN?	N	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	733	0	90.57	0.0	1.95	1.00
1	734	0	90.57	1.0	1.95	1.00
1	735	0	90.56	2.0	1.94	0.99
1	740	0	90.53	7.0	1.91	0.98
1	745	0	90.51	12.0	1.89	0.97
1	750	0	90.44	17.0	1.82	0.93
1	907	0	90.2	94.0	1.58	0.81
1	1007	30	90.04	154.5	1.42	0.73
1	1150	30	89.78	257.5	1.16	0.59
1	1400	0	89.53	387.0	0.91	0.47
1	1553	0	89.33	500.0	0.71	0.36

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-100-SD

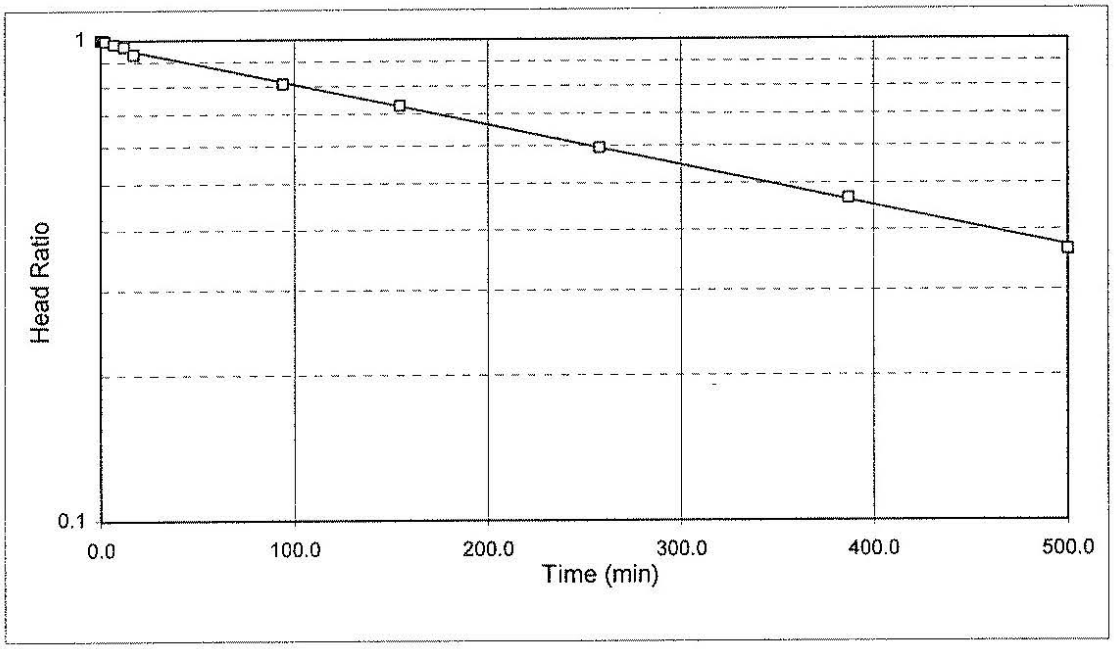
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where:
- r_c = casing radius (feet)
- R_e = filter pack radius (feet)
- L_e = length of screened interval (feet)
- t = time (seconds)
- h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	15.5
t_1 (min) =	0
t_2 (min) =	500
h_1/h_0 =	0.98
h_2/h_0 =	0.37

RESULTS

K=	9.11E-07	cm/sec
K=	2.58E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/31/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/19/96

BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-100-SD

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

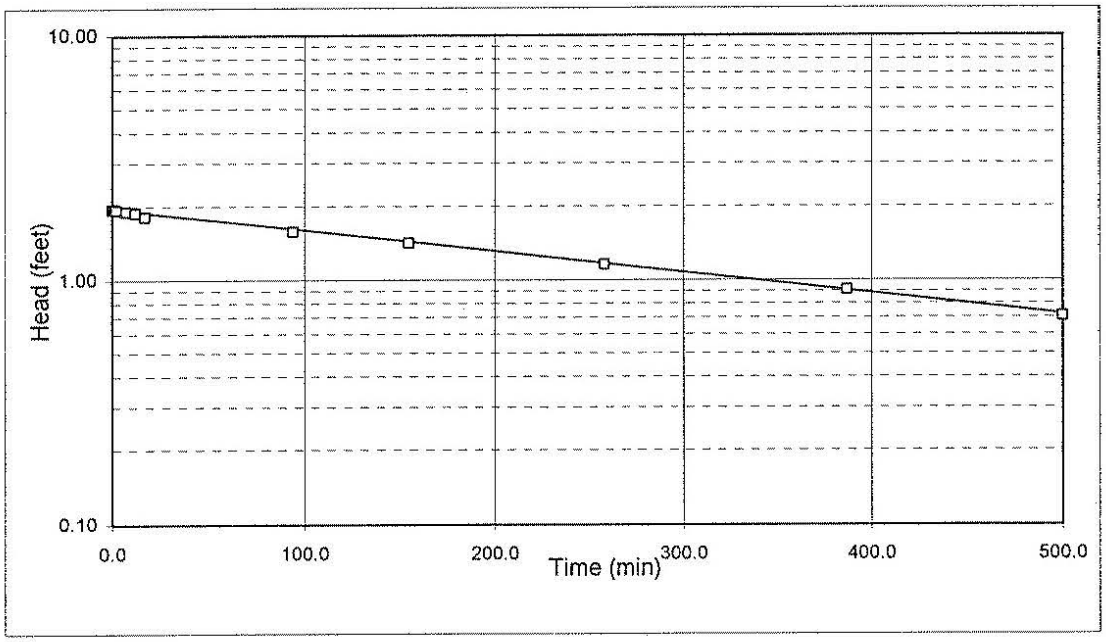
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.25
L_e =	15.5
$\ln(R_e/r_w)$	4.20
y_0 =	1.95
y_t =	0.72
t =	500.0

RESULTS

K=	6.36E-07	cm/sec
K=	1.80E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/31/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/19/96

RISING HEAD TEST PZ-100-KS

WELL NO PZ-100-KS

DATE	6/20/95	
INITIAL DEPTH TO WATER	48.1	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	368.9	FEET (btoc)
BOTTOM OF OPEN INTERVAL	387.9	FEET (btoc)
BOTTOM OF AQUIFER	519	FEET (btoc)
SATURATED THICKNESS	150	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	19	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.77	FEET
MAX. HEAD IN SCREEN?	N	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (SEC)	HEAD (FEET)	HEAD RATIO
1	741	0	51.87	0.0	3.77	1.00
1	742	0	51.8	60.0	3.70	0.98
1	749	0	51.7	480.0	3.60	0.95
1	755	23	51.6	863.0	3.50	0.93
1	801	45	51.5	1245.0	3.40	0.90
1	808	15	51.4	1635.0	3.30	0.88
1	816	20	51.3	2120.0	3.20	0.85
1	825	15	51.2	2655.0	3.10	0.82
1	1039	42	50.02	10722.0	1.92	0.51
1	1140	30	49.63	14370.0	1.53	0.41
1	1300	0	49.28	19140.0	1.18	0.31
1	1347	30	49.16	21990.0	1.06	0.28
1	1352	30	49.13	22290.0	1.03	0.27
1	1357	30	49.12	22590.0	1.02	0.27
1	1402	30	49.1	22890.0	1.00	0.27
1	1407	30	49.09	23190.0	0.99	0.26
1	1412	30	49.07	23490.0	0.97	0.26
1	1417	30	49.06	23790.0	0.96	0.25
1	1422	30	49.03	24090.0	0.93	0.25
1	1427	30	49.01	24390.0	0.91	0.24
1	1432	30	49	24690.0	0.90	0.24
1	1520	30	48.86	27570.0	0.76	0.20
1	1525	30	48.84	27870.0	0.74	0.20
1	1530	30	48.83	28170.0	0.73	0.19
1	1535	30	48.8	28470.0	0.70	0.19

COOPER-PAPADOPULOS SLUG TEST ANALYSIS
RISING HEAD TEST PZ-100-KS

$$K = \frac{r_c^{\,2}\beta}{tb} \qquad \text{and} \qquad S = \frac{r_c^{\,2}\alpha}{r_{ew}^{\,2}}$$

where:

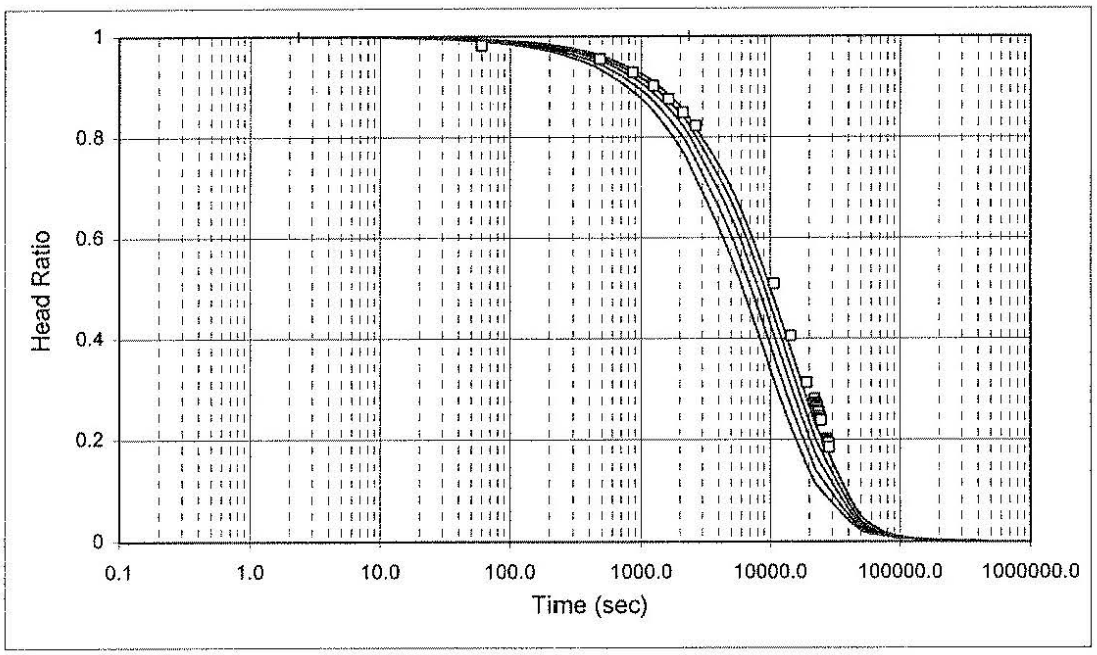
r_c = casing radius (feet)
r_{ew} = effective radius of screen (feet)
t = time (seconds)
K = Hydraulic conductivity (ft/sec)
$h_t/h_0 = F(\alpha,B)$

S = Storativity (dim)
h_t = Head at time t (feet)
b = Aquifer thickness (feet)

INPUT PARAMETERS	
r_c =	0.08
r_{ew} =	0.25
t =	2344.2
α =	1
B =	1E-09
b =	150.00

RESULTS

K=	6.02E-07	cm/sec
K=	0.002	ft/day
S =	1.11E-10	



Project Name: LAIDLAW / OU2 RIFS / MO
Project No.: 943-2848
Test Date: 06/20/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-101-SS

WELL NO. PZ-101-SS

DATE	6/20/95	
INITIAL DEPTH TO WATER	84.1	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	127.8	FEET (btoc)
BOTTOM OF OPEN INTERVAL	141.8	FEET (btoc)
SATURATED THICKNESS	150	FEET
WATER TABLE TO BOTTOM OF SCREEN	57.7	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	14	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	4.68	FEET
MAX. HEAD IN SCREEN?	N	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1101	45	88.78	0.0	4.68	1.00
1	1102	45	88.74	1.0	4.64	0.99
1	1103	45	88.73	2.0	4.63	0.99
1	1104	45	88.72	3.0	4.62	0.99
1	1105	45	88.69	4.0	4.59	0.98
1	1110	45	88.64	9.0	4.54	0.97
1	1115	45	88.58	14.0	4.48	0.96
1	1120	45	88.55	19.0	4.45	0.95
1	1125	45	88.5	24.0	4.40	0.94
1	1130	45	88.47	29.0	4.37	0.93
1	1150	0	88.3	48.3	4.20	0.90
1	1155	0	88.28	53.3	4.18	0.89
1	1200	0	88.22	58.3	4.12	0.88
1	1205	0	88.19	63.3	4.09	0.87
1	1210	0	88.16	68.3	4.06	0.87
1	1215	0	88.11	73.3	4.01	0.86
1	1220	0	88.07	78.2	3.97	0.85
1	1225	0	88.05	83.3	3.95	0.84
1	1230	0	88.01	88.3	3.91	0.84
1	1235	0	87.99	93.3	3.89	0.83
1	1240	0	87.95	98.3	3.85	0.82
1	1245	0	87.91	103.3	3.81	0.81
1	1316	30	87.67	134.8	3.57	0.76
1	1321	30	87.65	139.8	3.55	0.76
1	1438	30	87.38	216.8	3.28	0.70
1	1443	30	87.33	221.8	3.23	0.69
1	1448	30	87.32	226.8	3.22	0.69
1	1453	30	87.3	231.8	3.20	0.68
1	1458	30	87.28	236.8	3.18	0.68
1	1503	30	87.25	241.8	3.15	0.67

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-101-SS

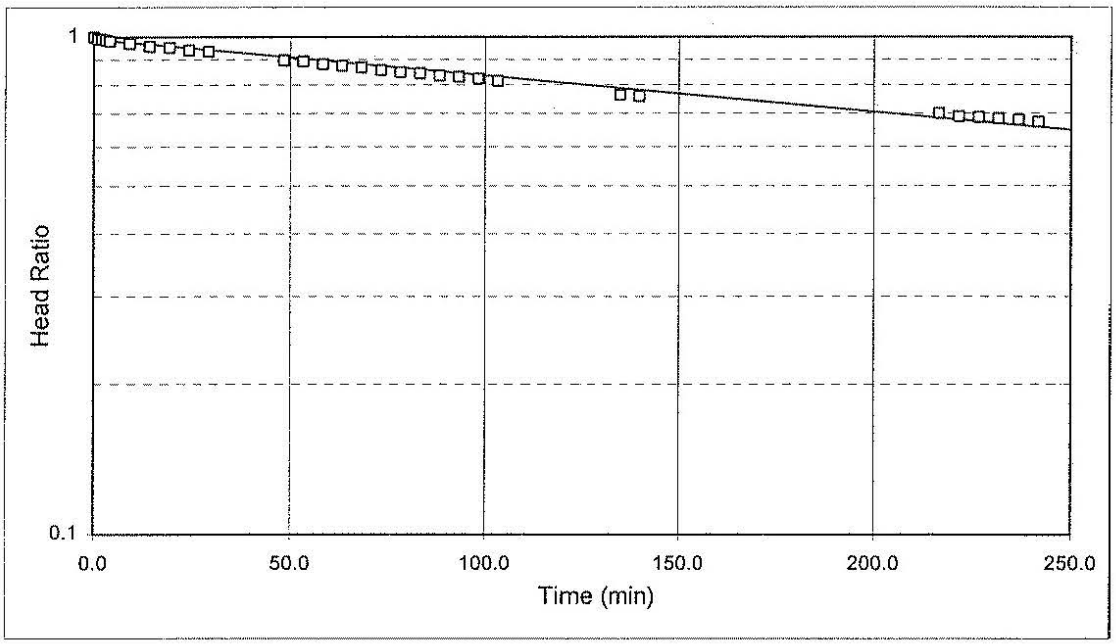
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	14
t_1 (min) =	0
t_2 (min) =	250
h_1/h_0 =	0.99
h_2/h_0 =	0.65

RESULTS

K=	8.58E-07	cm/sec
K=	2.43E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 06/20/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-101-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

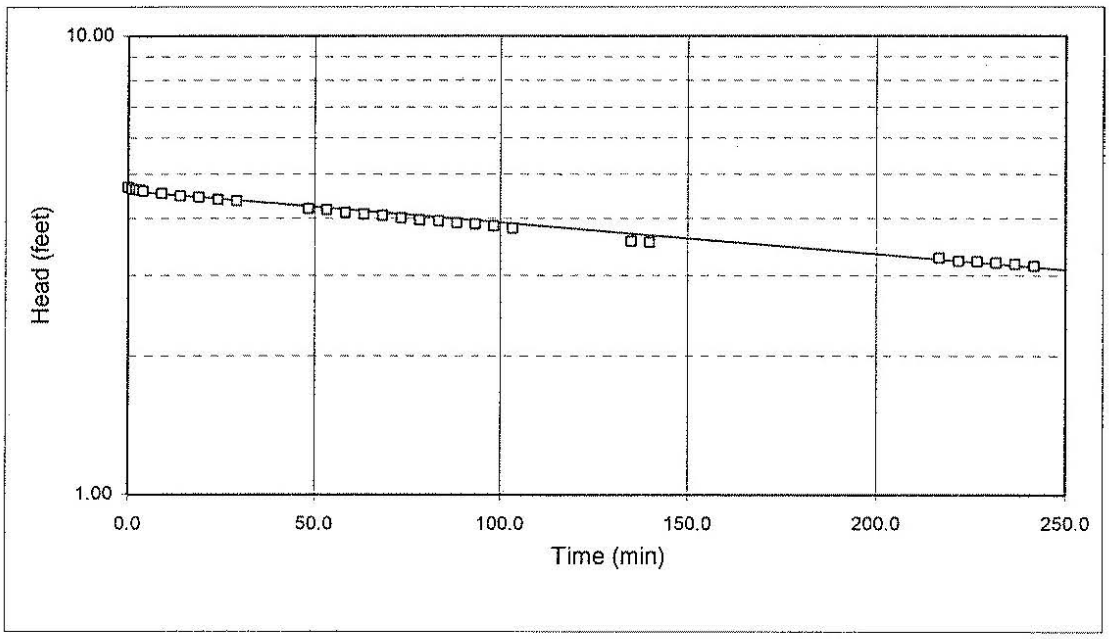
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.25
L_e =	14
$\ln(R_e/r_w)$	3.21
y_0 =	4.59
y_t =	3.09
t =	250.0

RESULTS

K=	5.10E-07	cm/sec
K=	1.45E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 06/20/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-102R-SS

WELL NO. PZ-102R-SS

DATE	7/24/95	
INITIAL DEPTH TO WATER	61.28	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	76.1	FEET (btoc)
BOTTOM OF OPEN INTERVAL	91.4	FEET (btoc)
SATURATED THICKNESS	180	FEET
WATER TABLE TO BOTTOM OF SCREEN	30.12	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	15.3	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.74	FEET
MAX. HEAD IN SCREEN?	N	

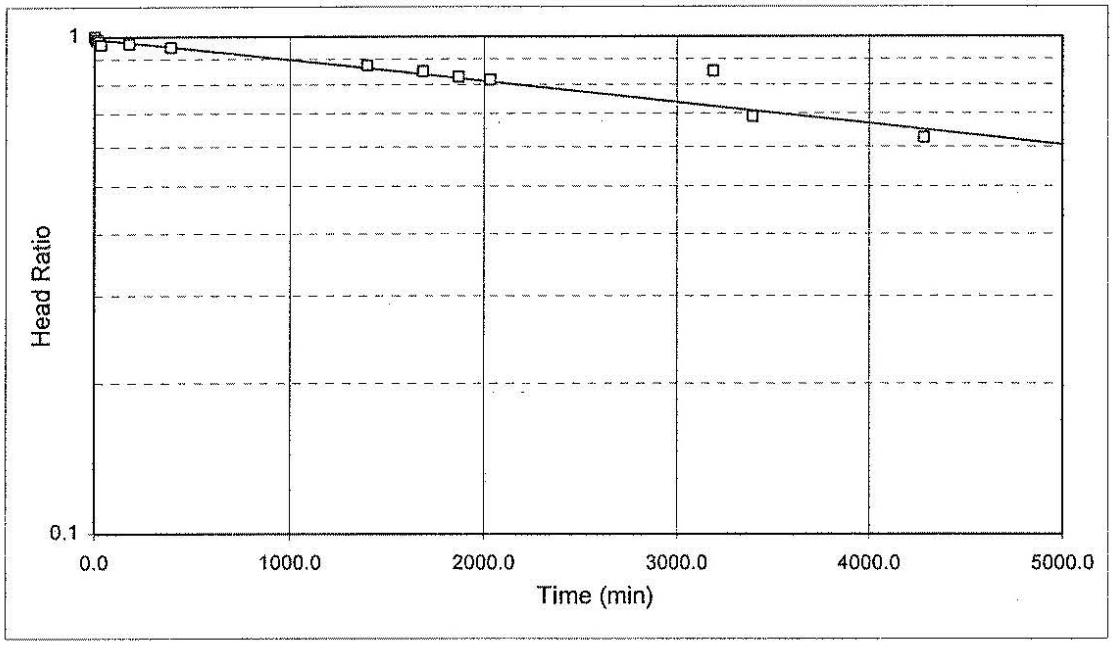
DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	803	30	65.02	0.0	3.74	1.00
1	805	0	65.02	1.5	3.74	1.00
1	810	0	64.97	6.5	3.69	0.99
1	815	0	64.96	11.5	3.68	0.98
1	820	0	64.96	16.5	3.68	0.98
1	825	0	64.94	21.5	3.66	0.98
1	835	0	64.88	31.5	3.60	0.96
1	1100	30	64.9	177.0	3.62	0.97
1	1432	0	64.84	388.5	3.56	0.95
2	719	0	64.55	1395.5	3.27	0.87
2	1205	0	64.46	1681.5	3.18	0.85
2	1512	0	64.38	1868.5	3.10	0.83
2	1756	0	64.34	2032.5	3.06	0.82
3	1314	0	64.46	3190.5	3.18	0.85
3	1639	0	63.86	3395.5	2.58	0.69
4	727	0	63.62	4283.5	2.34	0.63

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-102R-SS

$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
h_t = head at time t (feet)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
R_e =	0.25			
L_e =	15.3	K=	4.67E-08	cm/sec
t_1 (min) =	0	K=	1.32E-04	ft/day
t_2 (min) =	5000			
h_1/h_0 =	0.99			
h_2/h_0 =	0.61			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/24/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-102R-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

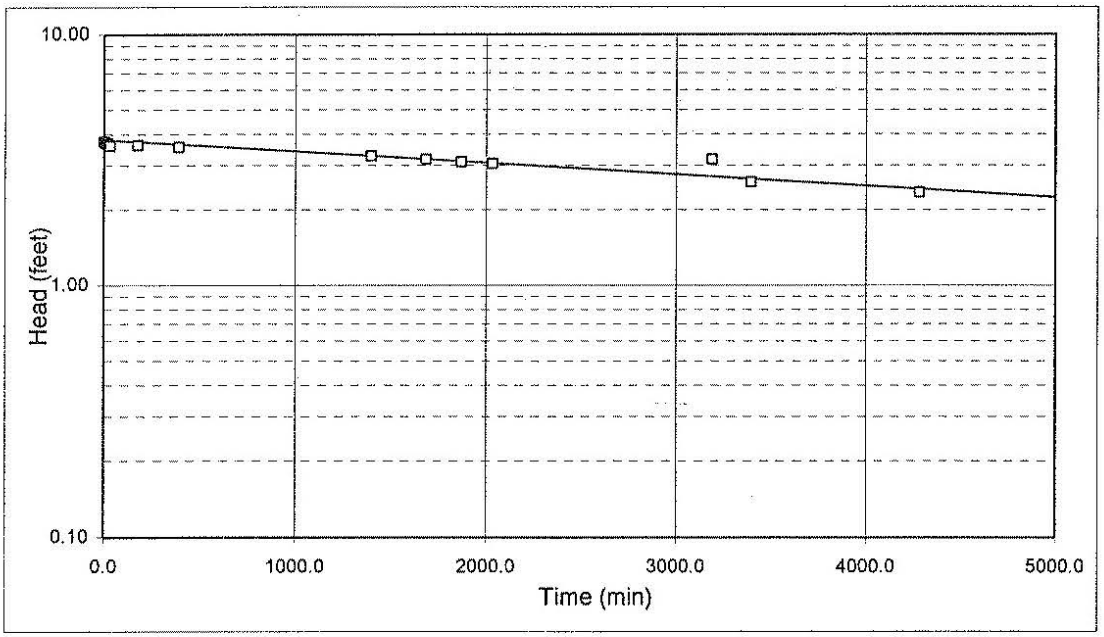
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.25
L_e =	15.3
$\ln(R_e/r_w)$	2.95
y_0 =	3.80
y_t =	2.24
t =	5000.0

RESULTS

K=	3.01E-08	cm/sec
K=	8.55E-05	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/24/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-103-SS

WELL NO. PZ-103-SS

DATE	7/17/95	
INITIAL DEPTH TO WATER	133.73	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	133.5	FEET (btoc)
BOTTOM OF OPEN INTERVAL	147.9	FEET (btoc)
SATURATED THICKNESS	130	FEET
WATER TABLE TO BOTTOM OF SCREEN	14.17	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	14.17	FEET
STATIC IN SCREEN?	Y	
MAX. HEAD CHANGE	4.09	FEET
MAX. HEAD IN SCREEN?	Y	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1208	30	137.82	0.0	4.09	1.00
1	1209	30	137.78	1.0	4.05	0.99
1	1214	30	137.65	6.0	3.92	0.96
1	1219	30	137.58	11.0	3.85	0.94
1	1224	30	137.51	16.0	3.78	0.92
1	1229	30	137.48	21.0	3.75	0.92
1	1234	30	137.45	26.0	3.72	0.91
1	1239	30	137.41	31.0	3.68	0.90
1	1244	30	137.38	36.0	3.65	0.89
1	1410	30	136.98	122.0	3.25	0.79
1	1520	0	136.71	191.5	2.98	0.73
1	1644	0	136.05	275.5	2.32	0.57
1	1821	0	135.83	372.5	2.10	0.51

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-103-SS

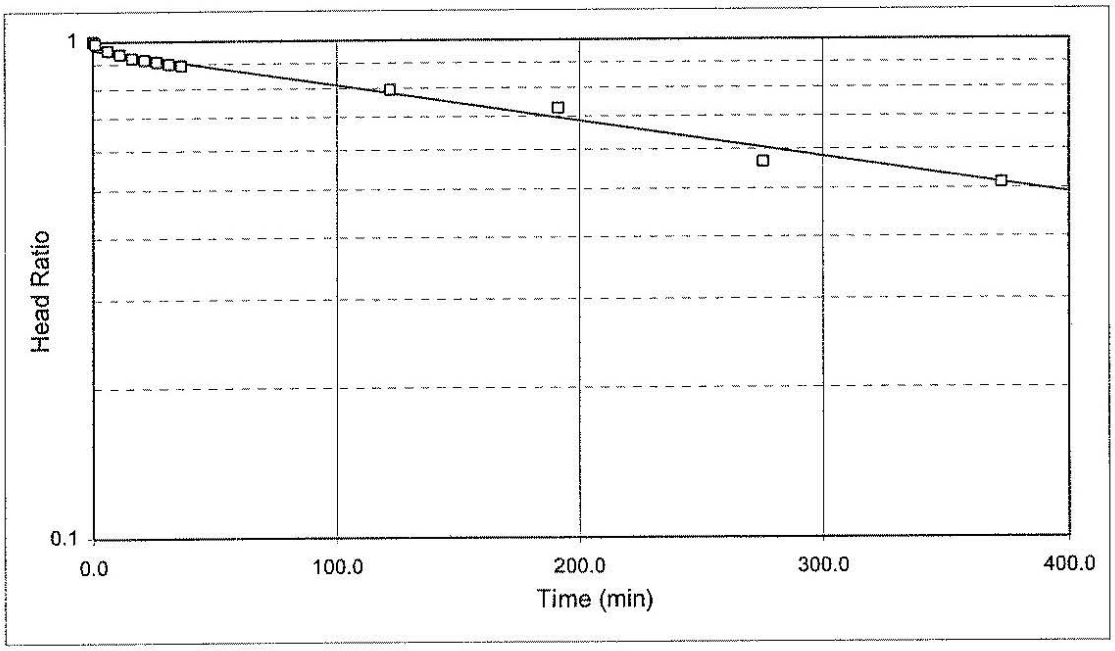
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
y_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	14.17
t_1 (min) =	0
t_2 (min) =	400
h_1/h_0 =	0.96
h_2/h_0 =	0.49

RESULTS

K=	8.43E-07	cm/sec
K=	2.39E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/17/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-103-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

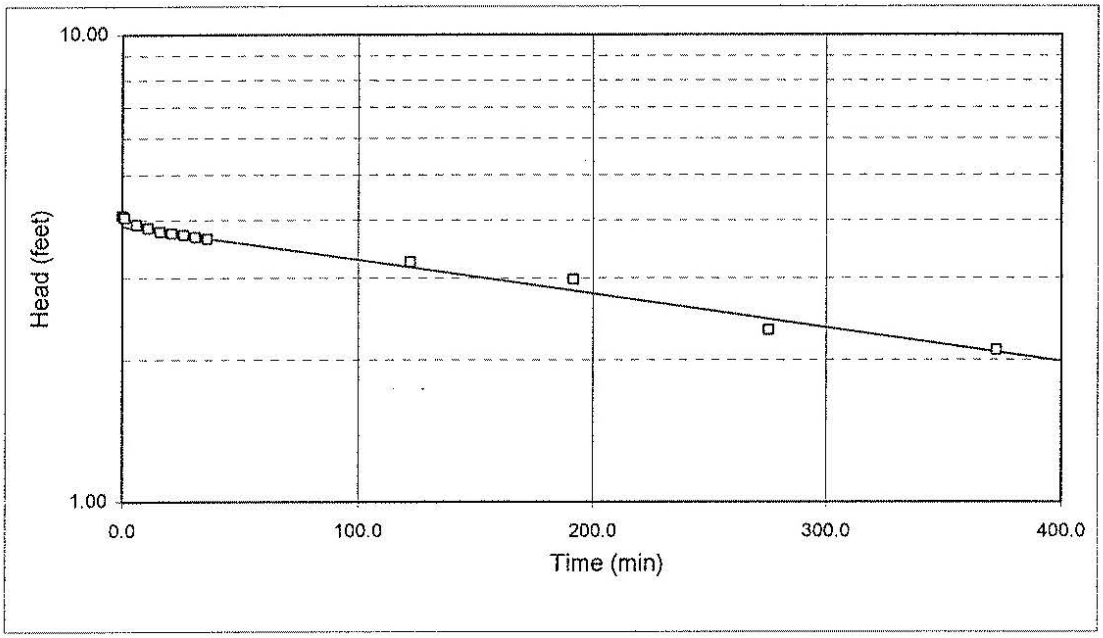
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.15
r_w =	0.25
L_e =	14.17
$\ln(R_e/r_w)$	2.61
y_0 =	3.88
y_t =	1.99
t =	400.0

RESULTS

K=	1.66E-06	cm/sec
K=	4.72E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/17/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-104-SS

WELL NO. PZ-104-SS

DATE	7/19/95	
INITIAL DEPTH TO WATER	132.18	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	132.6	FEET (btoc)
BOTTOM OF OPEN INTERVAL	147.1	FEET (btoc)
SATURATED THICKNESS	130	FEET
WATER TABLE TO BOTTOM OF SCREEN	14.92	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	14.5	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.24	FEET
MAX. HEAD IN SCREEN?	Y	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1237	0	135.42	0.0	3.24	1.00
1	1238	0	135.38	1.0	3.20	0.99
1	1243	0	135.3	6.0	3.12	0.96
1	1248	0	135.21	11.0	3.03	0.94
1	1253	0	135.17	16.0	2.99	0.92
1	1258	0	135.1	21.0	2.92	0.90
1	1439	0	134.73	122.0	2.55	0.79
1	1537	0	134.61	180.0	2.43	0.75
1	1637	0	134.48	240.0	2.30	0.71

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-104-SS

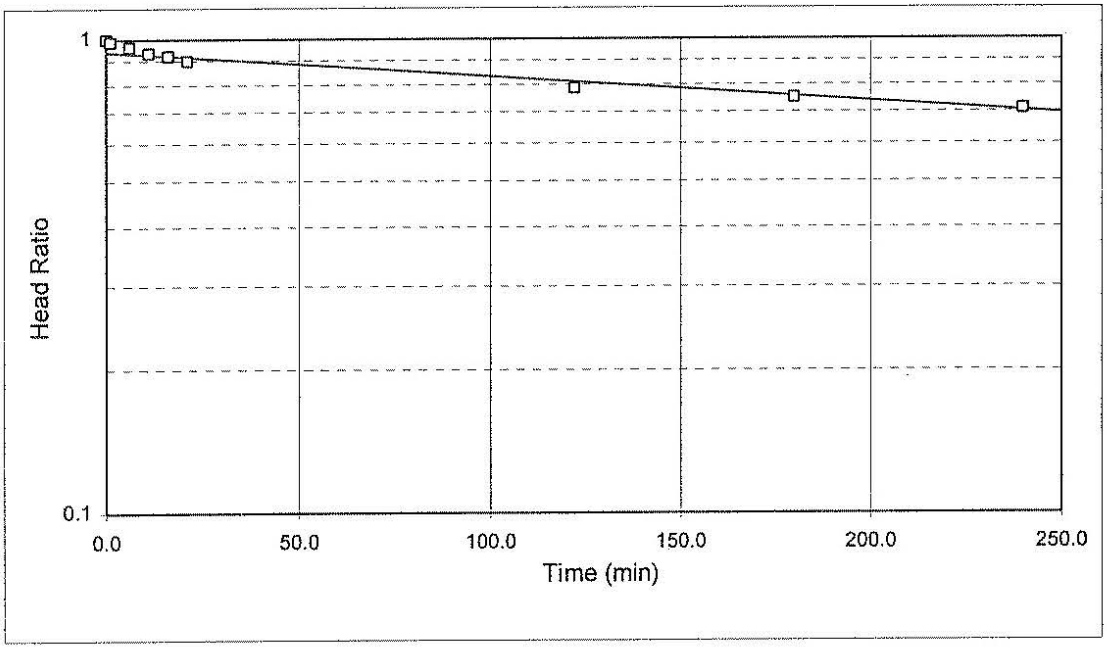
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	14.5
t_1 (min) =	0
t_2 (min) =	250
h_1/h_0 =	0.94
h_2/h_0 =	0.70

RESULTS

K=	5.97E-07	cm/sec
K=	1.69E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/19/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

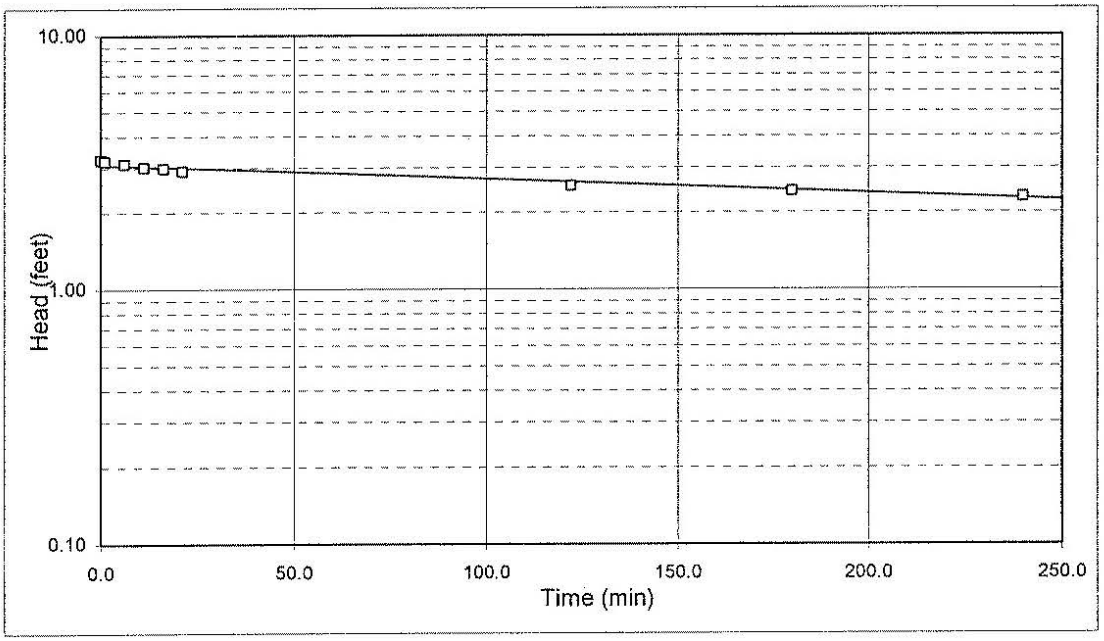
BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-104-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.15			
r_w =	0.25			
L_e =	14.5	K=	1.26E-06	cm/sec
$\ln(R_e/r_w)$	2.64	K=	3.57E-03	ft/day
y_0 =	3.09			
y_t =	2.24			
t =	250.0			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/19/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-104-SD

WELL NO. PZ-104-SD

DATE	7/20/95	
INITIAL DEPTH TO WATER	126.54	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	232.1	FEET (btoc)
BOTTOM OF OPEN INTERVAL	248.6	FEET (btoc)
SATURATED THICKNESS	125	FEET
WATER TABLE TO BOTTOM OF SCREEN	122.06	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	16.5	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	2.91	FEET
MAX. HEAD IN SCREEN?	N	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	852	0	129.45	0.0	2.91	1.00
1	854	0	129.26	2.0	2.72	0.93
1	855	0	129.17	3.0	2.63	0.90
1	857	0	128.96	5.0	2.42	0.83
1	858	0	128.84	6.0	2.30	0.79
1	859	0	128.77	7.0	2.23	0.77
1	900	0	128.69	8.0	2.15	0.74
1	905	0	128.3	13.0	1.76	0.60
1	910	0	127.99	18.0	1.45	0.50
1	915	0	127.73	23.0	1.19	0.41
1	920	0	127.49	28.0	0.95	0.33
1	927	0	126.96	35.0	0.42	0.14
1	932	0	126.72	40.0	0.18	0.06
1	937	0	126.62	45.0	0.08	0.03
1	942	0	126.62	50.0	0.08	0.03

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-104-SD

$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

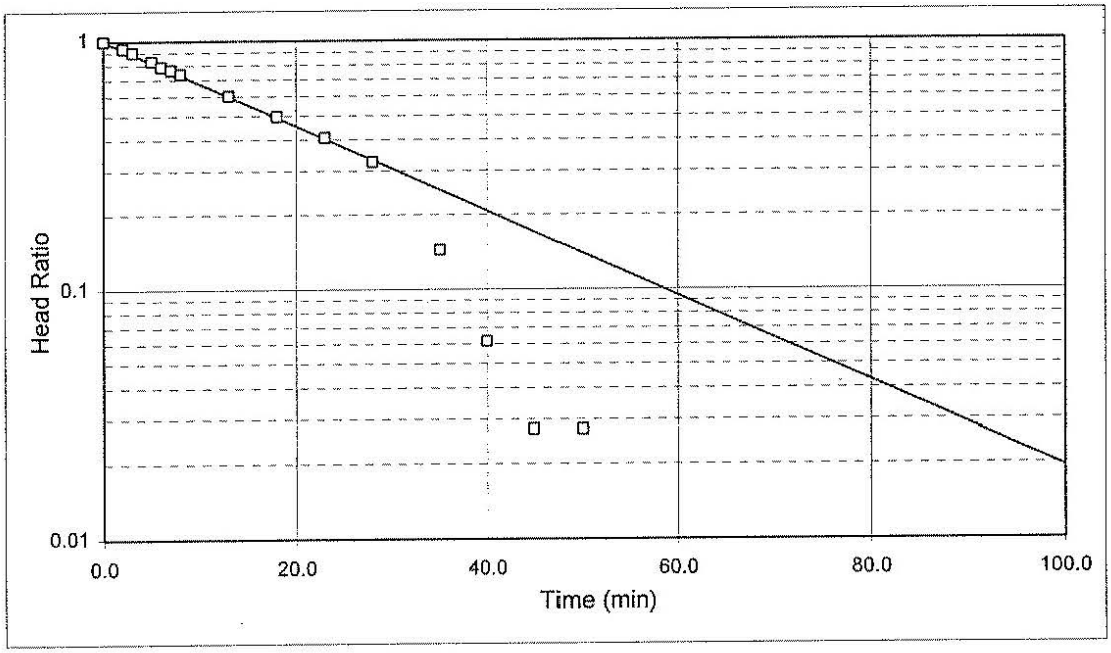
125

where:
- r_c = casing radius (feet)
- R_e = filter pack radius (feet)
- L_e = length of screened interval (feet)
- t = time (seconds)
- h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	16.5
t_1 (min) =	0
t_2 (min) =	100
h_1/h_0 =	1.00
h_2/h_0 =	0.02

RESULTS

K=	1.76E-05	cm/sec
K=	5.00E-02	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/20/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-104-SD

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_o}{y_t}$$

125

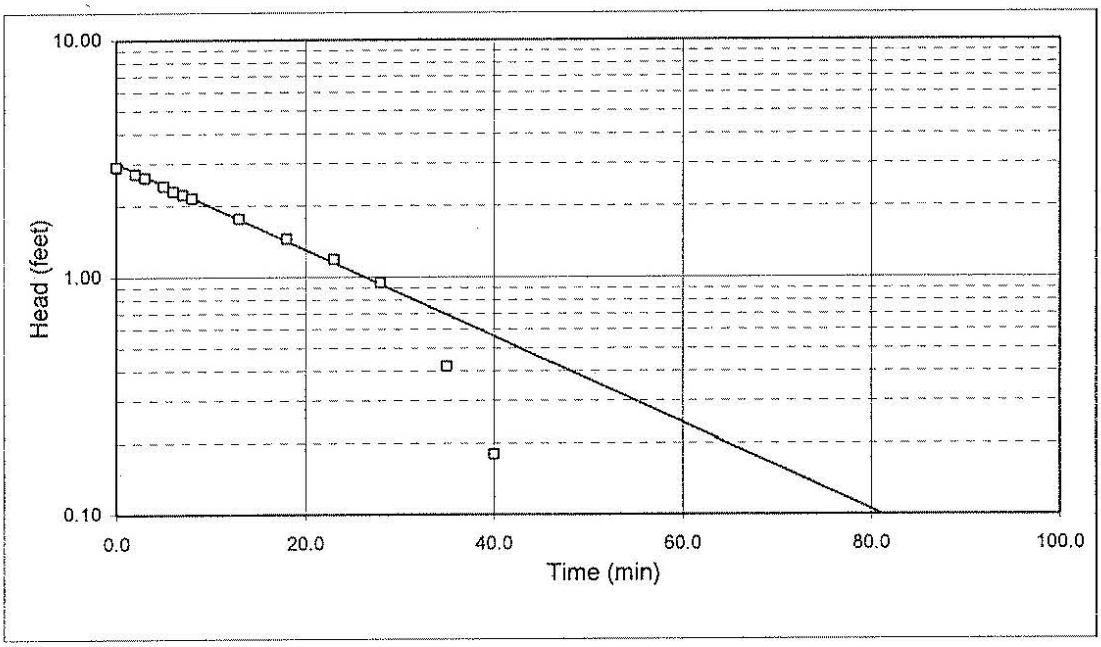
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.25
L_e =	16.5
$\ln(R_e/r_w)$	3.98
y_0 =	3.02
y_t =	0.10
t =	81.1

RESULTS

K=	1.24E-05	cm/sec
K=	3.52E-02	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/20/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-104-KS

WELL NO PZ-104-KS

DATE	7/20/95	
INITIAL DEPTH TO WATER	39.16	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	394.7	FEET (btoc)
BOTTOM OF OPEN INTERVAL	409.7	FEET (btoc)
BOTTOM OF AQUIFER	500	FEET (btoc)
SATURATED THICKNESS	370.54	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	15	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.36	FEET
MAX. HEAD IN SCREEN?	N	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (SEC)	HEAD (FEET)	HEAD RATIO
1	757	0	42.52	0.0	3.36	1.00
1	758	0	42.38	60.0	3.22	0.96
1	759	0	42.22	120.0	3.06	0.91
1	800	0	42.08	180.0	2.92	0.87
1	801	0	41.96	240.0	2.80	0.83
1	802	0	41.83	300.0	2.67	0.79
1	803	0	41.72	360.0	2.56	0.76
1	804	0	41.61	420.0	2.45	0.73
1	805	0	41.49	480.0	2.33	0.69
1	810	0	41.04	780.0	1.88	0.56
1	815	0	40.67	1080.0	1.51	0.45
1	820	0	40.37	1380.0	1.21	0.36
1	825	0	40.14	1680.0	0.98	0.29
1	832	0	39.89	2100.0	0.73	0.22
1	837	0	39.74	2400.0	0.58	0.17
1	842	0	39.61	2700.0	0.45	0.13
1	847	0	39.54	3000.0	0.38	0.11
1	856	0	39.4	3540.0	0.24	0.07
1	903	30	39.35	3990.0	0.19	0.06
1	916	0	39.25	4740.0	0.09	0.03

COOPER-PAPADOPULOS SLUG TEST ANALYSIS
RISING HEAD TEST PZ-104-KS

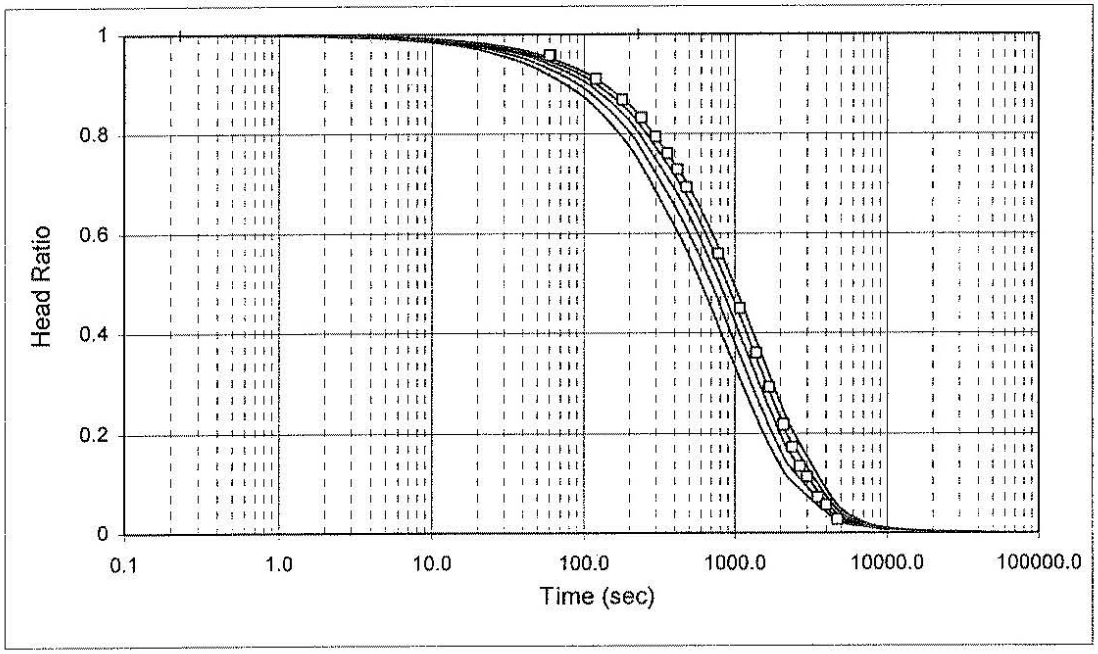
$$K = \frac{r_c^{\,2}\beta}{tb} \qquad \text{and} \qquad S = \frac{r_c^{\,2}\alpha}{r_{ew}^{\,2}}$$

where:

r_c = casing radius (feet)
r_{ew} = effective radius of screen (feet)
t = time (seconds)
K = Hydraulic conductivity (ft/sec)
$h_t/h_0 = F(\alpha,B)$

S = Storativity (dim)
h_t = Head at time t (feet)
b = Aquifer thickness (feet)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
r_{ew} =	0.25			
t =	229.1	K=	2.49E-06	cm/sec
α =	1	K=	0.007	ft/day
B =	1E-09	S =	1.11E-10	
b =	370.54			



Project Name: LAIDLAW / OU2 RIFS / MO
Project No.: 943-2848
Test Date: 07/20/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-105-SS

WELL NO. PZ-105-SS

DATE	7/20/95	
INITIAL DEPTH TO WATER	144.29	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	137.2	FEET (btoc)
BOTTOM OF OPEN INTERVAL	151.4	FEET (btoc)
SATURATED THICKNESS	500	FEET
WATER TABLE TO BOTTOM OF SCREEN	7.11	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	7.11	FEET
STATIC IN SCREEN?	Y	
MAX. HEAD CHANGE	1.56	FEET
MAX. HEAD IN SCREEN?	Y	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1300	30	145.85	0.0	1.56	1.00
1	1301	30	145.83	1.0	1.54	0.99
1	1302	30	145.8	2.0	1.51	0.97
1	1303	30	145.76	3.0	1.47	0.94
1	1305	0	145.73	4.5	1.44	0.92
1	1310	0	145.7	9.5	1.41	0.90
1	1315	0	145.64	14.5	1.35	0.87
1	1320	0	145.59	19.5	1.30	0.83
1	1325	0	145.53	24.5	1.24	0.79
1	1402	0	145.38	61.5	1.09	0.70
1	1435	0	145.34	94.5	1.05	0.67

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-105-SS

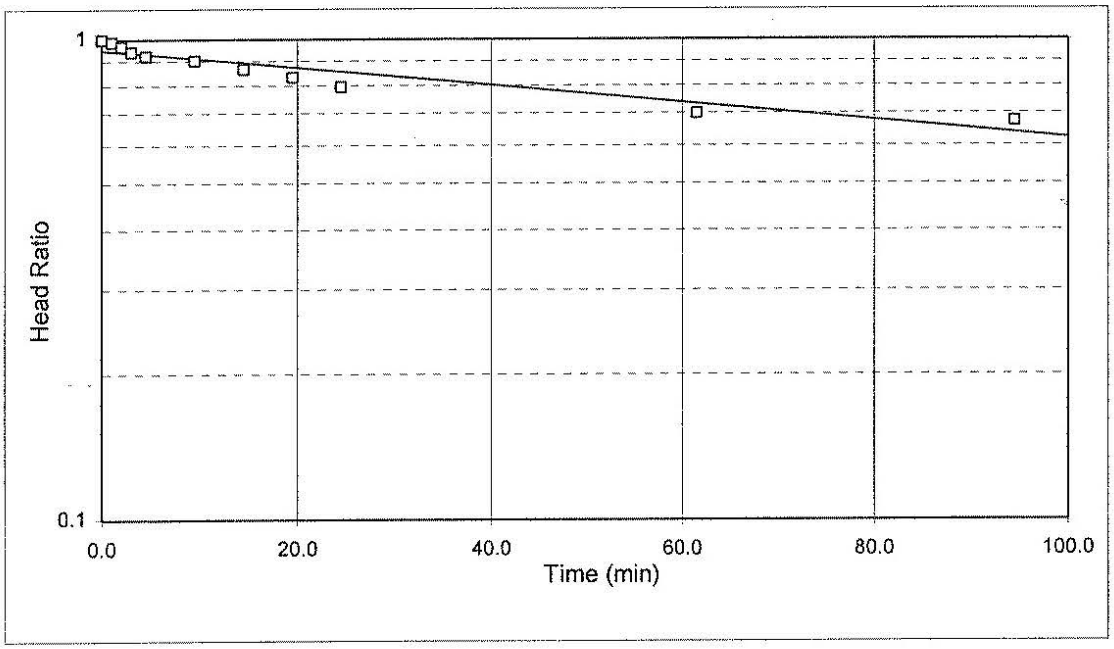
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	7.11
t_1 (min) =	0
t_2 (min) =	100
h_1/h_0 =	0.95
h_2/h_0 =	0.62

RESULTS

K=	3.51E-06	cm/sec
K=	9.96E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/20/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-105-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

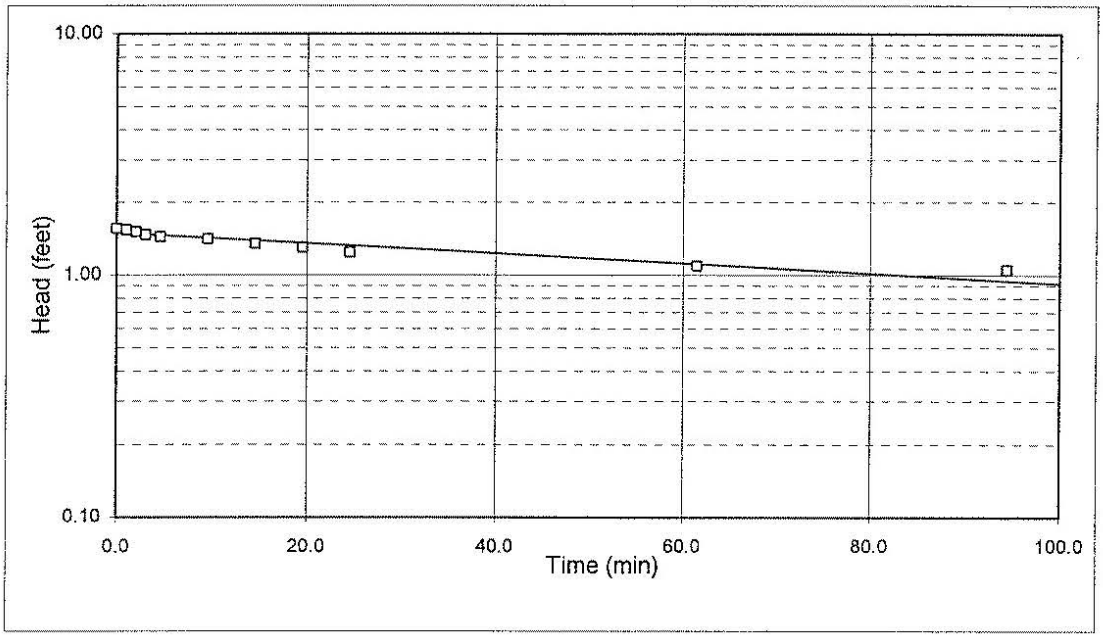
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.15
r_w =	0.25
L_e =	7.11
$\ln(R_e/r_w)$	2.00
y_0 =	1.49
y_t =	0.92
t =	100.0

RESULTS

K=	8.46E-06	cm/sec
K=	2.40E-02	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/20/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-106-SS

WELL NO. PZ-106-SS

DATE	7/19/95	
INITIAL DEPTH TO WATER	105.11	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	151.5	FEET (btoc)
BOTTOM OF OPEN INTERVAL	166.8	FEET (btoc)
SATURATED THICKNESS	90	FEET
WATER TABLE TO BOTTOM OF SCREEN	61.69	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	15.3	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.63	FEET
MAX. HEAD IN SCREEN?	N	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	813	30	108.74	0.0	3.63	1.00
1	815	0	108.68	1.5	3.57	0.98
1	820	0	108.53	6.5	3.42	0.94
1	825	0	108.37	11.5	3.26	0.90
1	830	0	108.24	16.5	3.13	0.86
1	835	0	108.1	21.5	2.99	0.82
1	840	0	108	26.5	2.89	0.80
1	845	0	107.85	31.5	2.74	0.75
1	850	0	107.75	36.5	2.64	0.73
1	1045	30	106.12	152.0	1.01	0.28
1	1118	30	105.98	185.0	0.87	0.24
1	1140	0	105.74	206.5	0.63	0.17

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-106-SS

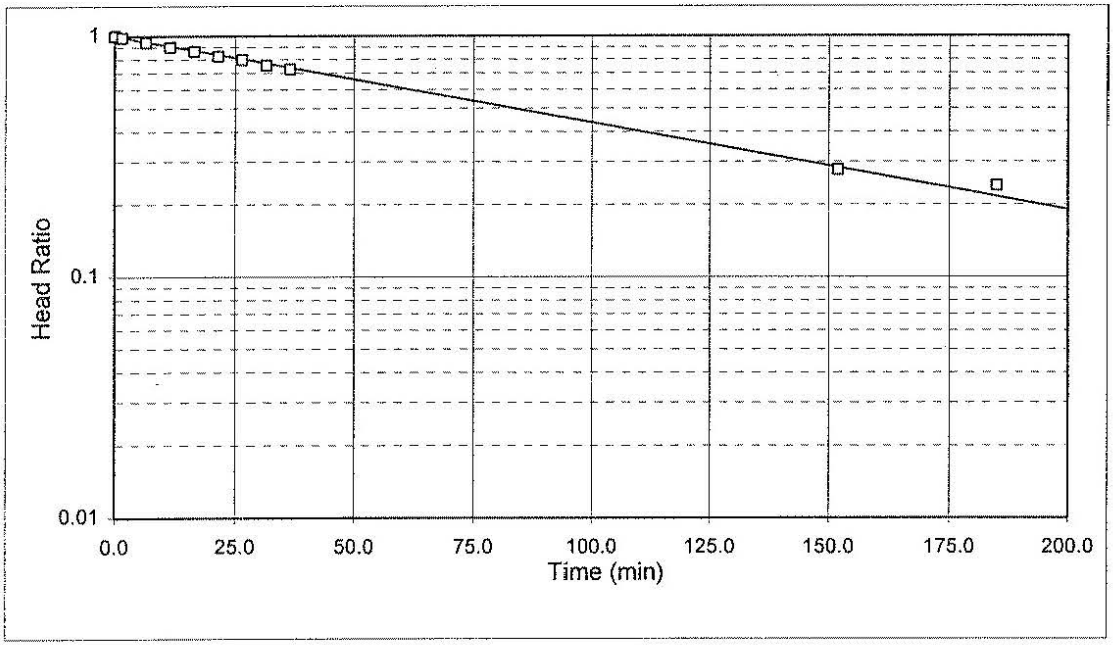
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2-t1)}\right]30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	15.3
t_1 (min) =	0
t_2 (min) =	200
h_1/h_0 =	1.00
h_2/h_0 =	0.19

RESULTS

K=	3.93E-06	cm/sec
K=	1.11E-02	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/19/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

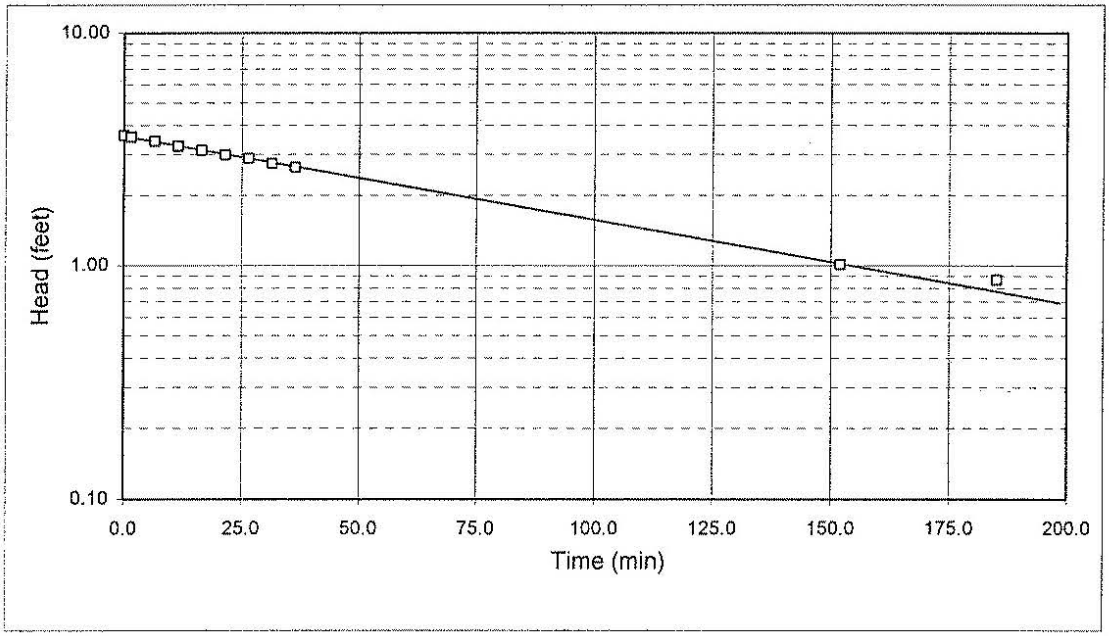
BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-106-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
r_w =	0.25			
L_e =	15.3	K=	2.50E-06	cm/sec
$\ln(R_e/r_w)$	3.39	K=	7.07E-03	ft/day
y_0 =	3.60			
y_t =	0.69			
t =	198.7			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/19/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-106-SD

WELL NO. PZ-106-SD

DATE	7/21/95	
INITIAL DEPTH TO WATER	107.17	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	189	FEET (btoc)
BOTTOM OF OPEN INTERVAL	203.1	FEET (btoc)
SATURATED THICKNESS	100	FEET
WATER TABLE TO BOTTOM OF SCREEN	95.93	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	14.1	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.84	FEET
MAX. HEAD IN SCREEN?	N	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1205	0	111.01	0.0	3.84	1.00
1	1207	0	110.88	2.0	3.71	0.97
1	1208	0	110.81	3.0	3.64	0.95
1	1209	0	110.76	4.0	3.59	0.93
1	1214	0	110.7	9.0	3.53	0.92
1	1219	0	110.66	14.0	3.49	0.91
1	1224	0	110.62	19.0	3.45	0.90
1	1240	0	110.6	35.0	3.43	0.89
1	1400	0	110.52	115.0	3.35	0.87
1	1421	0	110.5	136.0	3.33	0.87

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-106-SD

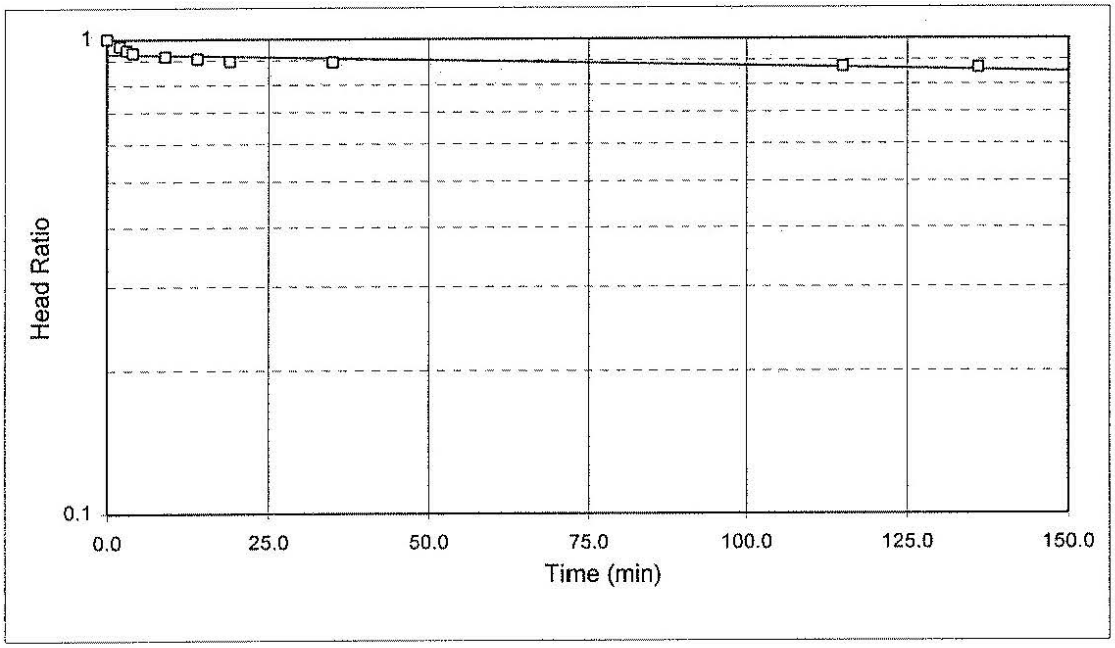
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{y_1}{y_2}\right)}{(t2 - t1)}\right] 30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	14.1
t_1 (min) =	0
t_2 (min) =	150
y_1 =	0.93
y_2 =	0.85

RESULTS

K=	2.98E-07	cm/sec
K=	8.45E-04	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/21/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 9/24/95

BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-106-SD

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

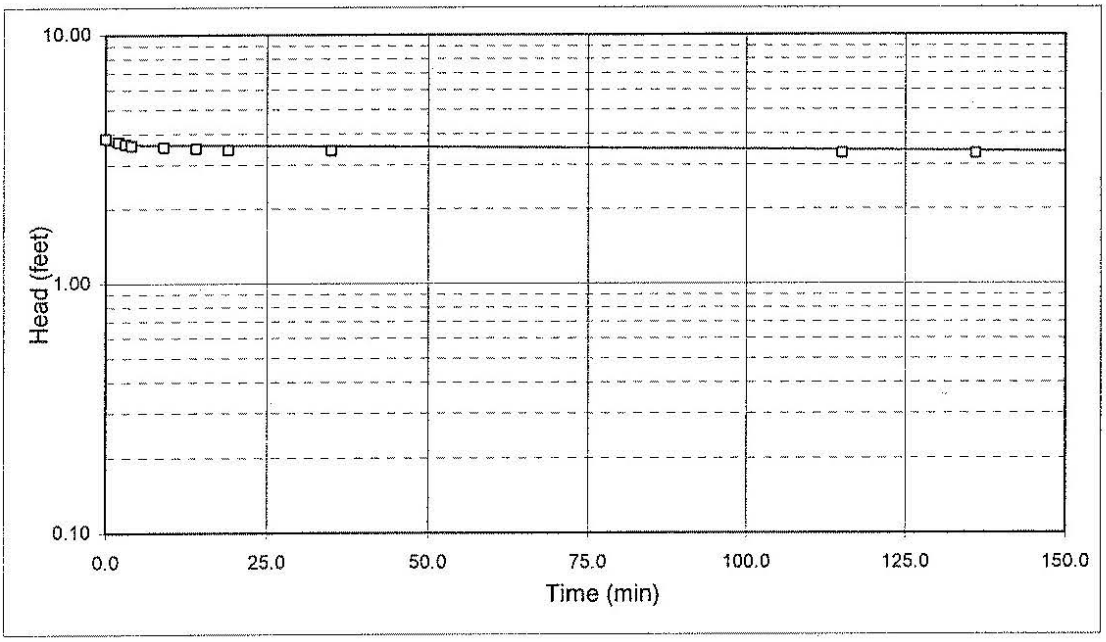
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.25
L_e =	14.1
$\ln(R_e/r_w)$ =	3.75
y_0 =	3.63
y_t =	3.39
t =	150.0

RESULTS

K=	1.56E-07	cm/sec
K=	4.42E-04	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/21/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 9/24/95

RISING HEAD TEST PZ-106-KS

WELL NO PZ-106-KS

DATE	7/20/95	
INITIAL DEPTH TO WATER	21.64	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	362.5	FEET (btoc)
BOTTOM OF OPEN INTERVAL	377.5	FEET (btoc)
BOTTOM OF AQUIFER	500	FEET (btoc)
SATURATED THICKNESS	355.86	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	15	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	1.81	FEET
MAX. HEAD IN SCREEN?	N	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (SEC)	HEAD (FEET)	HEAD RATIO
1	1123	30	23.45	0.0	1.81	1.00
1	1124	30	23.38	60.0	1.74	0.96
1	1125	30	23.29	120.0	1.65	0.91
1	1126	30	23.21	180.0	1.57	0.87
1	1127	30	23.13	240.0	1.49	0.82
1	1128	30	23.05	300.0	1.41	0.78
1	1129	30	22.99	360.0	1.35	0.75
1	1130	30	22.92	420.0	1.28	0.71
1	1131	30	22.85	480.0	1.21	0.67
1	1136	30	22.6	780.0	0.96	0.53
1	1141	30	22.38	1080.0	0.74	0.41
1	1146	30	22.2	1380.0	0.56	0.31
1	1151	30	22.09	1680.0	0.45	0.25
1	1156	30	22	1980.0	0.36	0.20
1	1201	30	21.91	2280.0	0.27	0.15
1	1210	0	21.82	2790.0	0.18	0.10

COOPER-PAPADOPULOS SLUG TEST ANALYSIS
RISING HEAD TEST PZ-106-KS

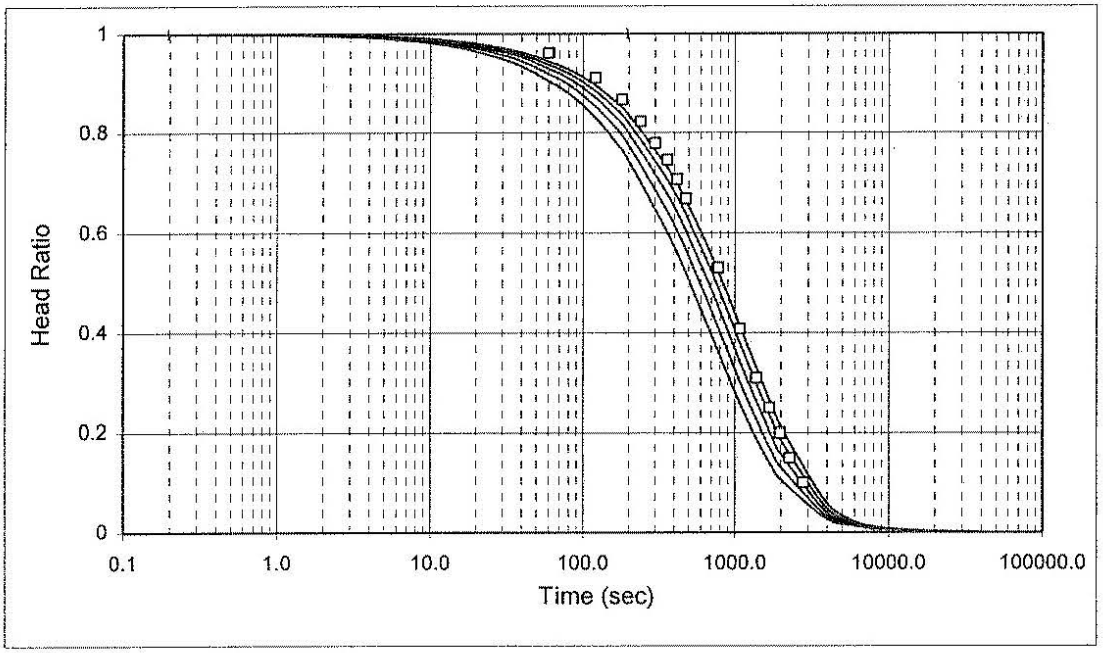
$$K = \frac{r_c^{\,2}\beta}{tb} \qquad \text{and} \qquad S = \frac{r_c^{\,2}\alpha}{r_{ew}^{\,2}}$$

where:

r_c = casing radius (feet)
r_{ew} = effective radius of screen (feet)
t = time (seconds)
K = Hydraulic conductivity (ft/sec)
$h_t/h_0 = F(\alpha,B)$

S = Storativity (dim)
h_t = Head at time t (feet)
b = Aquifer thickness (feet)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
r_{ew} =	0.25			
t =	195.0	K=	3.05E-06	cm/sec
α =	1	K=	0.009	ft/day
B =	1E-09	S =	1.11E-10	
b =	355.86			



Project Name: LAIDLAW / OU2 RIFS / MO
Project No.: 943-2848
Test Date: 07/20/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 9/24/95

RISING HEAD TEST PZ-107-SS

WELL NO. PZ-107-SS

DATE	7/15/95	
INITIAL DEPTH TO WATER	30.26	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	91.0	FEET (btoc)
BOTTOM OF OPEN INTERVAL	105.0	FEET (btoc)
SATURATED THICKNESS	170	FEET
WATER TABLE TO BOTTOM OF SCREEN	74.74	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	14	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	7.44	FEET
MAX. HEAD IN SCREEN?	N	

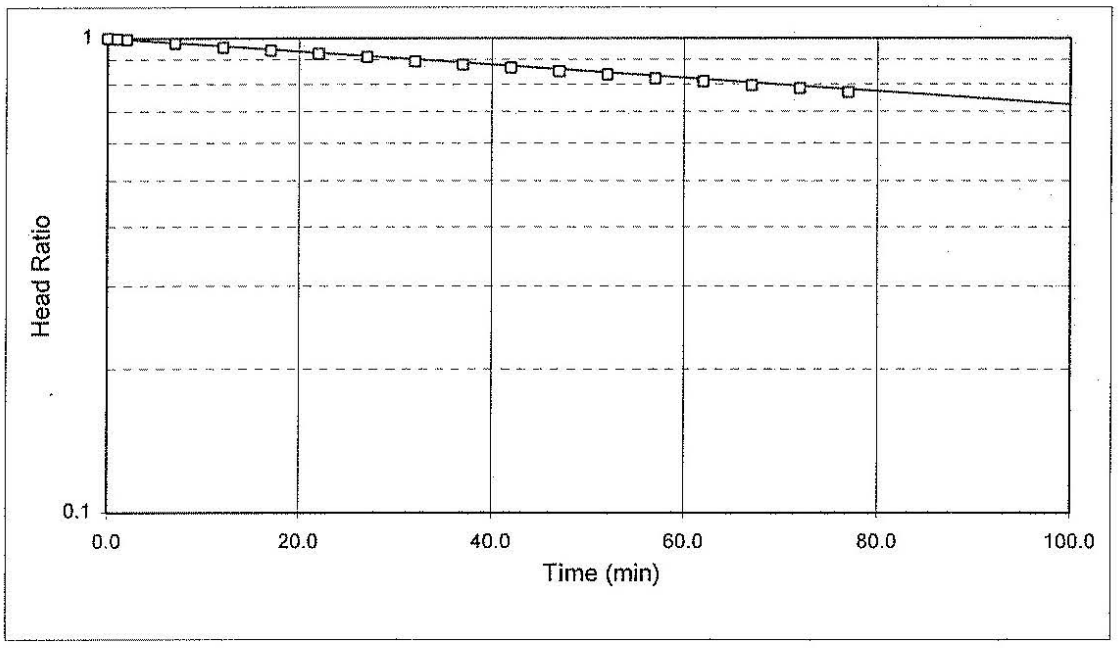
DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1143	0	37.7	0.0	7.44	1.00
1	1144	0	37.68	1.0	7.42	1.00
1	1145	0	37.65	2.0	7.39	0.99
1	1150	0	37.51	7.0	7.25	0.97
1	1155	0	37.37	12.0	7.11	0.96
1	1200	0	37.26	17.0	7.00	0.94
1	1205	0	37.15	22.0	6.89	0.93
1	1210	0	37.05	27.0	6.79	0.91
1	1215	0	36.9	32.0	6.64	0.89
1	1220	0	36.79	37.0	6.53	0.88
1	1225	0	36.7	42.0	6.44	0.87
1	1230	0	36.59	47.0	6.33	0.85
1	1235	0	36.49	52.0	6.23	0.84
1	1240	0	36.37	57.0	6.11	0.82
1	1245	0	36.29	62.0	6.03	0.81
1	1250	0	36.17	67.0	5.91	0.79
1	1255	0	36.09	72.0	5.83	0.78
1	1300	0	35.98	77.0	5.72	0.77
1	1325	0	35.52	102.0	5.26	0.71

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-107-SS

$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
h_t = head at time t (feet)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
R_e =	0.25			
L_e =	14	K=	1.63E-06	cm/sec
t_1 (min) =	0	K=	4.63E-03	ft/day
t_2 (min) =	100			
h_1/h_0 =	1.00			
h_2/h_0 =	0.72			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/15/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-107-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

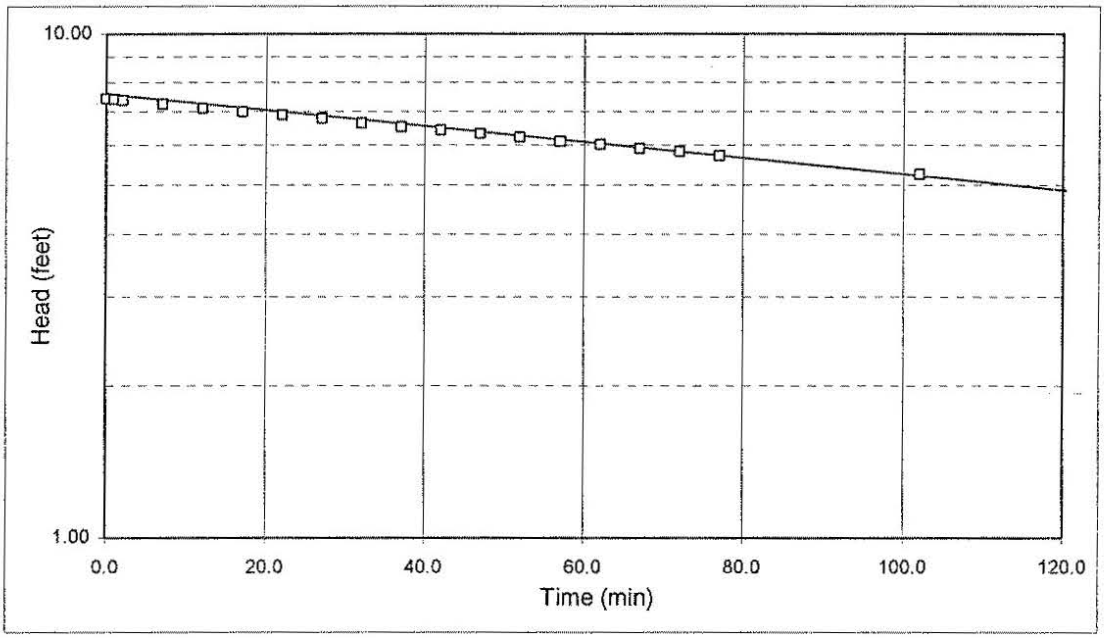
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.25
L_e =	14
$\ln(R_e/r_w)$	3.31
y_0 =	7.59
y_t =	4.89
t =	120.4

RESULTS

K=	1.19E-06	cm/sec
K=	3.37E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/15/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-108-SS

WELL NO. PZ-108-SS

DATE	7/21/95	
INITIAL DEPTH TO WATER	87.11	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	132.1	FEET (btoc)
BOTTOM OF OPEN INTERVAL	146.0	FEET (btoc)
SATURATED THICKNESS	110	FEET
WATER TABLE TO BOTTOM OF SCREEN	58.89	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	13.9	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.67	FEET
MAX. HEAD IN SCREEN?	N	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	927	30	90.78	0.0	3.67	1.00
1	928	30	90.74	1.0	3.63	0.99
1	929	30	90.71	2.0	3.60	0.98
1	930	30	90.69	3.0	3.58	0.98
1	935	30	90.66	8.0	3.55	0.97
1	940	30	90.61	13.0	3.50	0.95
1	945	30	90.58	18.0	3.47	0.95
1	955	30	90.54	28.0	3.43	0.93
1	1034	0	90.43	66.5	3.32	0.90
1	1243	30	89.94	196.0	2.83	0.77
1	1332	30	89.89	245.0	2.78	0.76
1	1449	0	89.8	321.5	2.69	0.73

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-108-SS

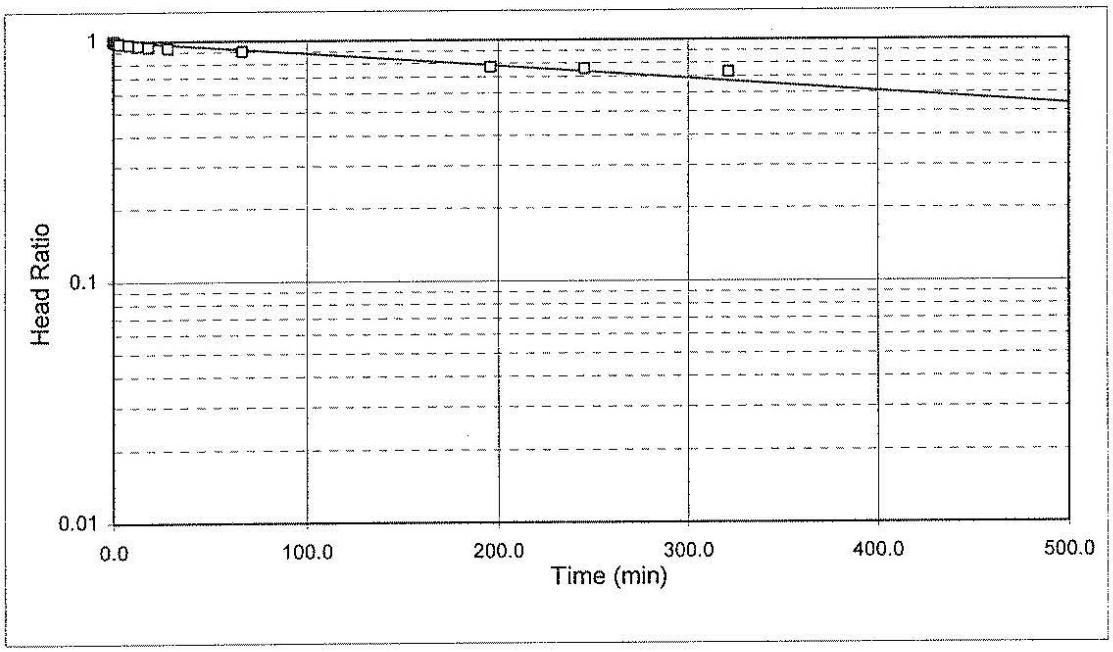
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	13.9
t_1(min) =	0
t_2(min) =	500
h_1/h_0 =	1.00
h_2/h_0 =	0.54

RESULTS

K=	6.34E-07	cm/sec
K=	1.80E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/21/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-108-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

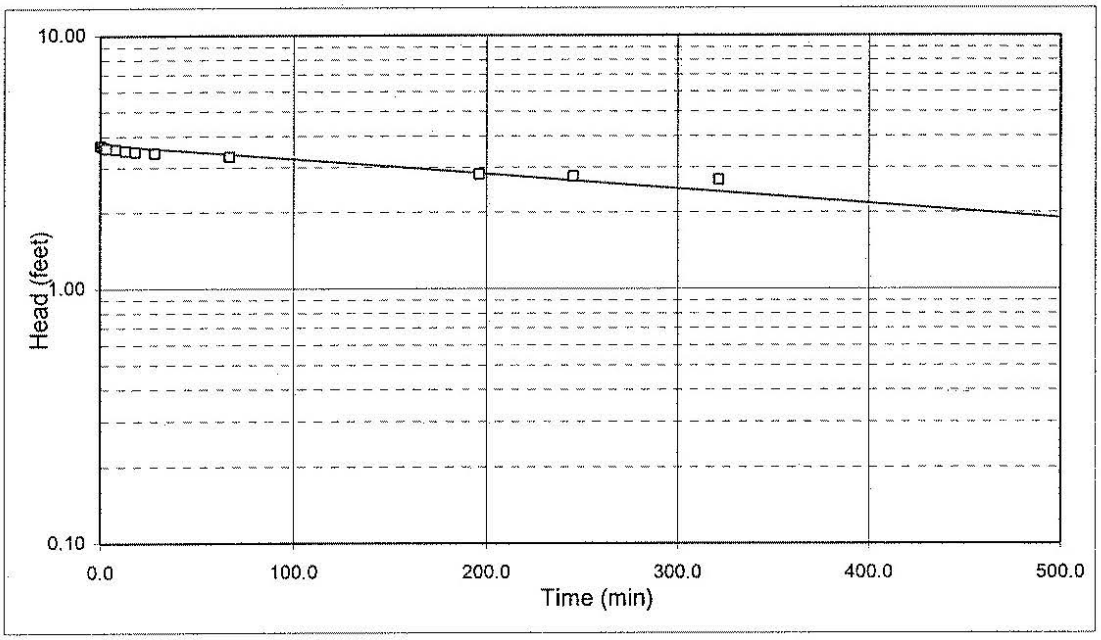
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.25
L_e =	13.9
$\ln(R_e/r_w)$	3.27
y_0 =	3.70
y_t =	1.91
t =	500.0

RESULTS

K=	4.33E-07	cm/sec
K=	1.23E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/21/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-109-SS

WELL NO. PZ-109-SS

DATE	7/21/95	
INITIAL DEPTH TO WATER	84.41	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	123.0	FEET (btoc)
BOTTOM OF OPEN INTERVAL	137.4	FEET (btoc)
SATURATED THICKNESS	110	FEET
WATER TABLE TO BOTTOM OF SCREEN	52.99	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	14.4	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.35	FEET
MAX. HEAD IN SCREEN?	N	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	850	0	87.76	0.0	3.35	1.00
1	851	0	87.74	1.0	3.33	0.99
1	852	0	87.73	2.0	3.32	0.99
1	853	0	87.72	3.0	3.31	0.99
1	858	0	87.69	8.0	3.28	0.98
1	903	0	87.68	13.0	3.27	0.98
1	910	30	87.67	20.5	3.26	0.97
1	1001	30	87.6	71.5	3.19	0.95
1	1029	30	87.58	99.5	3.17	0.95
1	1254	30	87.4	244.5	2.99	0.89
1	1328	0	87.39	278.0	2.98	0.89
1	1454	30	87.38	364.5	2.97	0.89

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-109-SS

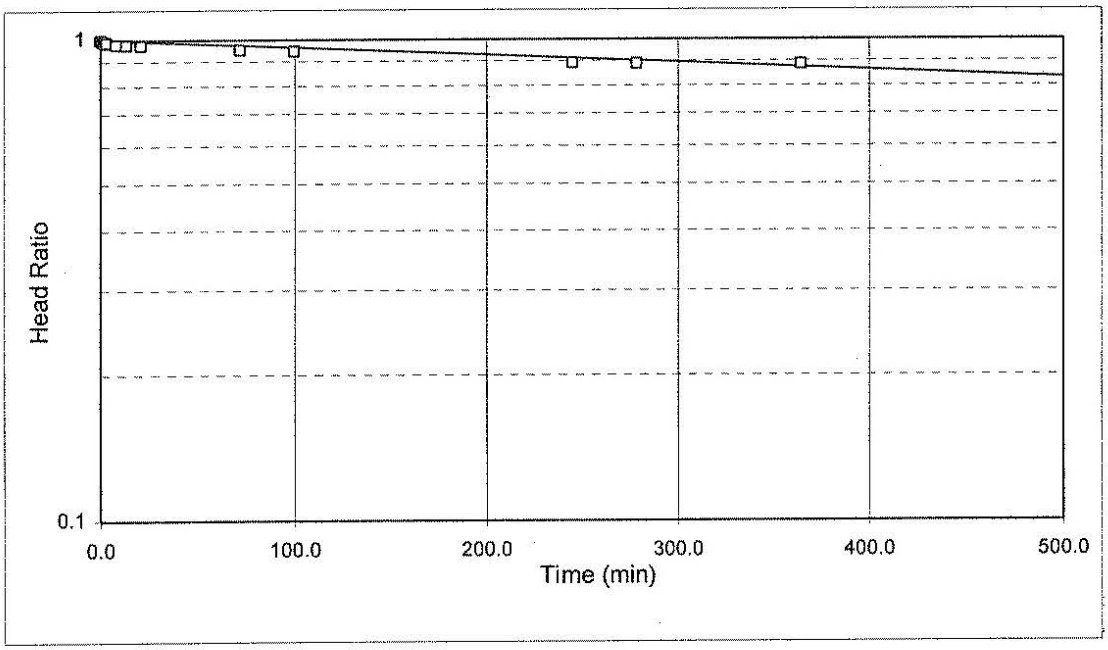
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	14.4
t_1 (min) =	0
t_2 (min) =	500
h_1/h_0 =	1.00
h_2/h_0 =	0.83

RESULTS

K=	1.83E-07	cm/sec
K=	5.19E-04	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/21/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-109-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

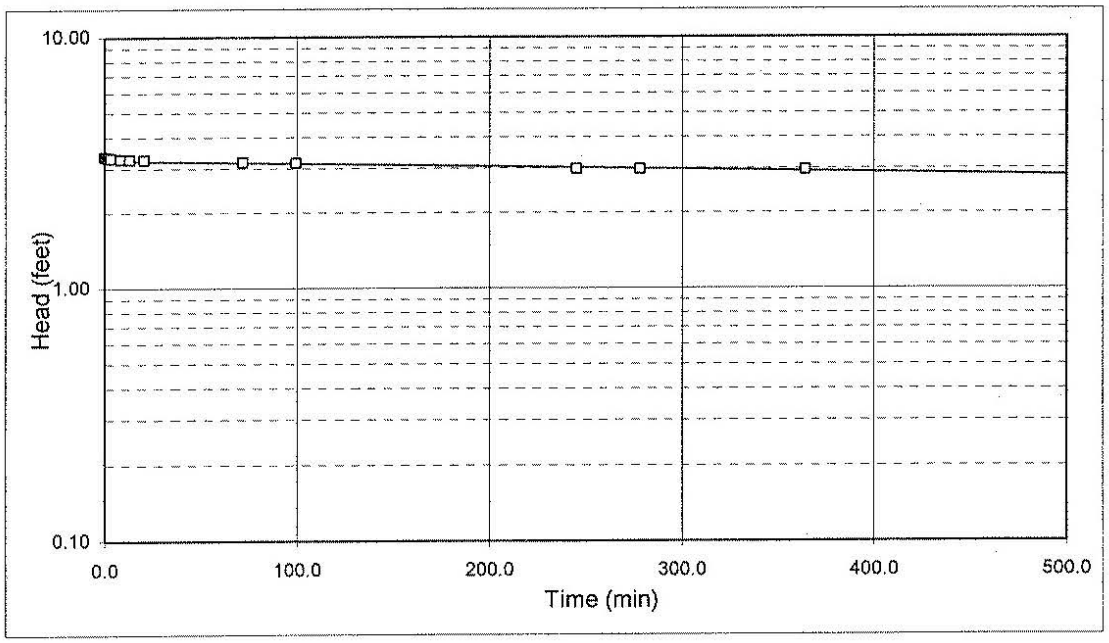
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.25
L_e =	14.4
$\ln(R_e/r_w)$	3.24
y_0 =	3.24
y_t =	2.82
t =	500.0

RESULTS

K=	8.67E-08	cm/sec
K=	2.46E-04	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/21/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-110-SS

WELL NO. PZ-110-SS

DATE	6/21/95	
INITIAL DEPTH TO WATER	85.75	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	98.6	FEET (btoc)
BOTTOM OF OPEN INTERVAL	113.6	FEET (btoc)
SATURATED THICKNESS	180	FEET
WATER TABLE TO BOTTOM OF SCREEN	27.85	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	15	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	2.77	FEET
MAX. HEAD IN SCREEN?	N	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1229	0	88.52	0.0	2.77	1.00
1	1230	0	88.5	1.0	2.75	0.99
1	1231	0	88.49	2.0	2.74	0.99
1	1236	0	88.4	7.0	2.65	0.96
1	1241	0	88.36	12.0	2.61	0.94
1	1246	0	88.34	17.0	2.59	0.94
1	1251	0	88.3	22.0	2.55	0.92
1	1256	0	88.27	27.0	2.52	0.91
1	1301	0	88.22	32.0	2.47	0.89
1	1306	0	88.18	37.0	2.43	0.88
1	1311	0	88.14	42.0	2.39	0.86
1	1316	0	88.1	47.0	2.35	0.85
1	1321	0	88.08	52.0	2.33	0.84
1	1326	0	88.03	57.0	2.28	0.82
1	1331	0	88	62.0	2.25	0.81
1	1336	0	87.96	67.0	2.21	0.80
1	1341	0	87.91	72.0	2.16	0.78
1	1346	0	87.88	77.0	2.13	0.77
1	1351	0	87.84	82.0	2.09	0.75
1	1356	0	87.82	87.0	2.07	0.75
1	1401	0	87.79	92.0	2.04	0.74
1	1406	0	87.73	97.0	1.98	0.71
1	1411	0	87.71	102.0	1.96	0.71
1	1416	0	87.69	107.0	1.94	0.70
1	1421	0	87.64	112.0	1.89	0.68

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1426	0	87.61	117.0	1.86	0.67
1	1431	0	87.57	122.0	1.82	0.66
1	1436	0	87.53	127.0	1.78	0.64
1	1550	0	87.46	201.0	1.71	0.62
1	1618	30	86.75	229.5	1.00	0.36
1	1623	30	86.74	234.5	0.99	0.36
1	1628	30	86.69	239.5	0.94	0.34
1	1633	30	86.66	244.5	0.91	0.33
1	1638	30	86.61	249.5	0.86	0.31
1	1643	30	86.57	254.5	0.82	0.30
1	1648	30	86.52	259.5	0.77	0.28

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-110-SS

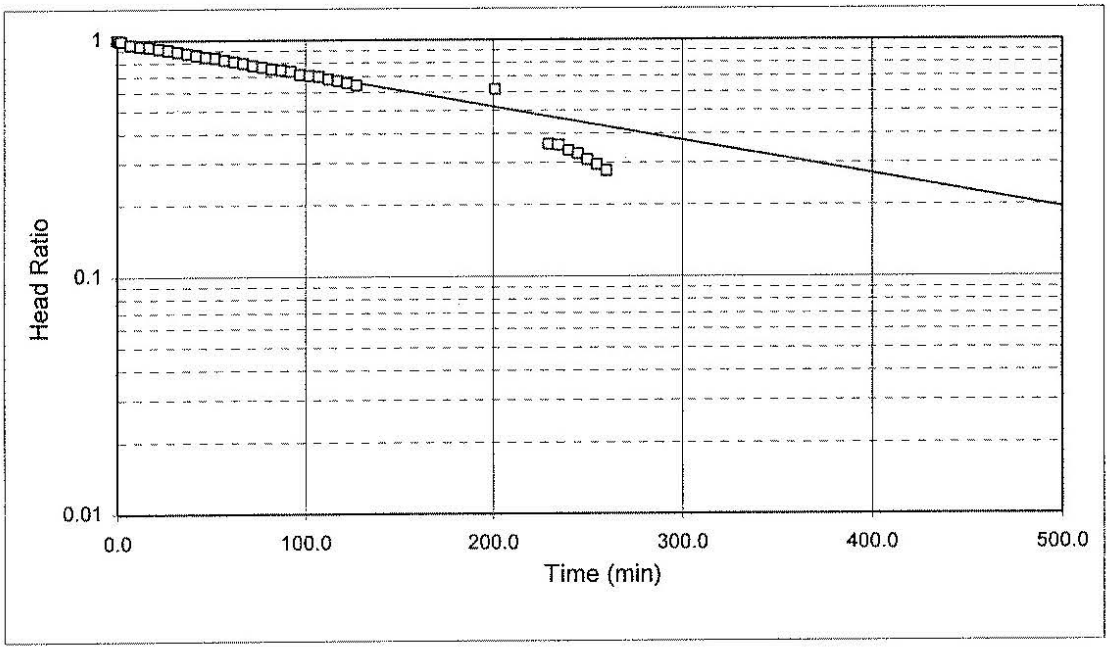
$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	15
t_1 (min) =	0
t_2 (min) =	500
h_1/h_0 =	1.00
h_2/h_0 =	0.19

RESULTS

K=	1.57E-06	cm/sec
K=	4.46E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 06/21/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

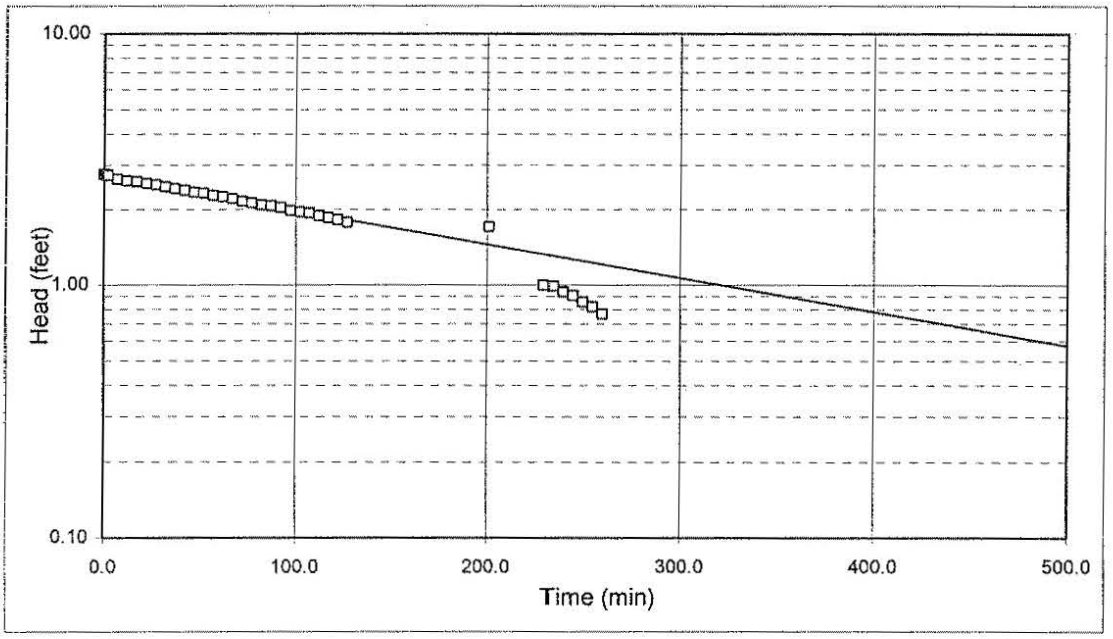
BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-110-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
r_w =	0.25			
L_e =	15	K=	8.91E-07	cm/sec
$\ln(R_e/r_w)$	2.91	K=	2.52E-03	ft/day
y_0 =	2.69			
y_t =	0.58			
t =	500.0			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 06/21/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-111-SD

WELL NO. PZ-111-SD

DATE	7/24/95	
INITIAL DEPTH TO WATER	37.68	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	197.0	FEET (btoc)
BOTTOM OF OPEN INTERVAL	212.3	FEET (btoc)
SATURATED THICKNESS	180	FEET
WATER TABLE TO BOTTOM OF SCREEN	174.62	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	15.3	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.88	FEET
MAX. HEAD IN SCREEN?	N	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1324	30	41.56	0.0	3.88	1.00
1	1325	30	41.54	1.0	3.86	0.99
1	1327	0	41.53	2.5	3.85	0.99
1	1330	0	41.53	5.5	3.85	0.99
1	1335	0	41.51	10.5	3.83	0.99
1	1340	0	41.5	15.5	3.82	0.98
1	1350	0	41.49	25.5	3.81	0.98
1	1440	0	41.48	75.5	3.80	0.98
2	711	0	40.88	1066.5	3.20	0.82
2	1146	0	40.63	1341.5	2.95	0.76
2	1527	0	40.53	1562.5	2.85	0.73
2	1744	0	40.45	1699.5	2.77	0.71
3	1014	0	39.88	2689.5	2.20	0.57
3	1619	0	39.67	3054.5	1.99	0.51
4	709	0	39.19	3944.5	1.51	0.39
4	1349	0	38.96	4344.5	1.28	0.33

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-111-SD

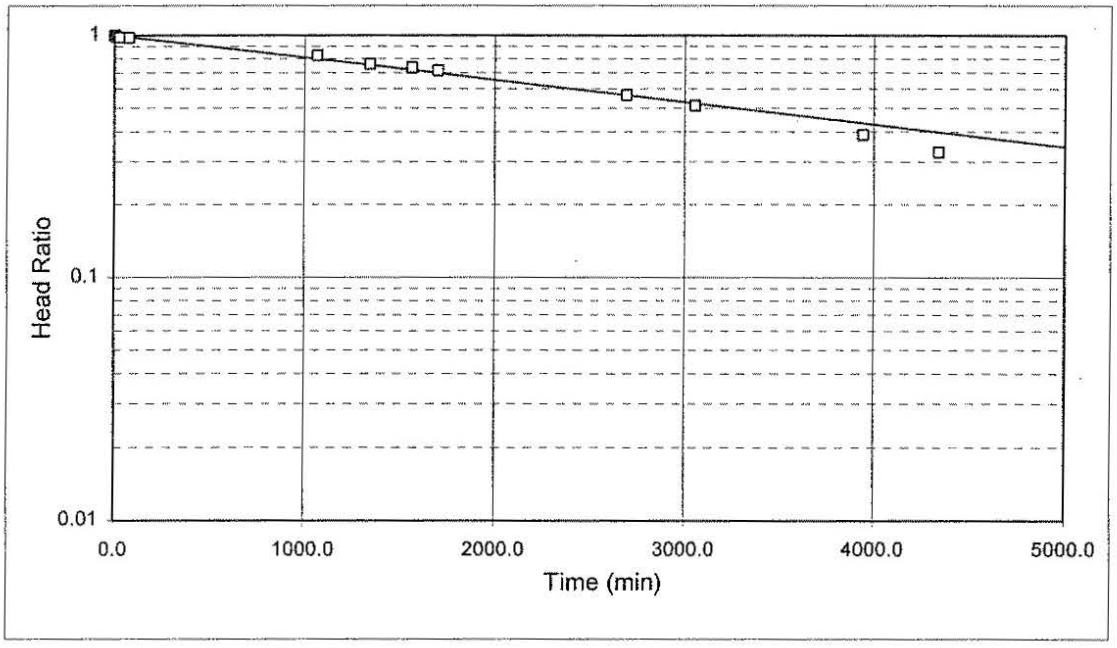
$$K = \frac{r_c^2}{2L_e} ln \frac{L_e}{R_e} \left[\frac{ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	15.3
t_1 (min) =	0
t_2 (min) =	5000
h_1/h_0 =	1.00
h_2/h_0 =	0.35

RESULTS

K=	1.00E-07	cm/sec
K=	2.85E-04	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/24/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-111-SD

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

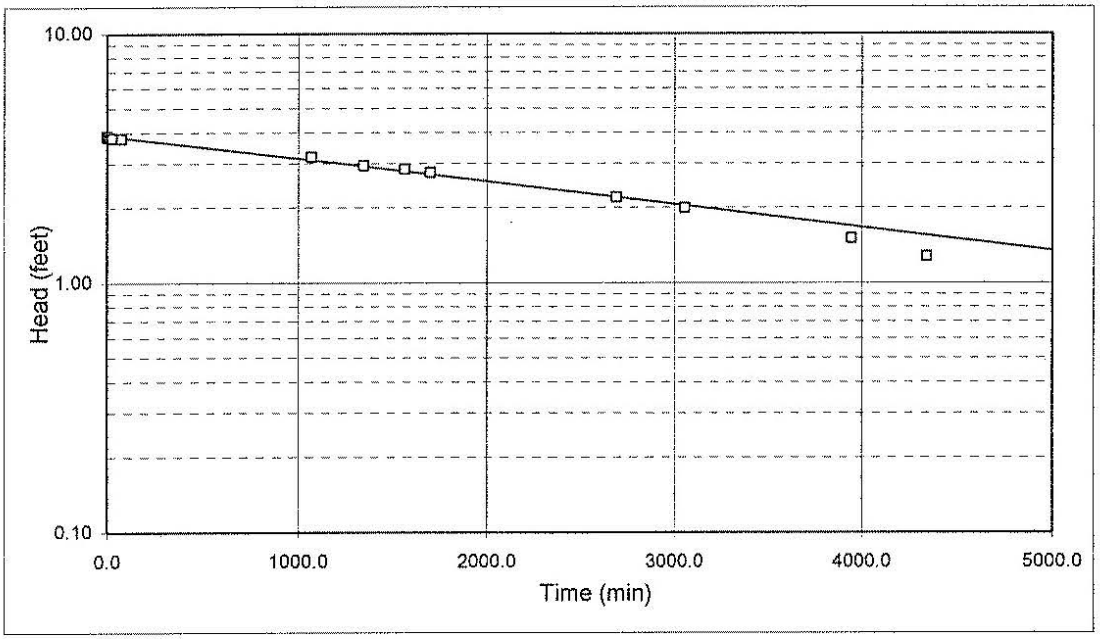
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.25
L_e =	15.3
$\ln(R_e/r_w)$	4.01
y_0 =	3.89
y_t =	1.35
t =	5000.0

RESULTS

K=	6.78E-08	cm/sec
K=	1.92E-04	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/24/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-111-KS

WELL NO PZ-111-KS

DATE	7/24/95	
INITIAL DEPTH TO WATER	18.89	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	353.1	FEET (btoc)
BOTTOM OF OPEN INTERVAL	370.5	FEET (btoc)
BOTTOM OF AQUIFER	500	FEET (btoc)
SATURATED THICKNESS	351.6	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	17.4	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.51	FEET
MAX. HEAD IN SCREEN?	N	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (SEC)	HEAD (FEET)	HEAD RATIO
1	1236	30	22.4	0.0	3.51	1.00
1	1237	30	22.19	60.0	3.30	0.94
1	1238	0	22.08	90.0	3.19	0.91
1	1238	30	21.98	120.0	3.09	0.88
1	1239	0	21.88	150.0	2.99	0.85
1	1240	0	21.68	210.0	2.79	0.79
1	1241	0	21.53	270.0	2.64	0.75
1	1242	0	21.36	330.0	2.47	0.70
1	1243	0	21.21	390.0	2.32	0.66
1	1244	0	21.09	450.0	2.20	0.63
1	1245	0	20.96	510.0	2.07	0.59
1	1250	0	20.42	810.0	1.53	0.44
1	1255	0	20.02	1110.0	1.13	0.32
1	1300	0	19.74	1410.0	0.85	0.24
1	1305	0	19.53	1710.0	0.64	0.18
1	1310	0	19.37	2010.0	0.48	0.14
1	1315	0	19.24	2310.0	0.35	0.10
1	1320	0	19.17	2610.0	0.28	0.08
1	1328	0	19.07	3090.0	0.18	0.05
1	1331	0	19.05	3270.0	0.16	0.05

COOPER-PAPADOPULOS SLUG TEST ANALYSIS
RISING HEAD TEST PZ-111-KS

$$K = \frac{r_c^{\,2}\beta}{tb} \qquad \text{and} \qquad S = \frac{r_c^{\,2}\alpha}{r_{ew}^{\,2}}$$

where:

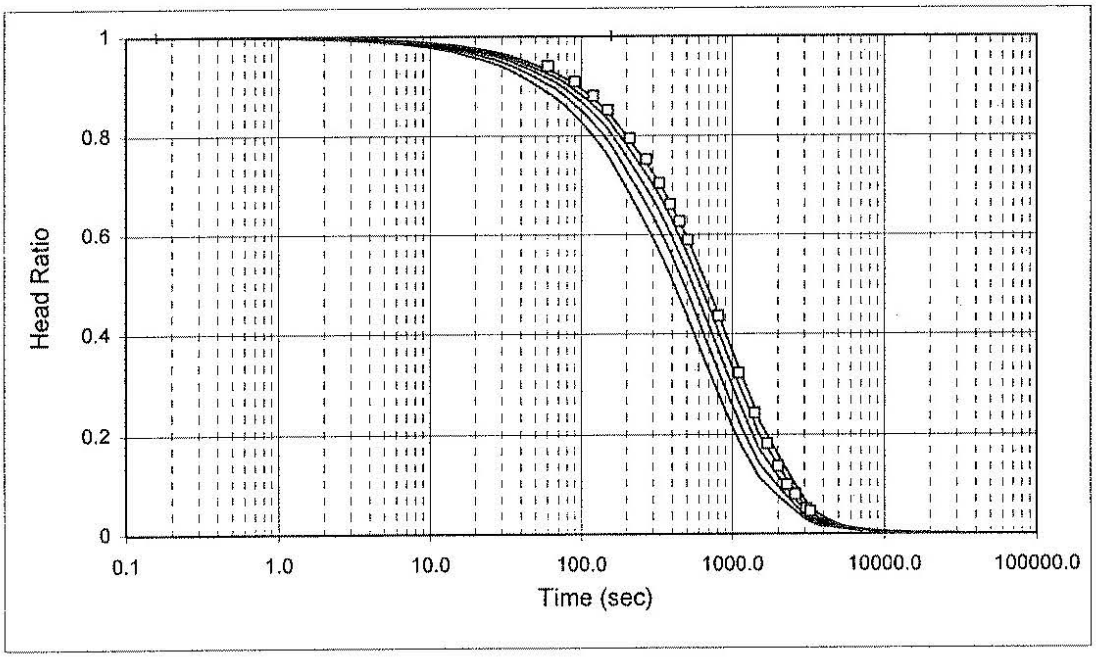
r_c = casing radius (feet)
r_{ew} = effective radius of screen (feet)
t = time (seconds)
K = Hydraulic conductivity (ft/sec)
$h_t/h_0 = F(\alpha,B)$

S = Storativity (dim)
h_t = Head at time t (feet)
b = Aquifer thickness (feet)

INPUT PARAMETERS	
r_c =	0.08
r_{ew} =	0.25
t =	157.8
α =	1
B =	1E-09
b =	351.61

RESULTS

K=	3.82E-06	cm/sec
K=	0.011	ft/day
S =	1.11E-10	



Project Name: LAIDLAW / OU2 RIFS / MO
Project No.: 943-2848
Test Date: 07/24/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

FALLING HEAD TEST PZ-112-AS-FH1

WELL NO. PZ-112-AS-FH1

DATE	7/25/95	
INITAL HEAD ON TRANSDUCER	10.19	FEET H_2O
INITIAL DEPTH TO WATER	24.79	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	28.5	FEET (btoc)
BOTTOM OF OPEN INTERVAL	37.9	FEET (btoc)
SATURATED THICKNESS	100	FEET
WATER TABLE TO BOTTOM OF SCREEN	13.11	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	9.4	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	2.37	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	206	930	5	12.563	0.00	22.42	2.37	1.00
1995	206	930	6	12.297	0.02	22.68	2.11	0.89
1995	206	930	7	12.132	0.03	22.85	1.94	0.82
1995	206	930	8	11.973	0.05	23.01	1.78	0.75
1995	206	930	9	11.829	0.07	23.15	1.64	0.69
1995	206	930	10	11.698	0.08	23.28	1.51	0.64
1995	206	930	11	11.577	0.10	23.40	1.39	0.58
1995	206	930	12	11.469	0.12	23.51	1.28	0.54
1995	206	930	13	11.366	0.13	23.61	1.18	0.50
1995	206	930	14	11.273	0.15	23.71	1.08	0.46
1995	206	930	15	11.189	0.17	23.79	1.00	0.42
1995	206	930	16	11.111	0.18	23.87	0.92	0.39
1995	206	930	17	11.04	0.20	23.94	0.85	0.36
1995	206	930	18	10.973	0.22	24.01	0.78	0.33
1995	206	930	19	10.913	0.23	24.07	0.72	0.30
1995	206	930	20	10.858	0.25	24.12	0.67	0.28
1995	206	930	21	10.807	0.27	24.17	0.62	0.26
1995	206	930	22	10.76	0.28	24.22	0.57	0.24
1995	206	930	23	10.718	0.30	24.26	0.53	0.22
1995	206	930	24	10.679	0.32	24.30	0.49	0.21
1995	206	930	25	10.643	0.33	24.34	0.45	0.19
1995	206	930	26	10.61	0.35	24.37	0.42	0.18
1995	206	930	27	10.58	0.37	24.40	0.39	0.16
1995	206	930	28	10.55	0.38	24.43	0.36	0.15
1995	206	930	29	10.527	0.40	24.45	0.34	0.14
1995	206	930	30	10.501	0.42	24.48	0.31	0.13
1995	206	930	31	10.48	0.43	24.50	0.29	0.12

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	206	930	32	10.459	0.45	24.52	0.27	0.11
1995	206	930	33	10.437	0.47	24.54	0.25	0.10
1995	206	930	34	10.419	0.48	24.56	0.23	0.10
1995	206	930	35	10.405	0.50	24.58	0.22	0.09
1995	206	930	36	10.391	0.52	24.59	0.20	0.08
1995	206	930	37	10.376	0.53	24.60	0.19	0.08
1995	206	930	38	10.363	0.55	24.62	0.17	0.07
1995	206	930	39	10.354	0.57	24.63	0.16	0.07
1995	206	930	40	10.341	0.58	24.64	0.15	0.06
1995	206	930	41	10.332	0.60	24.65	0.14	0.06
1995	206	930	42	10.323	0.62	24.66	0.13	0.06
1995	206	930	43	10.316	0.63	24.66	0.13	0.05
1995	206	930	44	10.305	0.65	24.68	0.12	0.05
1995	206	930	45	10.301	0.67	24.68	0.11	0.05
1995	206	930	46	10.292	0.68	24.69	0.10	0.04
1995	206	930	47	10.29	0.70	24.69	0.10	0.04
1995	206	930	48	10.281	0.72	24.70	0.09	0.04
1995	206	930	49	10.277	0.73	24.70	0.09	0.04
1995	206	930	50	10.272	0.75	24.71	0.08	0.03
1995	206	930	51	10.266	0.77	24.71	0.08	0.03
1995	206	930	52	10.264	0.78	24.72	0.07	0.03
1995	206	930	53	10.258	0.80	24.72	0.07	0.03
1995	206	930	54	10.255	0.82	24.73	0.07	0.03
1995	206	930	55	10.252	0.83	24.73	0.06	0.03
1995	206	930	56	10.247	0.85	24.73	0.06	0.02
1995	206	930	57	10.245	0.87	24.74	0.05	0.02
1995	206	930	58	10.243	0.88	24.74	0.05	0.02
1995	206	930	59	10.24	0.90	24.74	0.05	0.02
1995	206	931	0	10.236	0.92	24.74	0.05	0.02
1995	206	931	1	10.237	0.93	24.74	0.05	0.02
1995	206	931	2	10.234	0.95	24.75	0.04	0.02

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-112-AS-FH1

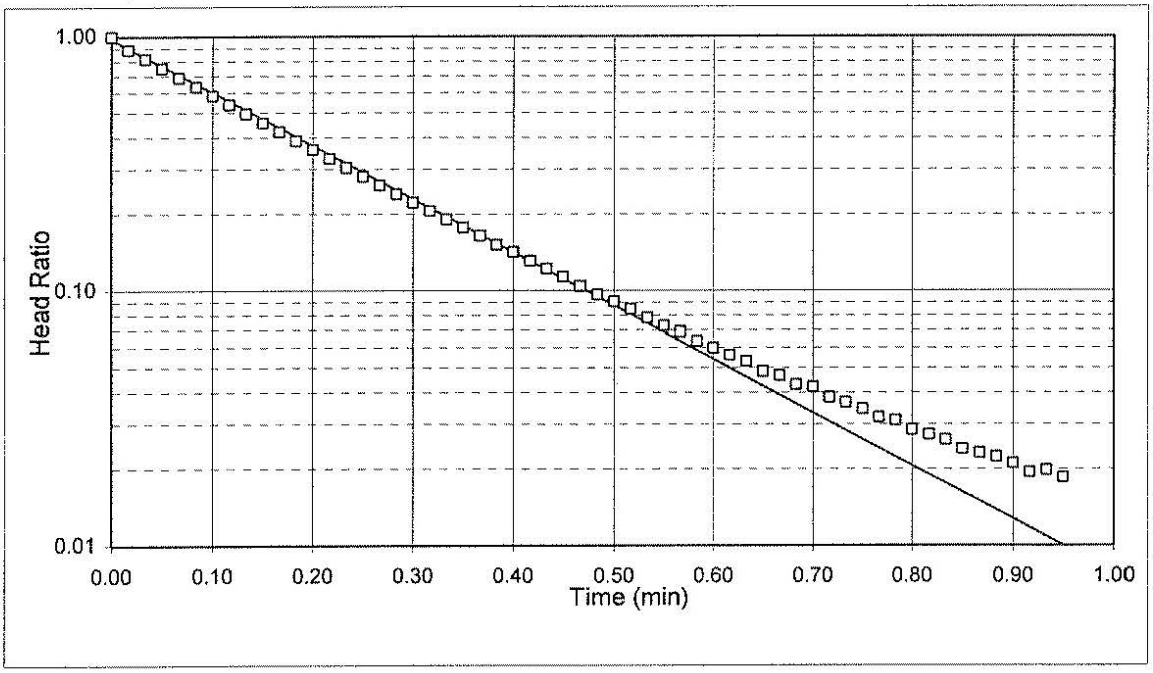
$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
Re =	0.34
L_e =	9.4
t_1 (min) =	0
t_2 (min) =	0.95
h_1/h_0 =	0.98
h_2/h_0 =	0.01

RESULTS

K=	2.99E-03	cm/sec
K=	8.49E+00	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-112-AS-FH1

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

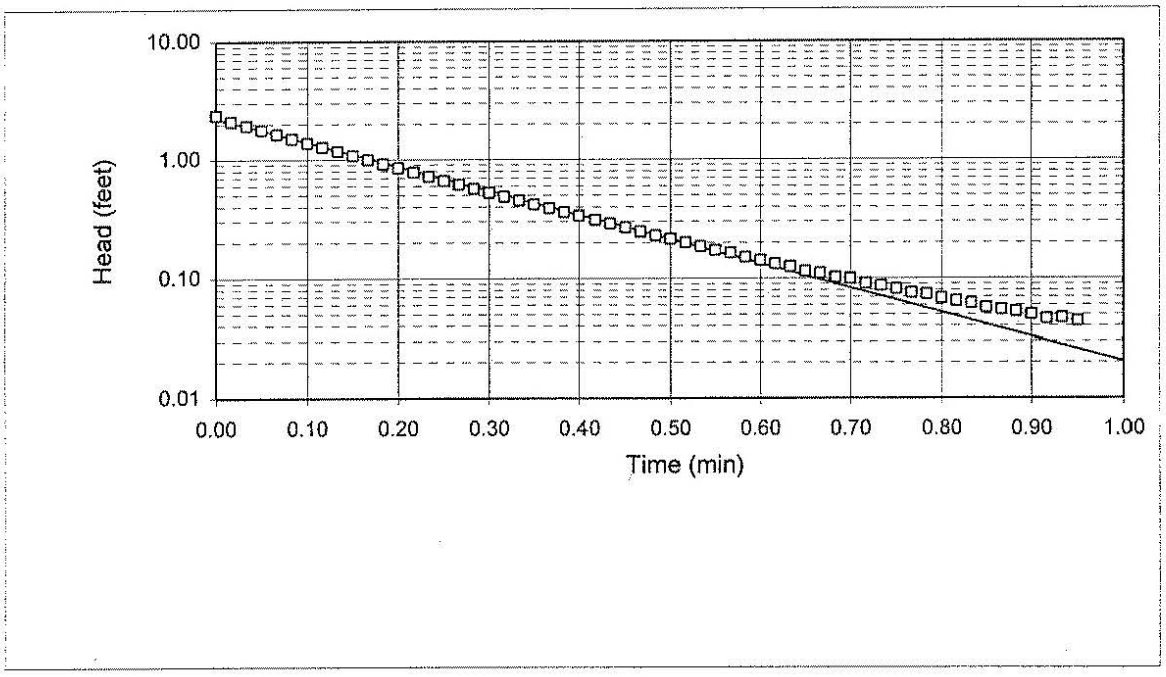
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.34
L_e =	9.4
$\ln(R_e/r_w)$	1.91
y_0 =	2.24
y_t =	0.02
t =	1.00

RESULTS

K=	1.69E-03	cm/sec
K=	4.78E+00	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-112-AS-RH1

WELL NO. PZ-112-AS-RH1

DATE	7/25/95	
INITAL HEAD ON TRANSDUCER	10.19	FEET H_2O
INITIAL DEPTH TO WATER	24.79	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	28.5	FEET (btoc)
BOTTOM OF OPEN INTERVAL	37.9	FEET (btoc)
SATURATED THICKNESS	100	FEET
WATER TABLE TO BOTTOM OF SCREEN	13.11	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	9.4	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	2.11	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	206	927	3	8.0808	0.00	26.90	2.11	1.00
305	206	927	4	8.3167	0.02	26.66	1.87	0.89
305	206	927	5	8.4263	0.03	26.55	1.76	0.84
305	206	927	6	8.5257	0.05	26.45	1.66	0.79
305	206	927	7	8.6166	0.07	26.36	1.57	0.75
305	206	927	8	8.6893	0.08	26.29	1.50	0.71
305	206	927	9	8.777	0.10	26.20	1.41	0.67
305	206	927	10	8.8401	0.12	26.14	1.35	0.64
305	206	927	11	8.9063	0.13	26.07	1.28	0.61
305	206	927	12	8.9705	0.15	26.01	1.22	0.58
305	206	927	13	9.0322	0.17	25.95	1.16	0.55
305	206	927	14	9.0879	0.18	25.89	1.10	0.52
305	206	927	15	9.1451	0.20	25.83	1.04	0.50
305	206	927	16	9.1968	0.22	25.78	0.99	0.47
305	206	927	17	9.2457	0.23	25.73	0.94	0.45
305	206	927	18	9.2924	0.25	25.69	0.90	0.43
305	206	927	19	9.331	0.27	25.65	0.86	0.41
305	206	927	20	9.3731	0.28	25.61	0.82	0.39
305	206	927	21	9.4275	0.30	25.55	0.76	0.36
305	206	927	22	9.464	0.32	25.52	0.73	0.34
305	206	927	23	9.4971	0.33	25.48	0.69	0.33
305	206	927	24	9.5336	0.35	25.45	0.66	0.31
305	206	927	25	9.5627	0.37	25.42	0.63	0.30
305	206	927	26	9.5944	0.38	25.39	0.60	0.28
305	206	927	27	9.6222	0.40	25.36	0.57	0.27
305	206	927	28	9.6506	0.42	25.33	0.54	0.26
305	206	927	29	9.677	0.43	25.30	0.51	0.24

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	206	927	30	9.702	0.45	25.28	0.49	0.23
305	206	927	31	9.7254	0.47	25.25	0.46	0.22
305	206	927	32	9.7484	0.48	25.23	0.44	0.21
305	206	927	33	9.7687	0.50	25.21	0.42	0.20
305	206	927	34	9.7907	0.52	25.19	0.40	0.19
305	206	927	35	9.8072	0.53	25.17	0.38	0.18
305	206	927	36	9.8284	0.55	25.15	0.36	0.17
305	206	927	37	9.8434	0.57	25.14	0.35	0.16
305	206	927	38	9.8597	0.58	25.12	0.33	0.16
305	206	927	39	9.8793	0.60	25.10	0.31	0.15
305	206	927	40	9.8906	0.62	25.09	0.30	0.14
305	206	927	41	9.9077	0.63	25.07	0.28	0.13
305	206	927	42	9.9219	0.65	25.06	0.27	0.13
305	206	927	43	9.9343	0.67	25.05	0.26	0.12
305	206	927	44	9.9423	0.68	25.04	0.25	0.12
305	206	927	45	9.9571	0.70	25.02	0.23	0.11
305	206	927	46	9.9673	0.72	25.01	0.22	0.11
305	206	927	47	9.9784	0.73	25.00	0.21	0.10
305	206	927	48	9.9858	0.75	24.99	0.20	0.10
305	206	927	49	9.9954	0.77	24.98	0.19	0.09
305	206	927	50	10.01	0.78	24.97	0.18	0.09
305	206	927	51	10.015	0.80	24.97	0.17	0.08
305	206	927	52	10.024	0.82	24.96	0.17	0.08
305	206	927	53	10.031	0.83	24.95	0.16	0.08
305	206	927	54	10.037	0.85	24.94	0.15	0.07
305	206	927	55	10.048	0.87	24.93	0.14	0.07
305	206	927	56	10.052	0.88	24.93	0.14	0.07
305	206	927	57	10.062	0.90	24.92	0.13	0.06
305	206	927	58	10.065	0.92	24.92	0.13	0.06
305	206	927	59	10.074	0.93	24.91	0.12	0.05
305	206	928	0	10.078	0.95	24.90	0.11	0.05
305	206	928	1	10.084	0.97	24.90	0.11	0.05
305	206	928	2	10.089	0.98	24.89	0.10	0.05
305	206	928	3	10.094	1.00	24.89	0.10	0.05
305	206	928	4	10.098	1.02	24.88	0.09	0.04
305	206	928	5	10.101	1.03	24.88	0.09	0.04
305	206	928	6	10.109	1.05	24.87	0.08	0.04
305	206	928	7	10.112	1.07	24.87	0.08	0.04
305	206	928	8	10.116	1.08	24.86	0.07	0.04
305	206	928	9	10.119	1.10	24.86	0.07	0.03
305	206	928	10	10.122	1.12	24.86	0.07	0.03
305	206	928	11	10.127	1.13	24.85	0.06	0.03
305	206	928	12	10.126	1.15	24.85	0.06	0.03
305	206	928	13	10.136	1.17	24.84	0.05	0.03
305	206	928	14	10.136	1.18	24.84	0.05	0.03

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	206	928	15	10.138	1.20	24.84	0.05	0.02
305	206	928	16	10.141	1.22	24.84	0.05	0.02
305	206	928	17	10.147	1.23	24.83	0.04	0.02
305	206	928	18	10.155	1.25	24.83	0.04	0.02
305	206	928	19	10.157	1.27	24.82	0.03	0.02
305	206	928	20	10.154	1.28	24.83	0.04	0.02
305	206	928	21	10.152	1.30	24.83	0.04	0.02
305	206	928	22	10.164	1.32	24.82	0.03	0.01
305	206	928	23	10.163	1.33	24.82	0.03	0.01
305	206	928	24	10.166	1.35	24.81	0.02	0.01

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-112-AS-RH1

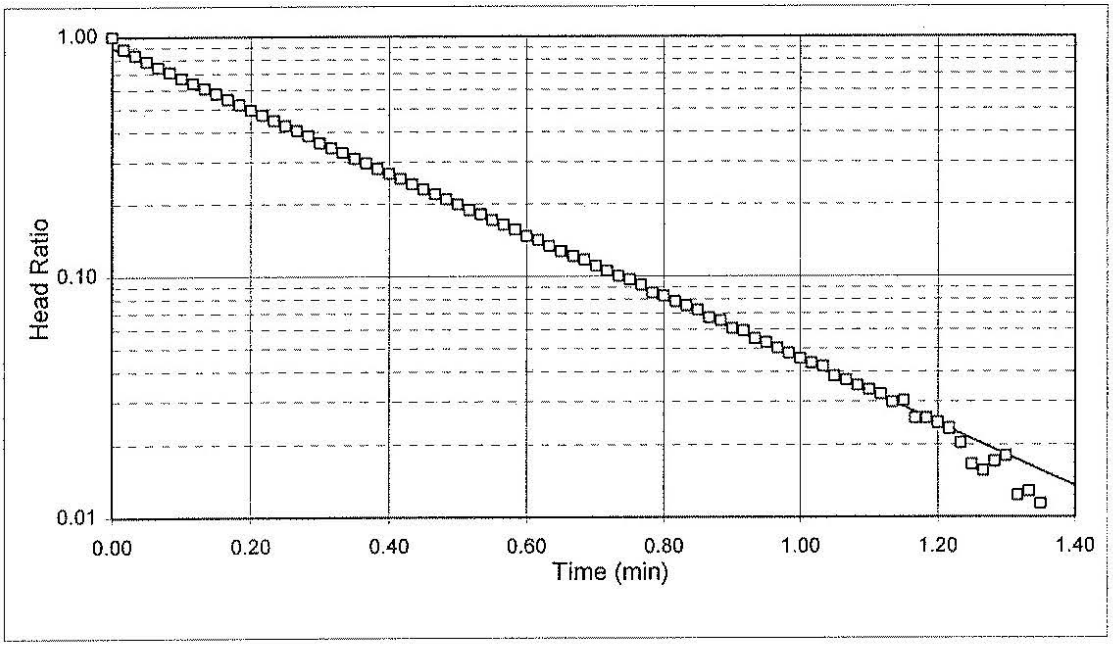
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = equivalent radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.34
L_e =	9.4
t_1 (min) =	0
t_2 (min) =	1.40
h_1/h_0 =	0.90
h_2/h_0 =	0.01

RESULTS

K=	1.86E-03	cm/sec
K=	5.28E+00	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

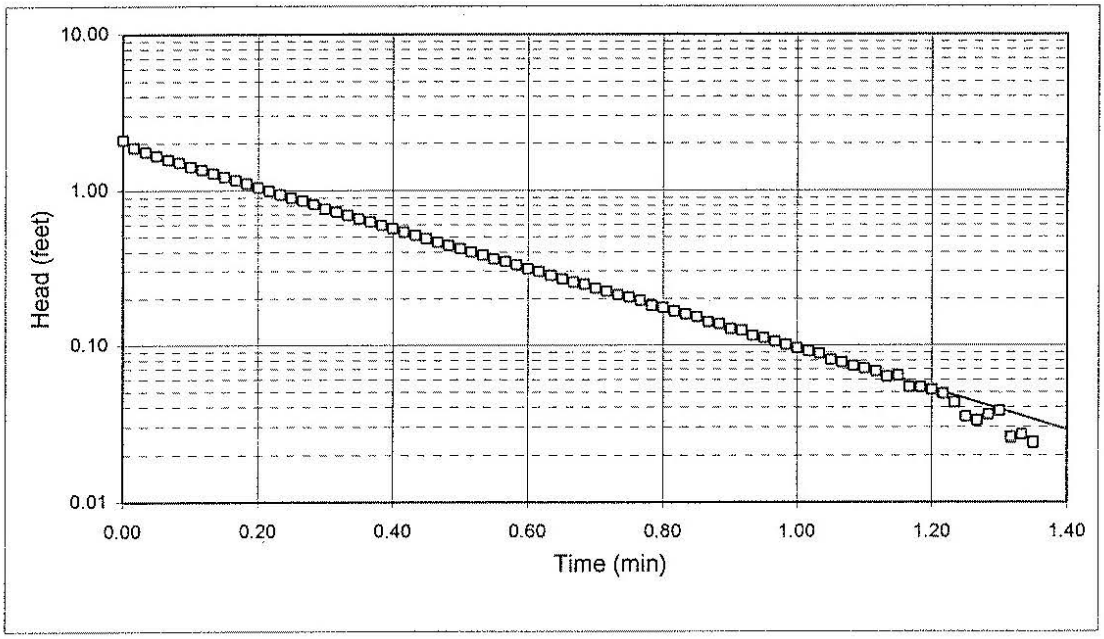
BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-112-AS-RH1

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS	
r_c =	0.08		
r_w =	0.34		
L_e =	9.4	K=	1.09E-03 cm/sec
$\ln(R_e/r_w)$	1.91	K=	3.08E+00 ft/day
y_0 =	2.00		
y_t =	0.03		
t =	1.40		



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

FALLING HEAD TEST PZ-113-AS

WELL NO. PZ-113-AS

DATE	7/25/95	
INITAL HEAD ON TRANSDUCER	9.9	FEET H_2O
INITIAL DEPTH TO WATER	26.27	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	26.5	FEET (btoc)
BOTTOM OF OPEN INTERVAL	41.5	FEET (btoc)
SATURATED THICKNESS	80	FEET
WATER TABLE TO BOTTOM OF SCREEN	15.23	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	15	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	0.98	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	206	1447	2	10.881	0.00	25.29	0.98	1.000
1995	206	1447	3	10.804	0.02	25.37	0.90	0.922
1995	206	1447	4	10.62	0.03	25.55	0.72	0.734
1995	206	1447	5	10.323	0.05	25.85	0.42	0.431
1995	206	1447	6	10.174	0.07	26.00	0.27	0.279
1995	206	1447	7	10.027	0.08	26.14	0.13	0.129
1995	206	1447	8	9.856	0.10	26.23	0.04	0.045
1995	206	1447	10	9.8452	0.13	26.22	0.05	0.056
1995	206	1447	11	9.9191	0.15	26.25	0.02	0.019
1995	206	1447	12	9.8198	0.17	26.19	0.08	0.082
1995	206	1447	13	9.8705	0.18	26.24	0.03	0.030
1995	206	1447	15	9.906	0.22	26.26	0.01	0.006
1995	206	1447	16	9.9122	0.23	26.26	0.01	0.012
1995	206	1447	17	9.9082	0.25	26.26	0.01	0.008
1995	206	1447	18	9.9086	0.27	26.26	0.01	0.009
1995	206	1447	19	9.9071	0.28	26.26	0.01	0.007
1995	206	1447	20	9.9054	0.30	26.26	0.01	0.006

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-113-AS

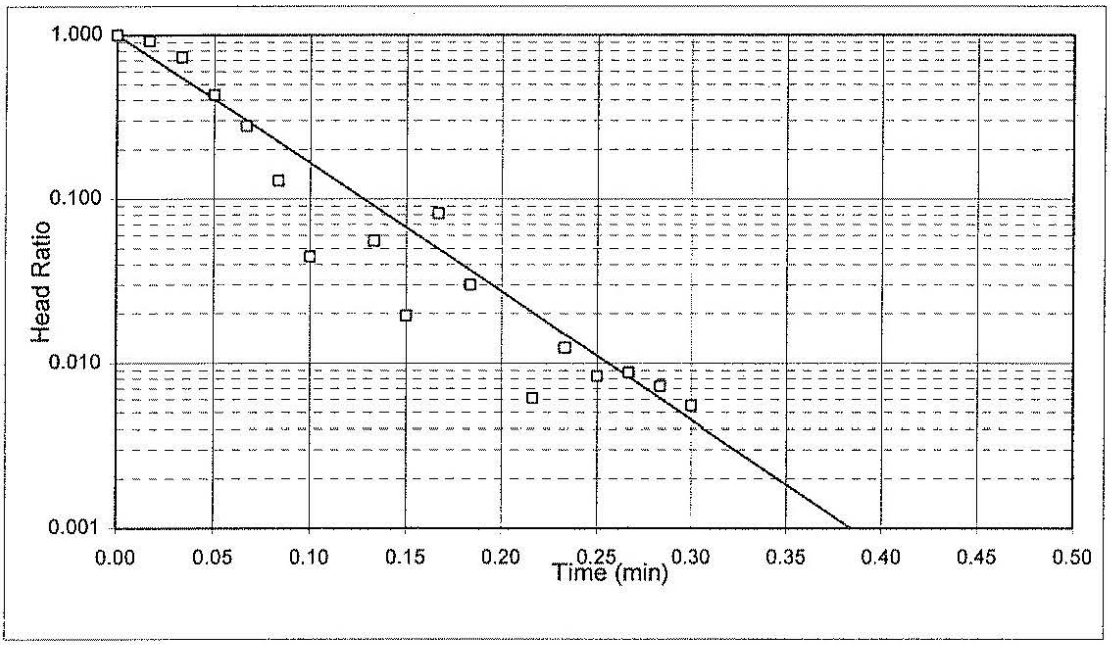
$$K = \frac{r_c^{\,2}}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.34
L_e =	15
t_1 (min) =	0
t_2 (min) =	0.38
h_1/h_0 =	1.00
h_2/h_0 =	0.00

RESULTS

K=	7.99E-03	cm/sec
K=	2.26E+01	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

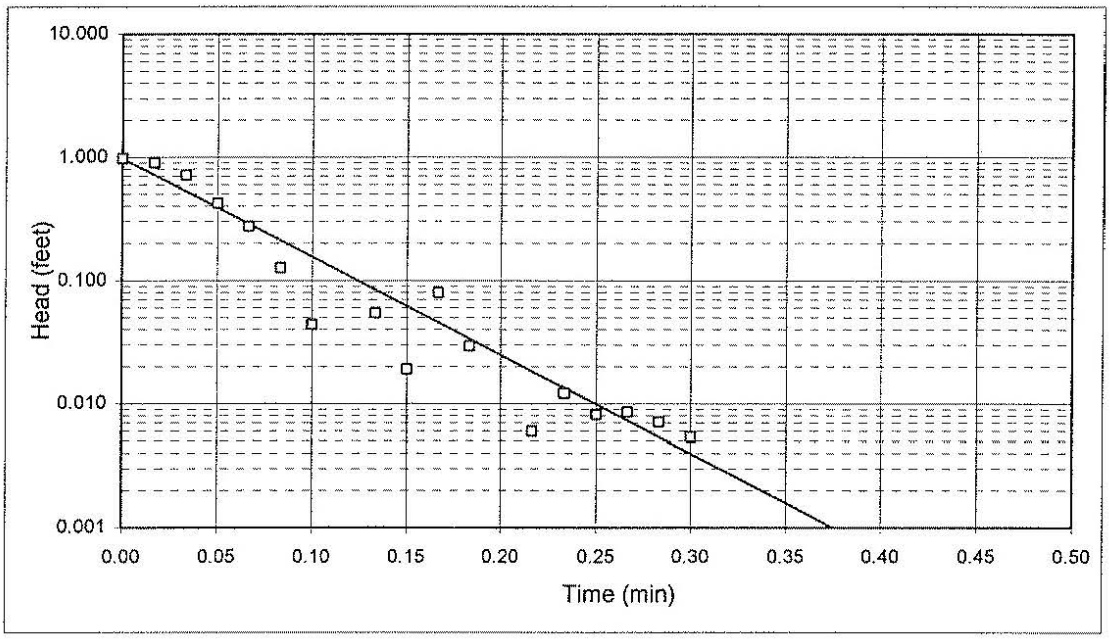
BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-113-AS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
r_w =	0.34			
L_e =	15	K=	5.08E-03	cm/sec
$\ln(R_e/r_w)$	2.35	K=	1.44E+01	ft/day
y_0 =	0.98			
y_t =	0.00			
t =	0.38			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

RISING HEAD TEST PZ-113-AS

WELL NO. PZ-113-AS

DATE	7/25/95	
INITAL HEAD ON TRANSDUCER	9.9	FEET H_2O
INITIAL DEPTH TO WATER	26.27	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	26.5	FEET (btoc)
BOTTOM OF OPEN INTERVAL	41.5	FEET (btoc)
SATURATED THICKNESS	80	FEET
WATER TABLE TO BOTTOM OF SCREEN	15.23	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	15	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	1.53	FEET
MAX. HEAD IN SCREEN?	Y	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	206	1449	2	8.3689	0.00	27.80	1.53	1.00
1995	206	1449	3	9.045	0.02	27.13	0.86	0.56
1995	206	1449	4	9.4283	0.03	26.74	0.47	0.31
1995	206	1449	5	9.6252	0.05	26.54	0.27	0.18
1995	206	1449	6	9.732	0.07	26.44	0.17	0.11
1995	206	1449	7	9.7835	0.08	26.39	0.12	0.08
1995	206	1449	8	9.8142	0.10	26.36	0.09	0.06
1995	206	1449	9	9.8263	0.12	26.34	0.07	0.05

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-113-AS

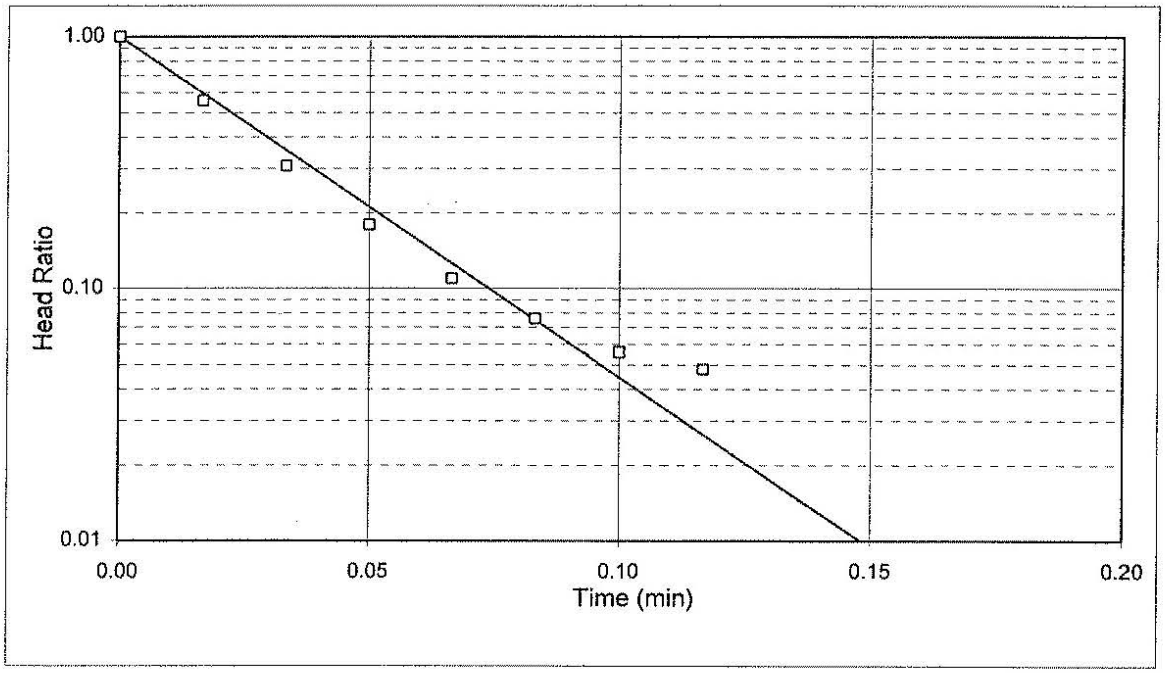
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.34
L_e =	15
t_1 (min) =	0
t_2 (min) =	0.15
h_1/h_0 =	1.00
h_2/h_0 =	0.01

RESULTS

K=	1.38E-02	cm/sec
K=	3.91E+01	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-113-AS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

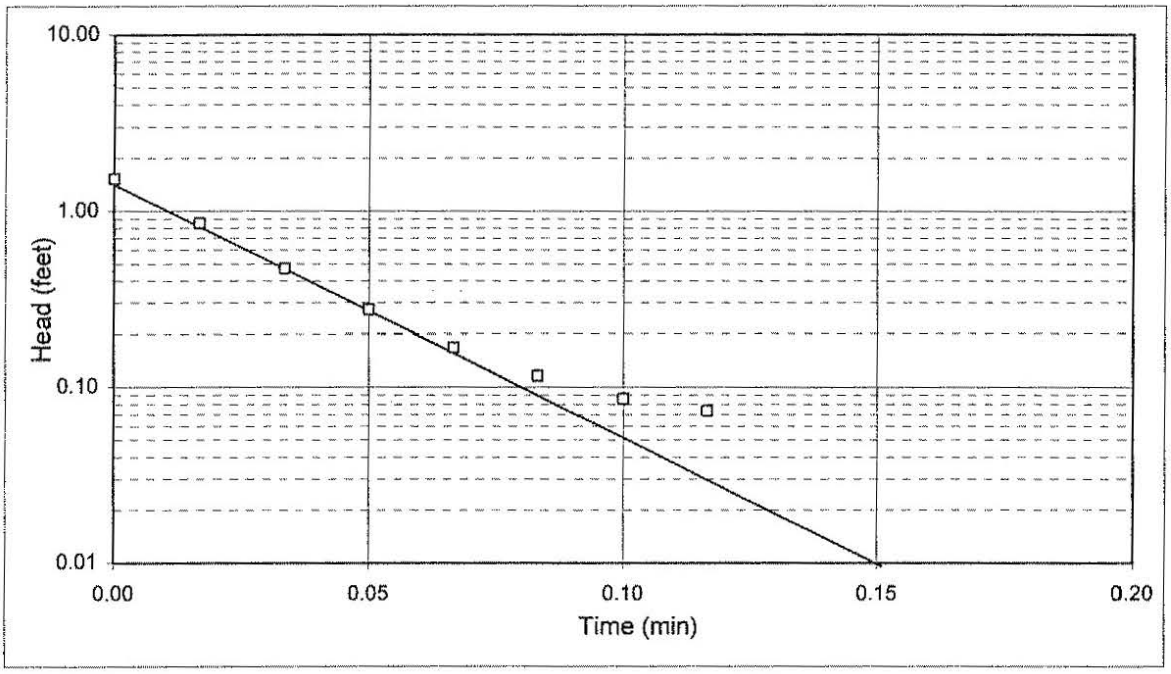
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.20
r_w =	0.34
L_e =	15
$\ln(R_e/r_w)$	2.35
y_0 =	1.41
y_t =	0.01
t =	0.15

RESULTS

K=	5.31E-02	cm/sec
K=	1.51E+02	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

FALLING HEAD TEST PZ-113-AD (TEST 1)

WELL NO.	PZ-113-AD (TEST 1)	
DATE	7/25/95	
INITAL HEAD ON TRANSDUCER	15.28	FEET H_2O
INITIAL DEPTH TO WATER	26.33	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	10.25	INCHES
TOP OF OPEN INTERVAL	90.7	FEET (btoc)
BOTTOM OF OPEN INTERVAL	110.3	FEET (btoc)
SATURATED THICKNESS	85	FEET
WATER TABLE TO BOTTOM OF SCREEN	83.97	FEET
EQUIVALENT DIAMETER	5.86	INCHES
OPEN INTERVAL LENGTH	19.6	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	1.37	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	206	1404	2	16.649	0.00	24.96	1.37	1.00
1995	206	1404	3	15.649	0.02	25.96	0.37	0.27
1995	206	1404	4	15.688	0.03	25.92	0.41	0.30
1995	206	1404	5	14.46	0.05	25.51	0.82	0.60
1995	206	1404	6	14.767	0.07	25.82	0.51	0.37
1995	206	1404	7	14.47	0.08	25.52	0.81	0.59
1995	206	1404	8	14.736	0.10	25.79	0.54	0.40
1995	206	1404	9	15.135	0.12	26.19	0.15	0.11
1995	206	1404	10	15.514	0.13	26.10	0.23	0.17
1995	206	1404	11	15.75	0.15	25.86	0.47	0.34
1995	206	1404	12	15.801	0.17	25.81	0.52	0.38
1995	206	1404	13	15.681	0.18	25.93	0.40	0.29
1995	206	1404	14	15.451	0.20	26.16	0.17	0.12
1995	206	1404	15	15.204	0.22	26.25	0.08	0.06
1995	206	1404	16	15.007	0.23	26.06	0.27	0.20
1995	206	1404	17	14.941	0.25	25.99	0.34	0.25
1995	206	1404	18	14.985	0.27	26.04	0.30	0.22
1995	206	1404	19	15.126	0.28	26.18	0.15	0.11
1995	206	1404	21	15.422	0.32	26.19	0.14	0.10
1995	206	1404	22	15.5	0.33	26.11	0.22	0.16
1995	206	1404	23	15.494	0.35	26.12	0.21	0.16
1995	206	1404	24	15.417	0.37	26.19	0.14	0.10
1995	206	1404	27	15.147	0.42	26.20	0.13	0.10
1995	206	1404	28	15.136	0.43	26.19	0.14	0.11
1995	206	1404	29	15.17	0.45	26.22	0.11	0.08
1995	206	1404	30	15.237	0.47	26.29	0.04	0.03

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	206	1404	31	15.305	0.48	26.31	0.02	0.02
1995	206	1404	32	15.356	0.50	26.25	0.08	0.06
1995	206	1404	33	15.372	0.52	26.24	0.09	0.07
1995	206	1404	34	15.358	0.53	26.25	0.08	0.06
1995	206	1404	35	15.317	0.55	26.29	0.04	0.03
1995	206	1404	36	15.272	0.57	26.32	0.01	0.01
1995	206	1404	37	15.235	0.58	26.29	0.05	0.03
1995	206	1404	38	15.215	0.60	26.27	0.06	0.05
1995	206	1404	39	15.219	0.62	26.27	0.06	0.04
1995	206	1404	40	15.239	0.63	26.29	0.04	0.03
1995	206	1404	41	15.269	0.65	26.32	0.01	0.01
1995	206	1404	42	15.298	0.67	26.31	0.02	0.01
1995	206	1404	43	15.314	0.68	26.30	0.03	0.02
1995	206	1404	44	15.318	0.70	26.29	0.04	0.03
1995	206	1404	45	15.305	0.72	26.31	0.02	0.02
1995	206	1404	46	15.285	0.73	26.33	0.01	0.00

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-113-AD (TEST 1)

$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

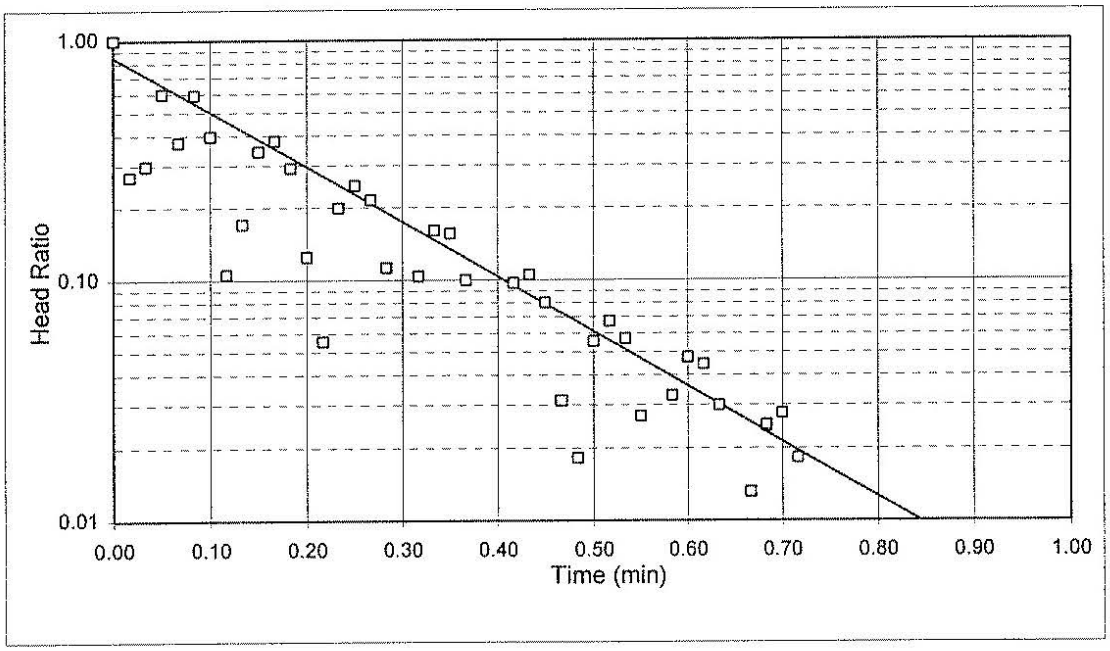
85

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.43
L_e =	19.6
t_1 (min) =	0
t_2 (min) =	0.84
h_1/h_0 =	0.85
h_2/h_0 =	0.01

RESULTS

K=	1.81E-03	cm/sec
K=	5.14E+00	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-113-AD (TEST 1)

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

85

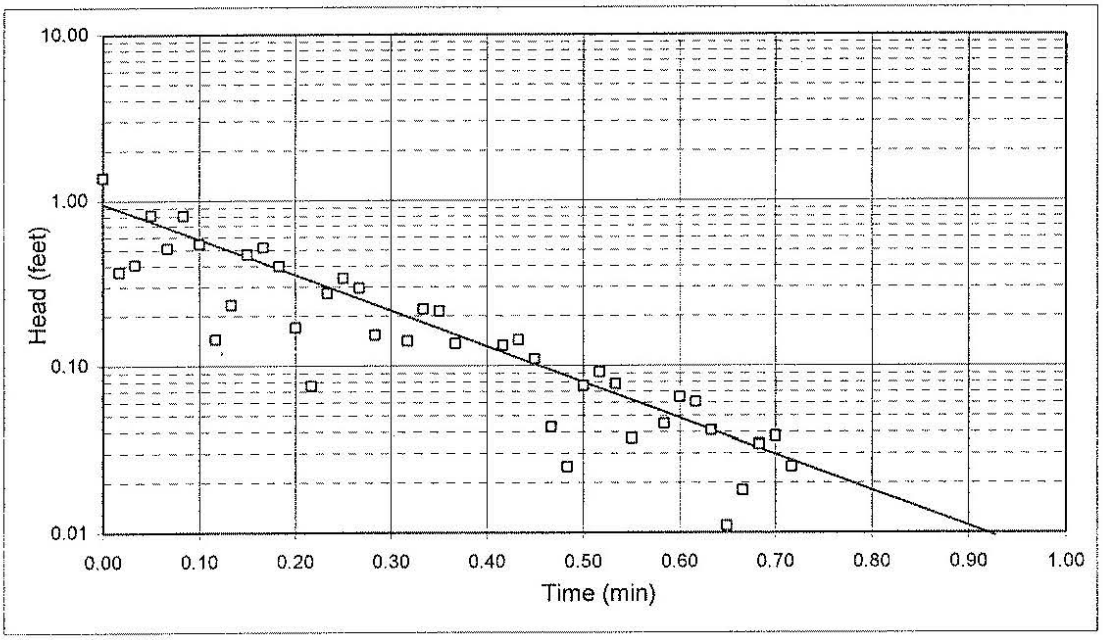
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.43
L_e =	19.6
$\ln(R_e/r_w)$	3.35
y_0 =	0.95
y_t =	0.01
t =	0.93

RESULTS

K=	1.49E-03	cm/sec
K=	4.24E+00	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

FALLING HEAD TEST PZ-113-AD (TEST 2)

WELL NO.	PZ-113-AD (TEST 2)	
DATE	7/25/95	
INITAL HEAD ON TRANSDUCER	15.28	FEET H_2O
INITIAL DEPTH TO WATER	26.33	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	10.25	INCHES
TOP OF OPEN INTERVAL	90.7	FEET (btoc)
BOTTOM OF OPEN INTERVAL	110.3	FEET (btoc)
SATURATED THICKNESS	80	FEET
WATER TABLE TO BOTTOM OF SCREEN	83.97	FEET
EQUIVALENT DIAMETER	5.86	INCHES
OPEN INTERVAL LENGTH	19.6	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	1.20	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	206	1407	5	16.477	0.00	25.13	1.20	1.00
305	206	1407	6	16.289	0.02	25.32	1.01	0.84
305	206	1407	7	15.788	0.03	25.82	0.51	0.42
305	206	1407	8	15.155	0.05	26.21	0.13	0.10
305	206	1407	9	14.646	0.07	25.70	0.63	0.53
305	206	1407	10	14.418	0.08	25.47	0.86	0.72
305	206	1407	11	14.524	0.10	25.57	0.76	0.63
305	206	1407	12	14.877	0.12	25.93	0.40	0.34
305	206	1407	13	15.313	0.13	26.30	0.03	0.03
305	206	1407	14	15.668	0.15	25.94	0.39	0.32
305	206	1407	15	15.832	0.17	25.78	0.55	0.46
305	206	1407	16	15.777	0.18	25.83	0.50	0.42
305	206	1407	17	15.553	0.20	26.06	0.27	0.23
305	206	1407	18	15.25	0.22	26.30	0.03	0.03
305	206	1407	19	14.993	0.23	26.04	0.29	0.24
305	206	1407	20	14.86	0.25	25.91	0.42	0.35
305	206	1407	21	14.884	0.27	25.93	0.40	0.33
305	206	1407	22	15.032	0.28	26.08	0.25	0.21
305	206	1407	23	15.241	0.30	26.29	0.04	0.03
305	206	1407	24	15.427	0.32	26.18	0.15	0.12
305	206	1407	25	15.531	0.33	26.08	0.25	0.21
305	206	1407	26	15.526	0.35	26.08	0.25	0.21
305	206	1407	27	15.43	0.37	26.18	0.15	0.13
305	206	1407	28	15.287	0.38	26.32	0.01	0.01
305	206	1407	29	15.152	0.40	26.20	0.13	0.11
305	206	1407	30	15.073	0.42	26.12	0.21	0.17

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	206	1407	31	15.065	0.43	26.12	0.22	0.18
305	206	1407	32	15.126	0.45	26.18	0.15	0.13
305	206	1407	33	15.226	0.47	26.28	0.05	0.05
305	206	1407	34	15.324	0.48	26.29	0.04	0.04
305	206	1407	35	15.379	0.50	26.23	0.10	0.08
305	206	1407	36	15.386	0.52	26.22	0.11	0.09
305	206	1407	37	15.346	0.53	26.26	0.07	0.06

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-113-AD (TEST 2)

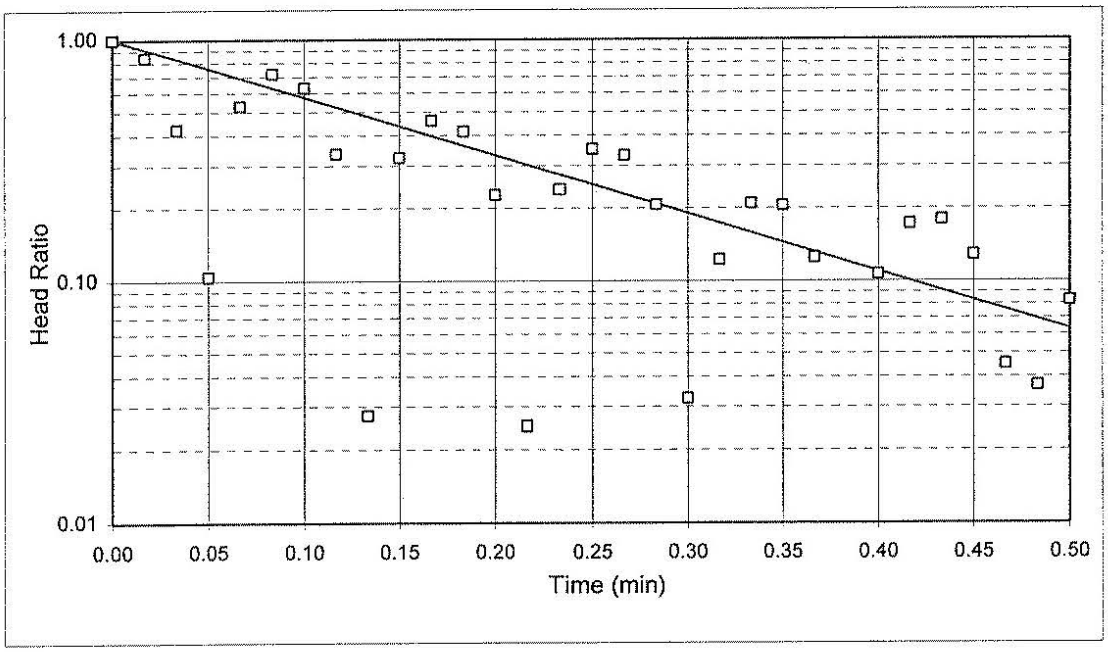
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.43
L_e =	19.6
t_1 (min) =	0
t_2 (min) =	0.50
h_1/h_0 =	1.00
h_2/h_0 =	0.06

RESULTS

K=	1.90E-03	cm/sec
K=	5.39E+00	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-113-AD (TEST 2)

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

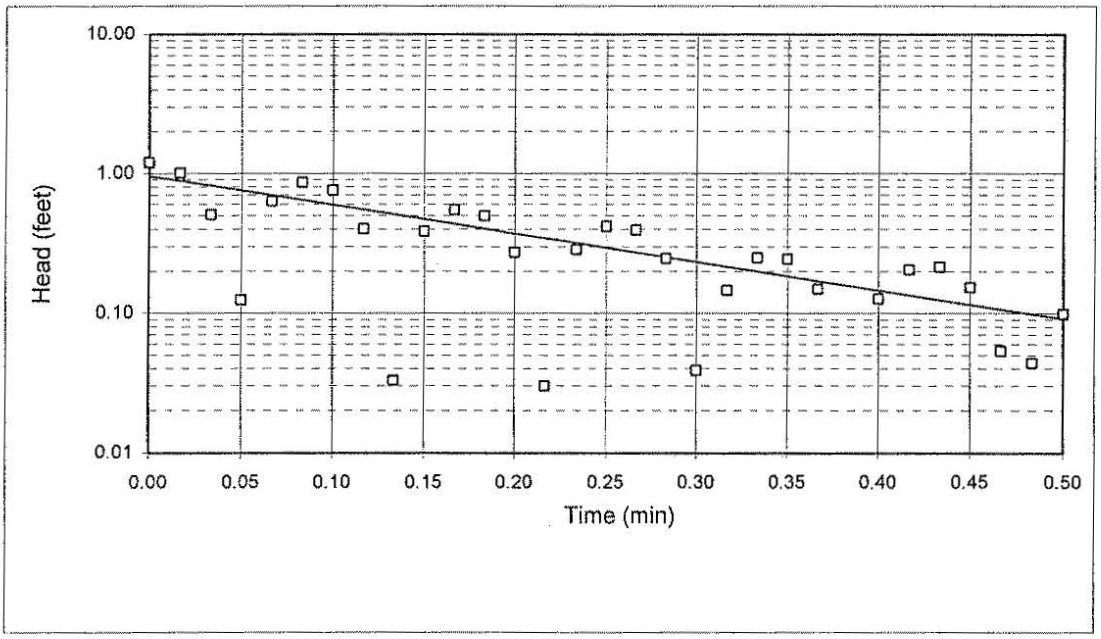
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.43
L_e =	19.6
$\ln(R_e/r_w)$	#N/A
y_0 =	0.95
y_t =	0.09
t =	0.50

RESULTS

K=	#N/A	cm/sec
K=	#N/A	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

FALLING HEAD TEST PZ-113-SS

WELL NO. PZ-113-SS

DATE	7/25/95	
INITAL HEAD ON TRANSDUCER	15.008	FEET H_2O
INITIAL DEPTH TO WATER	26.61	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	146.3	FEET (btoc)
BOTTOM OF OPEN INTERVAL	160.8	FEET (btoc)
SATURATED THICKNESS	190	FEET
WATER TABLE TO BOTTOM OF SCREEN	134.19	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	14.5	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.83	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	206	1117	35	18.834	0.00	22.78	3.83	1.00
1995	206	1117	37	18.248	0.03	23.37	3.24	0.85
1995	206	1117	39	18.23	0.07	23.39	3.22	0.84
1995	206	1117	41	18.226	0.10	23.39	3.22	0.84
1995	206	1117	43	18.225	0.13	23.39	3.22	0.84
1995	206	1117	45	18.226	0.17	23.39	3.22	0.84
1995	206	1117	47	18.228	0.20	23.39	3.22	0.84
1995	206	1117	49	18.224	0.23	23.39	3.22	0.84
1995	206	1117	51	18.223	0.27	23.40	3.22	0.84
1995	206	1117	53	18.224	0.30	23.39	3.22	0.84
1995	206	1117	55	18.225	0.33	23.39	3.22	0.84
1995	206	1117	57	18.224	0.37	23.39	3.22	0.84
1995	206	1117	59	18.224	0.40	23.39	3.22	0.84
1995	206	1118	1	18.223	0.43	23.40	3.22	0.84
1995	206	1118	3	18.224	0.47	23.39	3.22	0.84
1995	206	1118	5	18.224	0.50	23.39	3.22	0.84
1995	206	1118	8	18.223	0.55	23.40	3.22	0.84
1995	206	1118	10	18.222	0.58	23.40	3.21	0.84
1995	206	1118	12	18.223	0.62	23.40	3.22	0.84
1995	206	1118	14	18.223	0.65	23.40	3.22	0.84
1995	206	1118	16	18.224	0.68	23.39	3.22	0.84
1995	206	1118	18	18.222	0.72	23.40	3.21	0.84
1995	206	1118	20	18.222	0.75	23.40	3.21	0.84
1995	206	1118	22	18.222	0.78	23.40	3.21	0.84
1995	206	1118	24	18.221	0.82	23.40	3.21	0.84
1995	206	1118	26	18.222	0.85	23.40	3.21	0.84
1995	206	1118	28	18.221	0.88	23.40	3.21	0.84
1995	206	1118	30	18.219	0.92	23.40	3.21	0.84
1995	206	1118	32	18.221	0.95	23.40	3.21	0.84
1995	206	1118	34	18.22	0.98	23.40	3.21	0.84
1995	206	1118	36	18.221	1.02	23.40	3.21	0.84
1995	206	1118	38	18.219	1.05	23.40	3.21	0.84
1995	206	1118	40	18.218	1.08	23.40	3.21	0.84
1995	206	1118	42	18.219	1.12	23.40	3.21	0.84

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	206	1118	44	18.22	1.15	23.40	3.21	0.84
1995	206	1118	46	18.218	1.18	23.40	3.21	0.84
1995	206	1118	48	18.219	1.22	23.40	3.21	0.84
1995	206	1118	50	18.216	1.25	23.40	3.21	0.84
1995	206	1118	52	18.219	1.28	23.40	3.21	0.84
1995	206	1118	54	18.219	1.32	23.40	3.21	0.84
1995	206	1118	56	18.222	1.35	23.40	3.21	0.84
1995	206	1118	58	18.219	1.38	23.40	3.21	0.84
1995	206	1119	0	18.217	1.42	23.40	3.21	0.84
1995	206	1119	10	18.215	1.58	23.40	3.21	0.84
1995	206	1119	20	18.213	1.75	23.41	3.21	0.84
1995	206	1119	30	18.211	1.92	23.41	3.20	0.84
1995	206	1119	40	18.21	2.08	23.41	3.20	0.84
1995	206	1119	50	18.205	2.25	23.41	3.20	0.84
1995	206	1120	0	18.202	2.42	23.42	3.19	0.83
1995	206	1120	10	18.202	2.58	23.42	3.19	0.83
1995	206	1120	20	18.197	2.75	23.42	3.19	0.83
1995	206	1120	30	18.196	2.92	23.42	3.19	0.83
1995	206	1120	40	18.189	3.08	23.43	3.18	0.83
1995	206	1120	50	18.184	3.25	23.43	3.18	0.83
1995	206	1121	0	18.184	3.42	23.43	3.18	0.83
1995	206	1121	10	18.181	3.58	23.44	3.17	0.83
1995	206	1121	20	18.173	3.75	23.45	3.17	0.83
1995	206	1121	30	18.168	3.92	23.45	3.16	0.83
1995	206	1122	0	18.159	4.42	23.46	3.15	0.82
1995	206	1123	0	18.127	5.42	23.49	3.12	0.82
1995	206	1124	0	18.092	6.42	23.53	3.08	0.81
1995	206	1125	0	18.055	7.42	23.56	3.05	0.80
1995	206	1126	0	18.046	8.42	23.57	3.04	0.79
1995	206	1127	0	18.011	9.42	23.61	3.00	0.78
1995	206	1128	0	17.981	10.42	23.64	2.97	0.78
1995	206	1129	0	17.946	11.42	23.67	2.94	0.77
1995	206	1130	0	17.913	12.42	23.71	2.91	0.76
1995	206	1131	0	17.884	13.42	23.73	2.88	0.75
1995	206	1132	0	17.848	14.42	23.77	2.84	0.74
1995	206	1133	0	17.817	15.42	23.80	2.81	0.73
1995	206	1134	0	17.786	16.42	23.83	2.78	0.73
1995	206	1135	0	17.754	17.42	23.86	2.75	0.72
1995	206	1136	0	17.725	18.42	23.89	2.72	0.71
1995	206	1137	0	17.695	19.42	23.92	2.69	0.70
1995	206	1138	0	17.66	20.42	23.96	2.65	0.69
1995	206	1139	0	17.634	21.42	23.98	2.63	0.69
1995	206	1140	0	17.603	22.42	24.02	2.60	0.68
1995	206	1141	0	17.574	23.42	24.04	2.57	0.67
1995	206	1142	0	17.546	24.42	24.07	2.54	0.66
1995	206	1143	0	17.515	25.42	24.10	2.51	0.66
1995	206	1144	0	17.488	26.42	24.13	2.48	0.65
1995	206	1145	0	17.462	27.42	24.16	2.45	0.64
1995	206	1146	0	17.433	28.42	24.19	2.43	0.63
1995	206	1147	0	17.406	29.42	24.21	2.40	0.63
1995	206	1148	0	17.378	30.42	24.24	2.37	0.62
1995	206	1149	0	17.35	31.42	24.27	2.34	0.61
1995	206	1150	0	17.322	32.42	24.30	2.31	0.60

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	206	1151	0	17.298	33.42	24.32	2.29	0.60
1995	206	1152	0	17.273	34.42	24.35	2.27	0.59
1995	206	1153	0	17.244	35.42	24.37	2.24	0.58
1995	206	1154	0	17.217	36.42	24.40	2.21	0.58
1995	206	1155	0	17.194	37.42	24.42	2.19	0.57
1995	206	1156	0	17.168	38.42	24.45	2.16	0.56
1995	206	1157	0	17.144	39.42	24.47	2.14	0.56
1995	206	1158	0	17.123	40.42	24.50	2.12	0.55
1995	206	1159	0	17.099	41.42	24.52	2.09	0.55
1995	206	1200	0	17.074	42.42	24.54	2.07	0.54
1995	206	1201	0	17.052	43.42	24.57	2.04	0.53
1995	206	1202	0	17.031	44.42	24.59	2.02	0.53
1995	206	1203	0	17.008	45.42	24.61	2.00	0.52
1995	206	1204	0	16.987	46.42	24.63	1.98	0.52
1995	206	1205	0	16.965	47.42	24.65	1.96	0.51
1995	206	1206	0	16.943	48.42	24.68	1.94	0.51
1995	206	1207	0	16.922	49.42	24.70	1.91	0.50
1995	206	1208	0	16.898	50.42	24.72	1.89	0.49
1995	206	1209	0	16.879	51.42	24.74	1.87	0.49
1995	206	1210	0	16.86	52.42	24.76	1.85	0.48
1995	206	1211	0	16.841	53.42	24.78	1.83	0.48
1995	206	1212	0	16.82	54.42	24.80	1.81	0.47
1995	206	1213	0	16.8	55.42	24.82	1.79	0.47
1995	206	1214	0	16.781	56.42	24.84	1.77	0.46
1995	206	1215	0	16.764	57.42	24.85	1.76	0.46
1995	206	1216	0	16.745	58.42	24.87	1.74	0.45
1995	206	1217	0	16.726	59.42	24.89	1.72	0.45
1995	206	1218	0	16.709	60.42	24.91	1.70	0.44
1995	206	1219	0	16.691	61.42	24.93	1.68	0.44
1995	206	1220	0	16.672	62.42	24.95	1.66	0.43
1995	206	1221	0	16.654	63.42	24.96	1.65	0.43
1995	206	1222	0	16.634	64.42	24.98	1.63	0.42
1995	206	1223	0	16.617	65.42	25.00	1.61	0.42
1995	206	1224	0	16.599	66.42	25.02	1.59	0.42
1995	206	1225	0	16.584	67.42	25.03	1.58	0.41
1995	206	1226	0	16.569	68.42	25.05	1.56	0.41
1995	206	1227	0	16.551	69.42	25.07	1.54	0.40
1995	206	1228	0	16.537	70.42	25.08	1.53	0.40
1995	206	1229	0	16.517	71.42	25.10	1.51	0.39
1995	206	1230	0	16.504	72.42	25.11	1.50	0.39
1995	206	1231	0	16.487	73.42	25.13	1.48	0.39
1995	206	1232	0	16.47	74.42	25.15	1.46	0.38
1995	206	1233	0	16.453	75.42	25.17	1.45	0.38
1995	206	1234	0	16.437	76.42	25.18	1.43	0.37
1995	206	1235	0	16.425	77.42	25.19	1.42	0.37
1995	206	1236	0	16.411	78.42	25.21	1.40	0.37
1995	206	1237	0	16.397	79.42	25.22	1.39	0.36
1995	206	1238	0	16.38	80.42	25.24	1.37	0.36
1995	206	1239	0	16.367	81.42	25.25	1.36	0.36
1995	206	1240	0	16.352	82.42	25.27	1.34	0.35
1995	206	1241	0	16.338	83.42	25.28	1.33	0.35
1995	206	1242	0	16.325	84.42	25.29	1.32	0.34
1995	206	1243	0	16.313	85.42	25.31	1.31	0.34

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	206	1244	0	16.298	86.42	25.32	1.29	0.34
1995	206	1245	0	16.285	87.42	25.33	1.28	0.33
1995	206	1246	0	16.27	88.42	25.35	1.26	0.33
1995	206	1247	0	16.257	89.42	25.36	1.25	0.33
1995	206	1248	0	16.246	90.42	25.37	1.24	0.32
1995	206	1249	0	16.234	91.42	25.38	1.23	0.32
1995	206	1250	0	16.222	92.42	25.40	1.21	0.32
1995	206	1251	0	16.206	93.42	25.41	1.20	0.31
1995	206	1252	0	16.193	94.42	25.43	1.19	0.31
1995	206	1253	0	16.179	95.42	25.44	1.17	0.31
1995	206	1254	0	16.166	96.42	25.45	1.16	0.30
1995	206	1255	0	16.152	97.42	25.47	1.14	0.30
1995	206	1256	0	16.137	98.42	25.48	1.13	0.30
1995	206	1257	0	16.129	99.42	25.49	1.12	0.29
1995	206	1258	0	16.117	100.42	25.50	1.11	0.29
1995	206	1259	0	16.106	101.42	25.51	1.10	0.29
1995	206	1300	0	16.095	102.42	25.52	1.09	0.28
1995	206	1301	0	16.083	103.42	25.54	1.08	0.28
1995	206	1302	0	16.071	104.42	25.55	1.06	0.28
1995	206	1303	0	16.06	105.42	25.56	1.05	0.27
1995	206	1304	0	16.051	106.42	25.57	1.04	0.27
1995	206	1305	0	16.036	107.42	25.58	1.03	0.27
1995	206	1306	0	16.028	108.42	25.59	1.02	0.27
1995	206	1307	0	16.02	109.42	25.60	1.01	0.26
1995	206	1308	0	16.007	110.42	25.61	1.00	0.26
1995	206	1309	0	15.995	111.42	25.62	0.99	0.26
1995	206	1310	0	15.983	112.42	25.64	0.98	0.25
1995	206	1311	0	15.975	113.42	25.64	0.97	0.25
1995	206	1312	0	15.964	114.42	25.65	0.96	0.25
1995	206	1313	0	15.955	115.42	25.66	0.95	0.25
1995	206	1314	0	15.946	116.42	25.67	0.94	0.25
1995	206	1315	0	15.936	117.42	25.68	0.93	0.24
1995	206	1316	0	15.925	118.42	25.69	0.92	0.24
1995	206	1317	0	15.917	119.42	25.70	0.91	0.24
1995	206	1318	0	15.905	120.42	25.71	0.90	0.23
1995	206	1319	0	15.896	121.42	25.72	0.89	0.23
1995	206	1320	0	15.886	122.42	25.73	0.88	0.23
1995	206	1321	0	15.878	123.42	25.74	0.87	0.23
1995	206	1322	0	15.87	124.42	25.75	0.86	0.23

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-113-SS

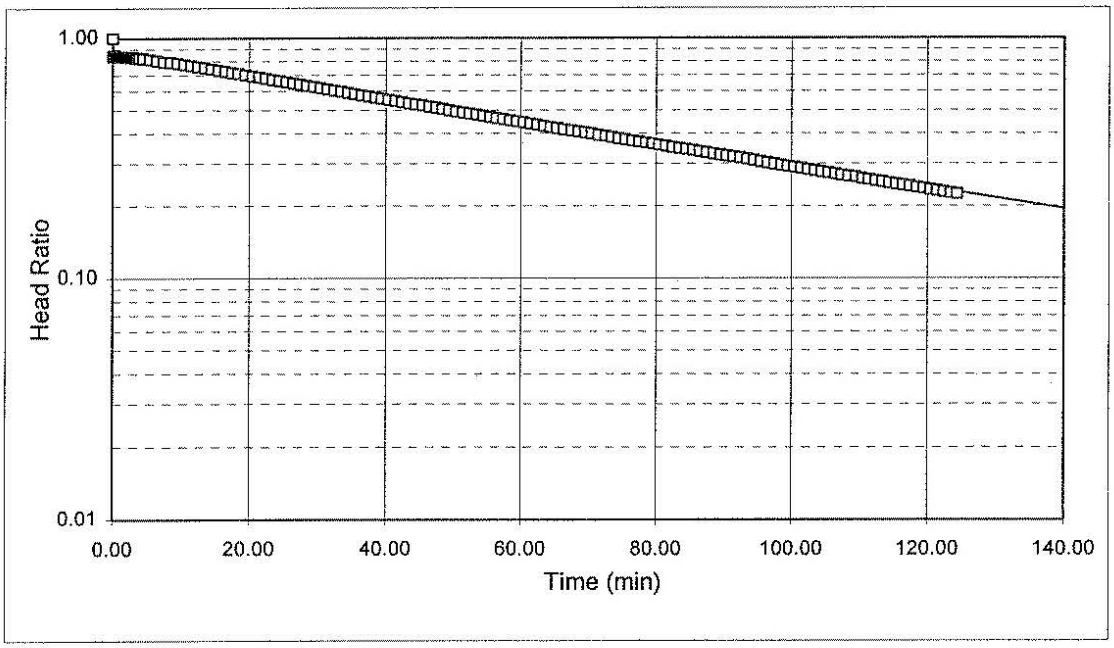
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	14.5
t_1 (min) =	9.42
t_2 (min) =	140.00
h_1/h_0 =	0.78
h_2/h_0 =	0.19

RESULTS

K=	5.24E-06	cm/sec
K=	1.49E-02	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/9/96

BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-113-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

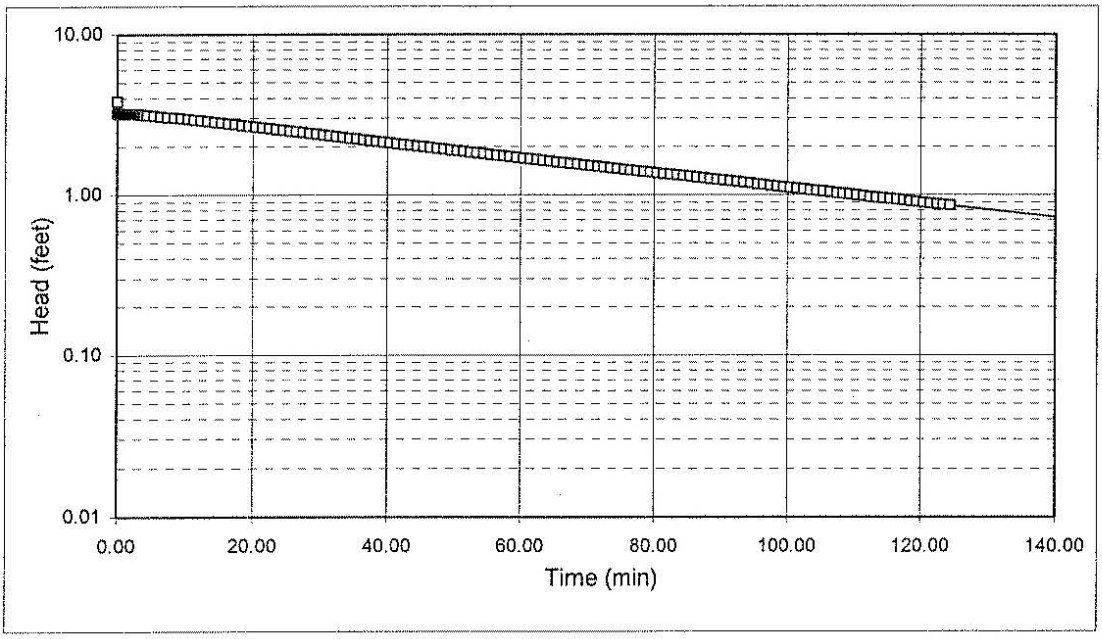
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.25
L_e =	14.5
$\ln(R_e/r_w)$	3.80
y_0 =	3.16
y_t =	0.72
t =	140.00

RESULTS

K=	4.86E-06	cm/sec
K=	1.38E-02	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/9/96

FALLING HEAD TEST PZ-114-AS (TEST 1)

WELL NO. PZ-114-AS (TEST 1)

DATE		
INITAL HEAD ON TRANSDUCER	10.02	FEET H_2O
INITIAL DEPTH TO WATER	12.07	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	10.25	INCHES
TOP OF OPEN INTERVAL	18.3	FEET (btoc)
BOTTOM OF OPEN INTERVAL	32.0	FEET (btoc)
SATURATED THICKNESS	40	FEET
WATER TABLE TO BOTTOM OF SCREEN	19.9	FEET
EQUIVALENT DIAMETER	5.86	INCHES
OPEN INTERVAL LENGTH	13.7	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	5.20	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	172	940	16	15.217	0.00	6.87	5.20	1.000
1995	172	940	18	11.364	0.03	10.73	1.34	0.259
1995	172	940	20	10.974	0.07	11.12	0.95	0.184
1995	172	940	22	10.832	0.10	11.26	0.81	0.156
1995	172	940	24	10.658	0.13	11.43	0.64	0.123
1995	172	940	26	10.519	0.17	11.57	0.50	0.096
1995	172	940	28	10.421	0.20	11.67	0.40	0.077
1995	172	940	30	10.343	0.23	11.75	0.32	0.062
1995	172	940	32	10.283	0.27	11.81	0.26	0.051
1995	172	940	34	10.235	0.30	11.86	0.22	0.041
1995	172	940	36	10.203	0.33	11.89	0.18	0.035
1995	172	940	38	10.173	0.37	11.92	0.15	0.029
1995	172	940	40	10.153	0.40	11.94	0.13	0.026
1995	172	940	42	10.128	0.43	11.96	0.11	0.021
1995	172	940	44	10.116	0.47	11.97	0.10	0.018
1995	172	940	46	10.102	0.50	11.99	0.08	0.016
1995	172	940	48	10.09	0.53	12.00	0.07	0.013
1995	172	940	50	10.087	0.57	12.00	0.07	0.013
1995	172	940	52	10.072	0.60	12.02	0.05	0.010
1995	172	940	54	10.066	0.63	12.02	0.05	0.009
1995	172	940	56	10.061	0.67	12.03	0.04	0.008
1995	172	940	58	10.058	0.70	12.03	0.04	0.007
1995	172	941	0	10.056	0.73	12.03	0.04	0.007
1995	172	941	2	10.058	0.77	12.03	0.04	0.007
1995	172	941	4	10.049	0.80	12.04	0.03	0.006

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-114-AS (TEST 1)

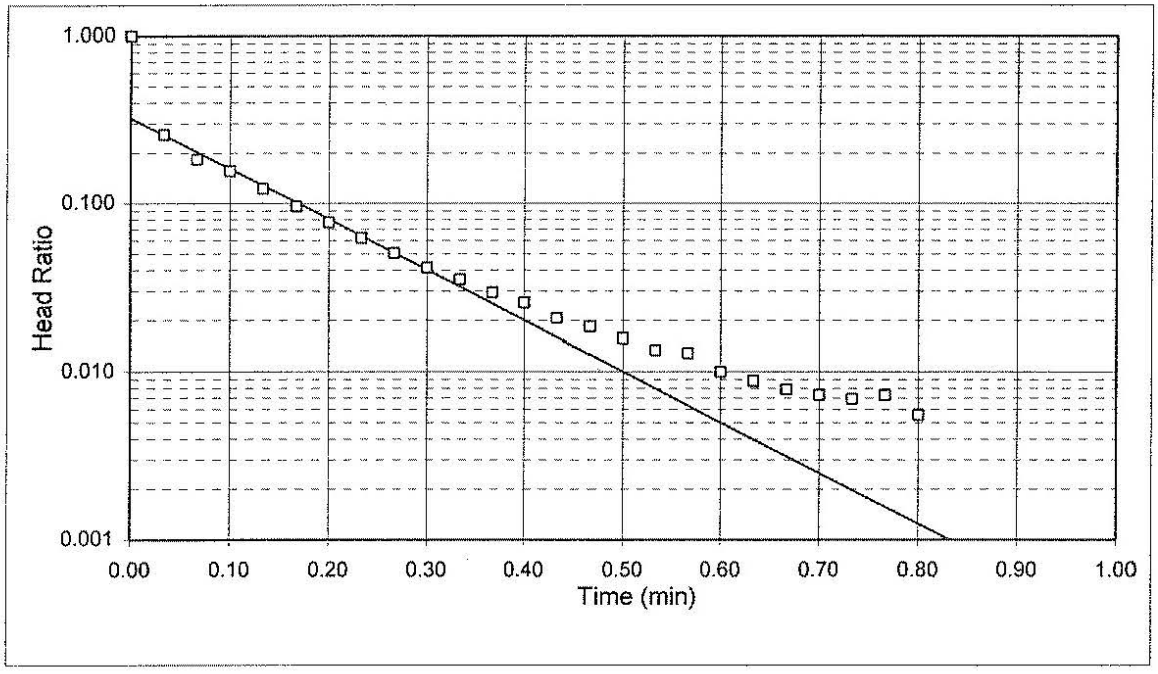
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.43
L_e =	13.7
t_1 (min) =	0
t_2 (min) =	0.83
h_1/h_0 =	0.32
h_2/h_0 =	0.00

RESULTS

K=	3.10E-03	cm/sec
K=	8.79E+00	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 06/21/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

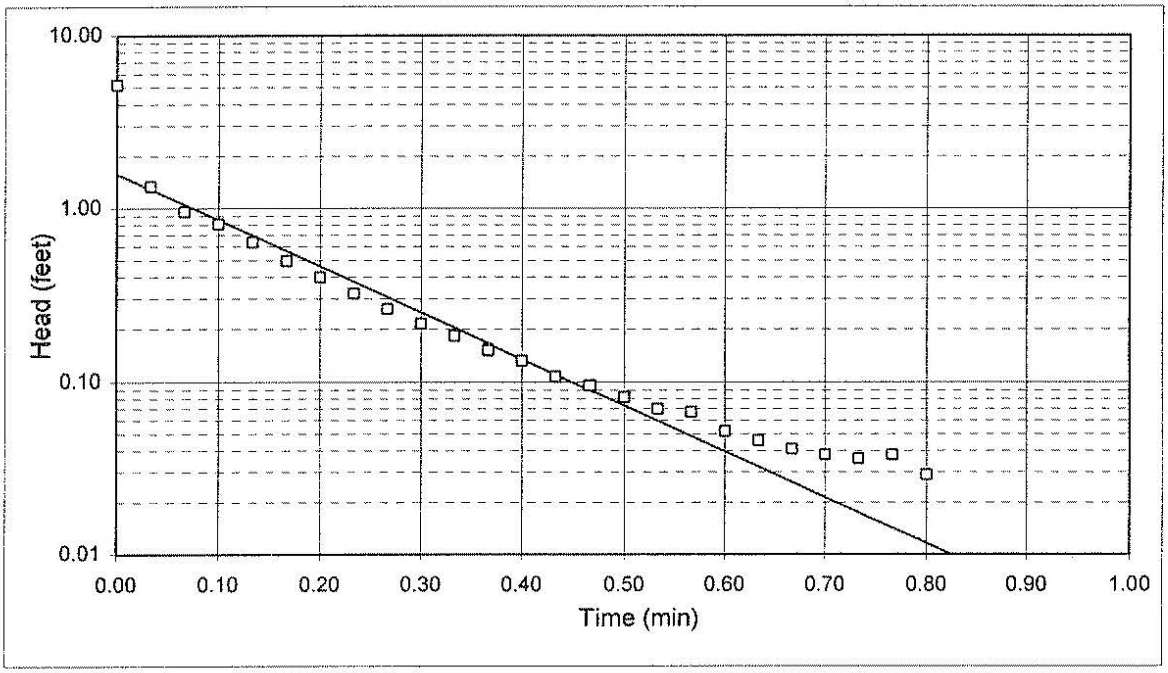
BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-114-AS (TEST 1)

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
r_w =	0.43			
L_e =	13.7	K=	1.69E-03	cm/sec
$\ln(R_e/r_w)$	2.14	K=	4.79E+00	ft/day
y_0 =	1.58			
y_t =	0.01			
t =	0.82			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 06/21/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

FALLING HEAD TEST PZ-114-AS (TEST 2)

WELL NO.	PZ-114-AS (TEST 2)	
DATE	6/21/95	
INITAL HEAD ON TRANSDUCER	10.02	FEET H_2O
INITIAL DEPTH TO WATER	12.07	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	10.25	INCHES
TOP OF OPEN INTERVAL	18.3	FEET (btoc)
BOTTOM OF OPEN INTERVAL	32.0	FEET (btoc)
SATURATED THICKNESS	40	FEET
WATER TABLE TO BOTTOM OF SCREEN	19.9	FEET
EQUIVALENT DIAMETER	5.86	INCHES
OPEN INTERVAL LENGTH	13.7	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	5.07	FEET
MAX. HEAD IN SCREEN?	N	

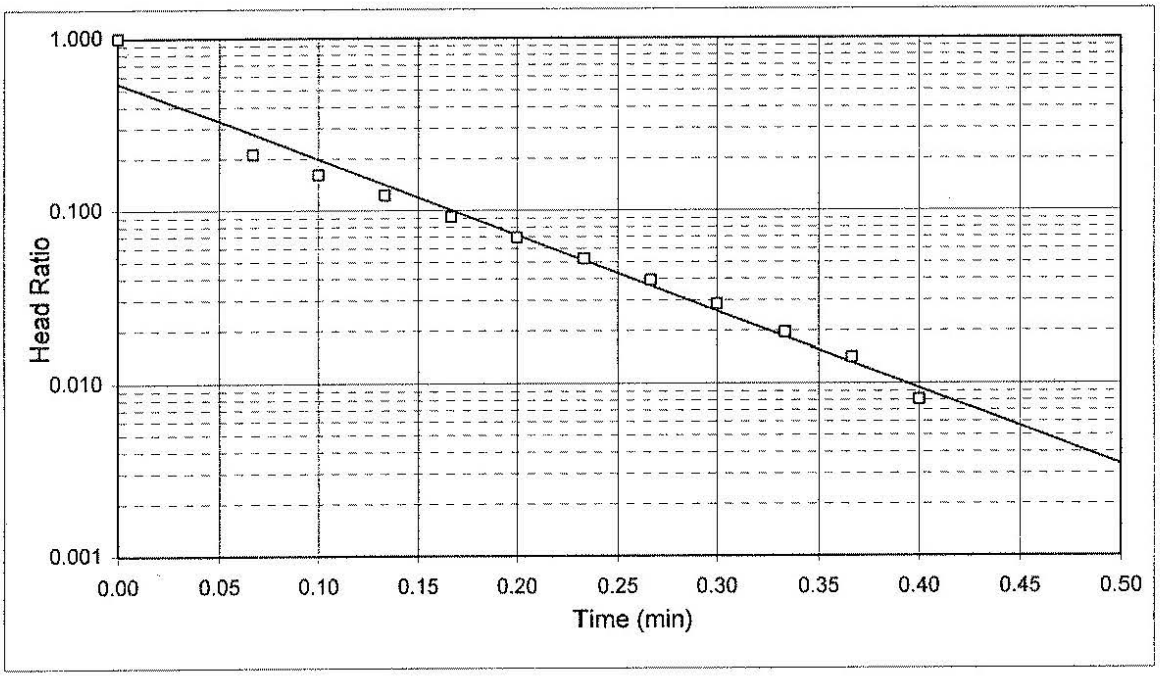
DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	172	944	8	15.094	0.00	7.00	5.07	1.000
1995	172	944	12	11.099	0.07	10.99	1.08	0.213
1995	172	944	14	10.84	0.10	11.25	0.82	0.162
1995	172	944	16	10.643	0.13	11.45	0.62	0.123
1995	172	944	18	10.486	0.17	11.60	0.47	0.092
1995	172	944	20	10.373	0.20	11.72	0.35	0.070
1995	172	944	22	10.286	0.23	11.80	0.27	0.052
1995	172	944	24	10.22	0.27	11.87	0.20	0.039
1995	172	944	26	10.165	0.30	11.93	0.15	0.029
1995	172	944	28	10.12	0.33	11.97	0.10	0.020
1995	172	944	30	10.092	0.37	12.00	0.07	0.014
1995	172	944	32	10.061	0.40	12.03	0.04	0.008

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-114-AS (TEST 2)

$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
R_e =	0.43			
L_e =	13.7	K=	4.54E-03	cm/sec
t_1 (min) =	0	K=	1.29E+01	ft/day
t_2 (min) =	0.50			
h_1/h_0 =	0.55			
h_2/h_0 =	0.00			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 06/21/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-114-AS (TEST 2)

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

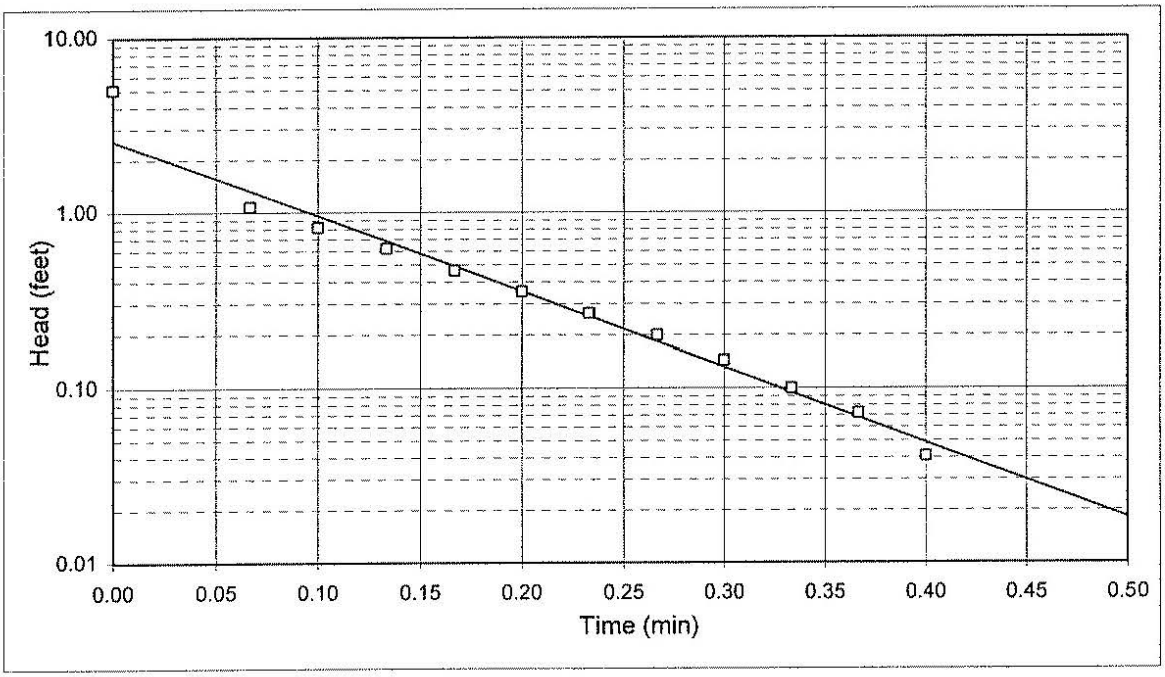
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.43
L_e =	13.7
$\ln(R_e/r_w)$	2.14
y_0 =	2.57
y_t =	0.02
t =	0.50

RESULTS

K=	2.72E-03	cm/sec
K=	7.72E+00	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 06/21/95

Analysis By: DSL
Checked By: CVK
Analysis Date: 10/11/95

FALLING HEAD TEST PZ-115-SS

WELL NO. PZ-115-SS

DATE	6/22/95	
INITAL HEAD ON TRANSDUCER	14.99	FEET H_2O
INITIAL DEPTH TO WATER	25.14	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	72.7	FEET (btoc)
BOTTOM OF OPEN INTERVAL	86.7	FEET (btoc)
SATURATED THICKNESS	170	FEET
WATER TABLE TO BOTTOM OF SCREEN	61.56	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	14	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.72	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	173	852	30	18.706	0.00	21.42	3.72	1.00
1995	173	852	40	18.191	0.17	21.94	3.20	0.86
1995	173	853	20	17.883	0.83	22.25	2.89	0.78
1995	173	853	30	17.836	1.00	22.29	2.85	0.77
1995	173	853	40	17.797	1.17	22.33	2.81	0.76
1995	173	853	50	17.759	1.33	22.37	2.77	0.75
1995	173	854	0	17.726	1.50	22.40	2.74	0.74
1995	173	854	10	17.689	1.67	22.44	2.70	0.73
1995	173	854	20	17.654	1.83	22.48	2.66	0.72
1995	173	854	30	17.623	2.00	22.51	2.63	0.71
1995	173	854	40	17.592	2.17	22.54	2.60	0.70
1995	173	854	50	17.562	2.33	22.57	2.57	0.69
1995	173	855	0	17.532	2.50	22.60	2.54	0.68
1995	173	855	10	17.499	2.67	22.63	2.51	0.68
1995	173	855	20	17.469	2.83	22.66	2.48	0.67
1995	173	855	30	17.442	3.00	22.69	2.45	0.66
1995	173	855	40	17.415	3.17	22.72	2.43	0.65
1995	173	855	50	17.388	3.33	22.74	2.40	0.65
1995	173	856	0	17.364	3.50	22.77	2.37	0.64
1995	173	856	10	17.336	3.67	22.79	2.35	0.63
1995	173	856	30	17.283	4.00	22.85	2.29	0.62
1995	173	857	0	17.21	4.50	22.92	2.22	0.60
1995	173	857	30	17.133	5.00	23.00	2.14	0.58
1995	173	858	0	17.068	5.50	23.06	2.08	0.56
1995	173	858	30	17.002	6.00	23.13	2.01	0.54
1995	173	859	0	16.942	6.50	23.19	1.95	0.53
1995	173	859	30	16.885	7.00	23.25	1.90	0.51

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	173	900	0	16.831	7.50	23.30	1.84	0.50
1995	173	900	30	16.778	8.00	23.35	1.79	0.48
1995	173	901	0	16.728	8.50	23.40	1.74	0.47
1995	173	901	30	16.68	9.00	23.45	1.69	0.45
1995	173	902	0	16.632	9.50	23.50	1.64	0.44
1995	173	902	30	16.589	10.00	23.54	1.60	0.43
1995	173	903	0	16.547	10.50	23.58	1.56	0.42
1995	173	903	30	16.507	11.00	23.62	1.52	0.41
1995	173	904	0	16.468	11.50	23.66	1.48	0.40
1995	173	905	0	16.392	12.50	23.74	1.40	0.38
1995	173	910	0	16.1	17.50	24.03	1.11	0.30
1995	173	915	0	15.903	22.50	24.23	0.91	0.25
1995	173	920	0	15.772	27.50	24.36	0.78	0.21
1995	173	925	0	15.683	32.50	24.45	0.69	0.19
1995	173	930	0	15.622	37.50	24.51	0.63	0.17
1995	173	935	0	15.582	42.50	24.55	0.59	0.16
1995	173	940	0	15.55	47.50	24.58	0.56	0.15
1995	173	945	0	15.523	52.50	24.61	0.53	0.14
1995	173	950	0	15.504	57.50	24.63	0.51	0.14
1995	173	955	0	15.491	62.50	24.64	0.50	0.13
1995	173	1000	0	15.475	67.50	24.66	0.48	0.13
1995	173	1005	0	15.463	72.50	24.67	0.47	0.13
1995	173	1010	0	15.452	77.50	24.68	0.46	0.12
1995	173	1015	0	15.441	82.50	24.69	0.45	0.12
1995	173	1020	0	15.433	87.50	24.70	0.44	0.12
1995	173	1025	0	15.422	92.50	24.71	0.43	0.12
1995	173	1030	0	15.412	97.50	24.72	0.42	0.11
1995	173	1035	0	15.407	102.50	24.72	0.42	0.11
1995	173	1040	0	15.399	107.50	24.73	0.41	0.11
1995	173	1045	0	15.392	112.50	24.74	0.40	0.11
1995	173	1050	0	15.386	117.50	24.74	0.40	0.11
1995	173	1055	0	15.379	122.50	24.75	0.39	0.10
1995	173	1100	0	15.37	127.50	24.76	0.38	0.10
1995	173	1105	0	15.366	132.50	24.76	0.38	0.10
1995	173	1110	0	15.359	137.50	24.77	0.37	0.10
1995	173	1115	0	15.354	142.50	24.78	0.36	0.10
1995	173	1120	0	15.346	147.50	24.78	0.36	0.10
1995	173	1125	0	15.339	152.50	24.79	0.35	0.09
1995	173	1130	0	15.336	157.50	24.79	0.35	0.09
1995	173	1135	0	15.331	162.50	24.80	0.34	0.09
1995	173	1140	0	15.327	167.50	24.80	0.34	0.09
1995	173	1145	0	15.32	172.50	24.81	0.33	0.09
1995	173	1150	0	15.314	177.50	24.82	0.32	0.09
1995	173	1155	0	15.31	182.50	24.82	0.32	0.09
1995	173	1200	0	15.305	187.50	24.83	0.31	0.08

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	173	1205	0	15.302	192.50	24.83	0.31	0.08
1995	173	1210	0	15.296	197.50	24.83	0.31	0.08
1995	173	1215	0	15.294	202.50	24.84	0.30	0.08
1995	173	1220	0	15.288	207.50	24.84	0.30	0.08
1995	173	1225	0	15.282	212.50	24.85	0.29	0.08
1995	173	1230	0	15.281	217.50	24.85	0.29	0.08
1995	173	1235	0	15.278	222.50	24.85	0.29	0.08
1995	173	1240	0	15.272	227.50	24.86	0.28	0.08
1995	173	1245	0	15.267	232.50	24.86	0.28	0.07

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-115-SS

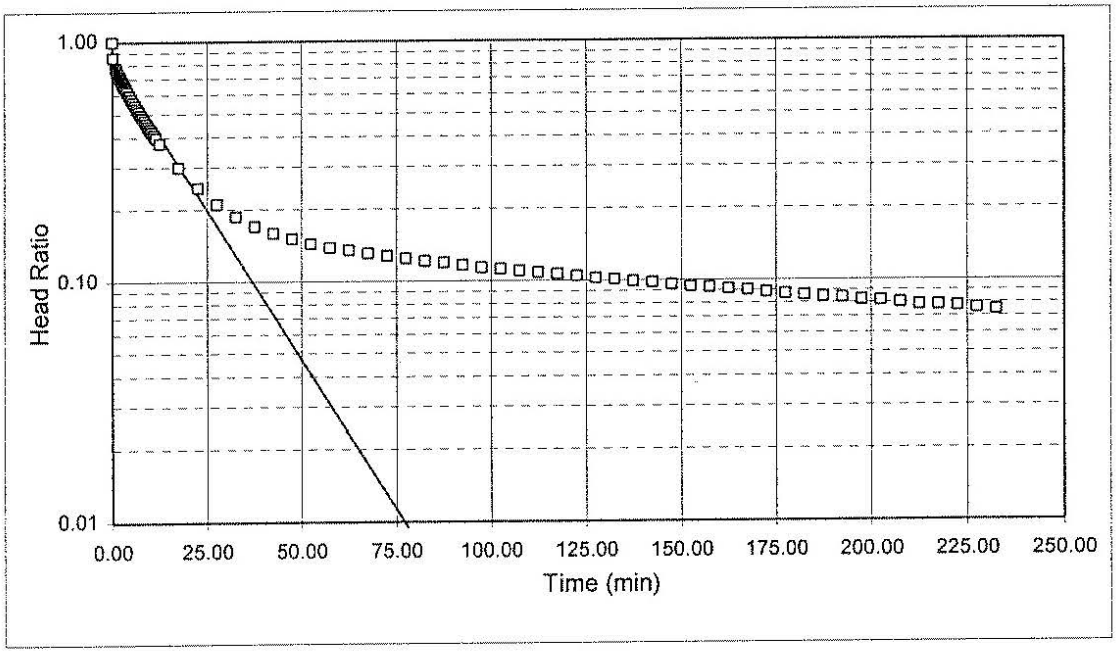
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	14
t_1 (min) =	1.17
t_2 (min) =	78.30
h_1/h_0 =	0.78
h_2/h_0 =	0.01

RESULTS

K=	2.91E-05	cm/sec
K=	8.24E-02	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 06/22/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/10/96

BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-115-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

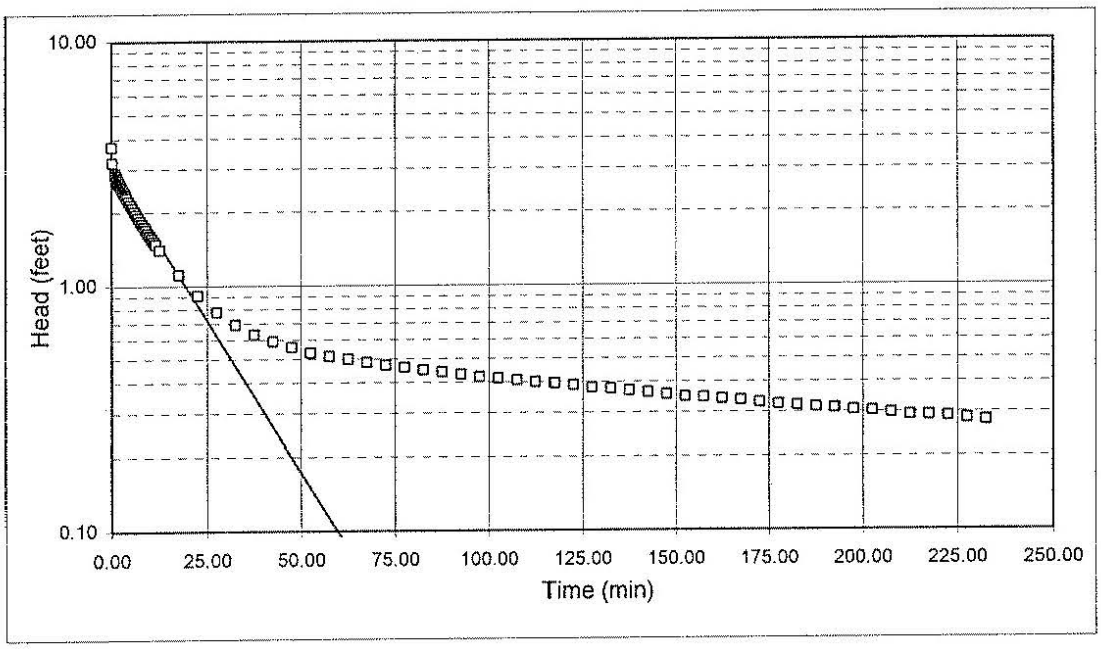
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.25
L_e =	14
$\ln(R_e/r_w)$	3.38
y_0 =	2.84
y_t =	0.01
t =	99.20

RESULTS

K=	2.40E-05 cm/sec
K=	6.81E-02 ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 06/22/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/10/96

RISING HEAD TEST PZ-116-SS

WELL NO. PZ-116-SS

DATE	7/24/95	
INITIAL DEPTH TO WATER	138.08	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	148.8	FEET (btoc)
BOTTOM OF OPEN INTERVAL	163.8	FEET (btoc)
SATURATED THICKNESS	80	FEET
WATER TABLE TO BOTTOM OF SCREEN	25.72	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	15	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.93	FEET
MAX. HEAD IN SCREEN?	N	

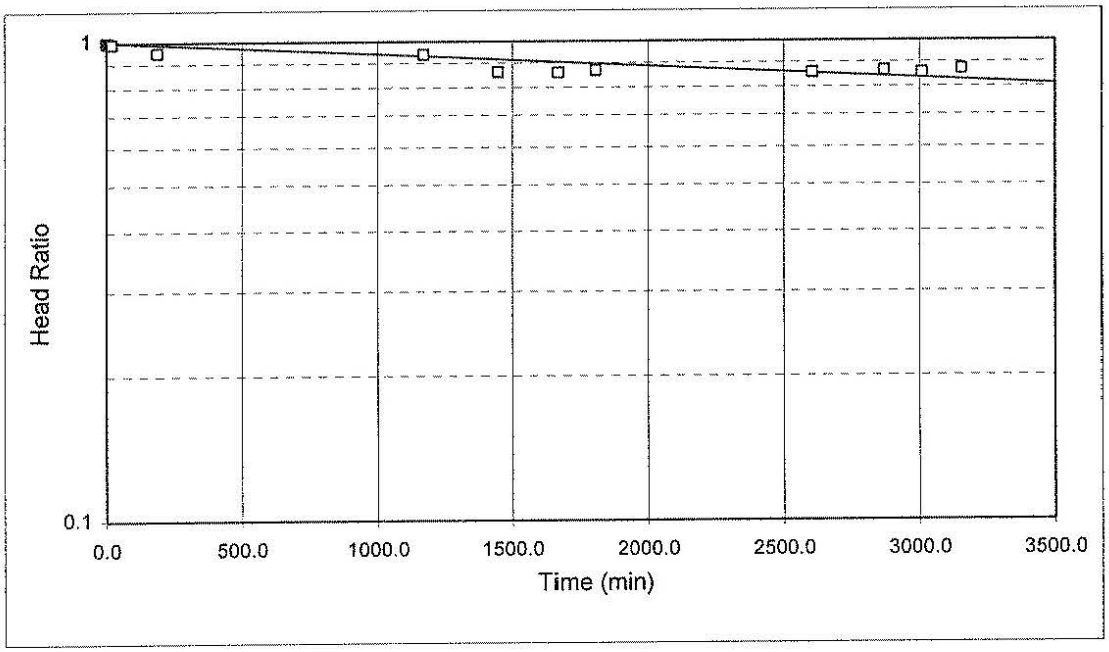
DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1132	30	142.01	0.0	3.93	1.00
1	1135	0	142	2.5	3.92	1.00
1	1140	0	141.99	7.5	3.91	0.99
1	1145	0	141.99	12.5	3.91	0.99
1	1152	30	141.98	20.0	3.90	0.99
1	1440	0	141.82	187.5	3.74	0.95
2	702	0	141.77	1169.5	3.69	0.94
2	1139	0	141.47	1446.5	3.39	0.86
2	1520	0	141.46	1667.5	3.38	0.86
2	1738	0	141.49	1805.5	3.41	0.87
3	1122	0	141.48	2869.5	3.40	0.87
3	1608	0	141.5	3155.5	3.42	0.87
3	658	0	141.45	2605.5	3.37	0.86
3	1342	0	141.44	3009.5	3.36	0.85

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-116-SS

$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where:
- r_c = casing radius (feet)
- R_e = filter pack radius (feet)
- L_e = length of screened interval (feet)
- t = time (seconds)
- h_t = head at time t (feet)

INPUT PARAMETERS		RESULTS	
r_c =	0.08		
R_e =	0.25		
L_e =	15	K=	2.90E-08 cm/sec
t_1 (min) =	0	K=	8.22E-05 ft/day
t_2 (min) =	3500		
h_1/h_0 =	1.00		
h_2/h_0 =	0.81		



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/24/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/9/96

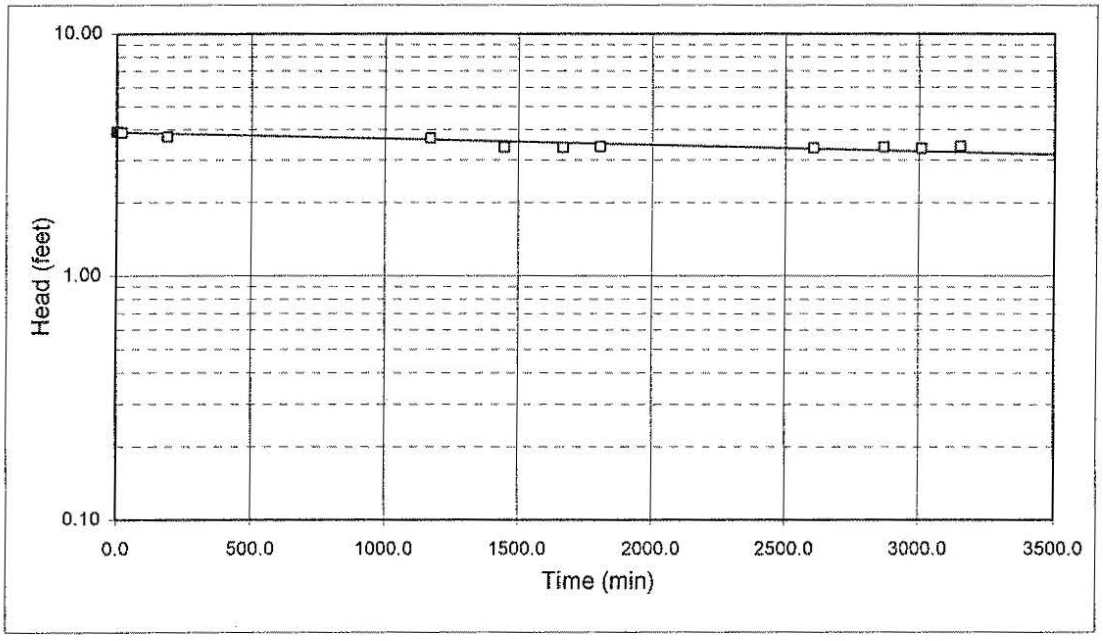
BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-116-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
r_w =	0.25			
L_e =	15	K=	1.73E-08	cm/sec
$\ln(R_e/r_w)$	2.95	K=	4.91E-05	ft/day
y_0 =	3.90			
y_t =	3.16			
t =	3500.0			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/24/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/9/96

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-200-SS

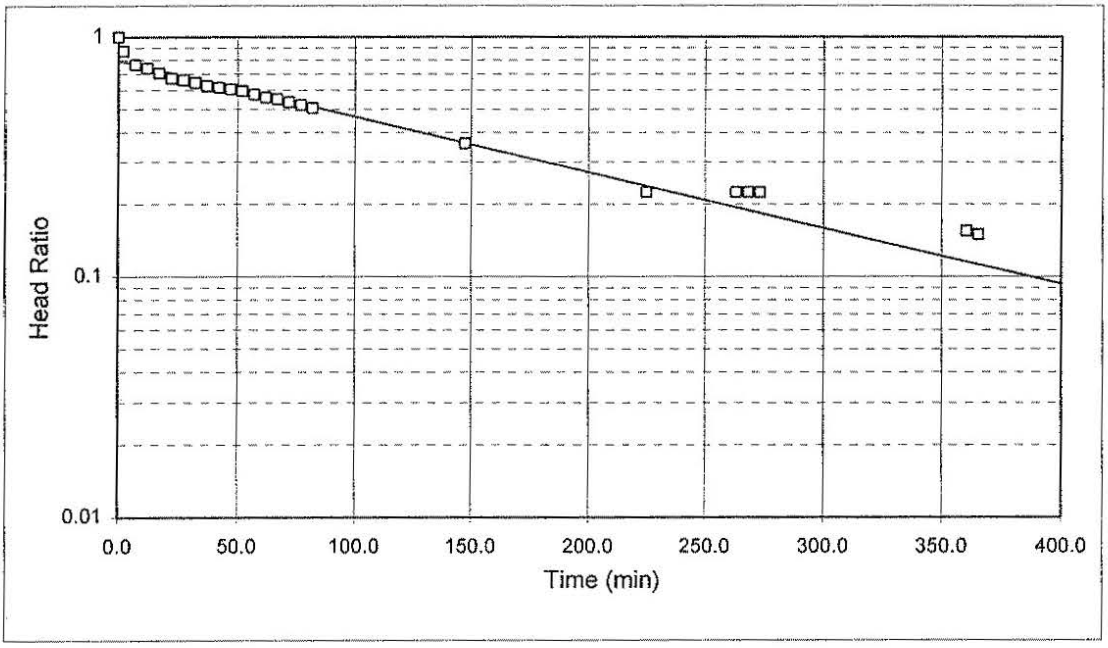
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	29.76
t_1 (min) =	0
t_2 (min) =	400
h_1/h_0 =	0.79
h_2/h_0 =	0.09

RESULTS

K=	1.52E-06	cm/sec
K=	4.30E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 06/20/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/10/96

RISING HEAD TEST PZ-201-SS

WELL NO. PZ-201-SS

DATE	7/17/95	
INITIAL DEPTH TO WATER	25.43	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	9.8	FEET (btoc)
BOTTOM OF OPEN INTERVAL	91.3	FEET (btoc)
SATURATED THICKNESS	220	FEET
WATER TABLE TO BOTTOM OF SCREEN	65.89	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	65.89	FEET
STATIC IN SCREEN?	Y	
MAX. HEAD CHANGE	1.40	FEET
MAX. HEAD IN SCREEN?	Y	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1115	0	26.83	0.0	1.40	1.00
1	1116	0	26.29	1.0	0.86	0.61
1	1116	30	26.18	1.5	0.75	0.54
1	1117	0	26.09	2.0	0.66	0.47
1	1117	30	26.01	2.5	0.58	0.41
1	1118	0	25.98	3.0	0.55	0.39
1	1119	30	25.91	4.5	0.48	0.34
1	1119	0	25.87	4.0	0.44	0.31
1	1120	30	25.82	5.5	0.39	0.28
1	1120	0	25.79	5.0	0.36	0.26
1	1121	30	25.75	6.5	0.32	0.23
1	1122	0	25.69	7.0	0.26	0.19
1	1122	30	25.67	7.5	0.24	0.17
1	1123	0	25.65	8.0	0.22	0.16
1	1123	30	25.63	8.5	0.20	0.14
1	1124	0	25.6	9.0	0.17	0.12
1	1124	30	25.59	9.5	0.16	0.11
1	1125	0	25.58	10.0	0.15	0.11
1	1125	30	25.56	10.5	0.13	0.09
1	1126	0	25.54	11.0	0.11	0.08
1	1126	30	25.51	11.5	0.08	0.06
1	1127	0	25.51	12.0	0.08	0.06

BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-201-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

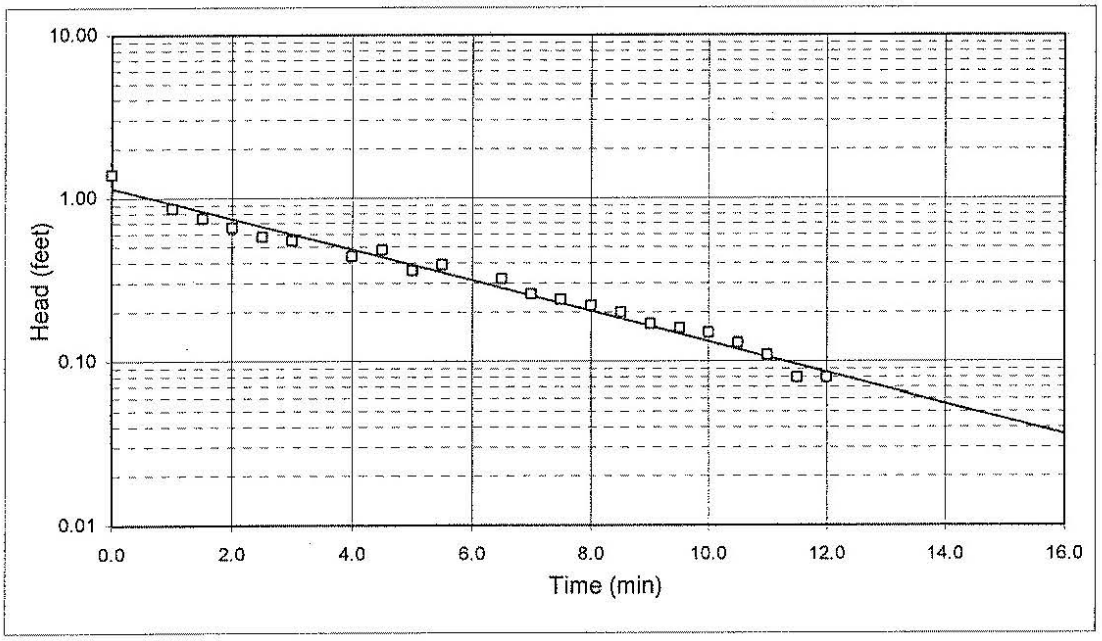
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.15
r_w =	0.25
L_e =	65.89
$\ln(R_e/r_w)$	3.88
y_0 =	1.15
y_t =	0.04
t =	16.0

RESULTS

K=	5.39E-05	cm/sec
K=	1.53E-01	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/17/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/10/96

FALLING HEAD TEST PZ-201A-SS

WELL NO. PZ-201A-SS

DATE	7/17/95	
INITIAL DEPTH TO WATER	65.46	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	76.9	FEET (btoc)
BOTTOM OF OPEN INTERVAL	91.8	FEET (btoc)
SATURATED THICKNESS	180	FEET
WATER TABLE TO BOTTOM OF SCREEN	26.34	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	14.89	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.42	FEET
MAX. HEAD IN SCREEN?	N	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1439	0	68.88	0.0	3.42	1.00
1	1440	0	68.87	1.0	3.41	1.00
1	1441	0	68.87	2.0	3.41	1.00
1	1446	0	68.8	7.0	3.34	0.98
1	1451	0	68.78	12.0	3.32	0.97
1	1456	0	68.77	17.0	3.31	0.97
1	1501	0	68.76	22.0	3.30	0.96
1	1506	0	68.75	27.0	3.29	0.96
1	1511	0	68.74	32.0	3.28	0.96
1	1516	0	68.72	37.0	3.26	0.95
1	1647	30	68.52	128.5	3.06	0.89
1	1816	0	68.62	217.0	3.16	0.92
2	654	0	68.11	975.0	2.65	0.77

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-201A-SS

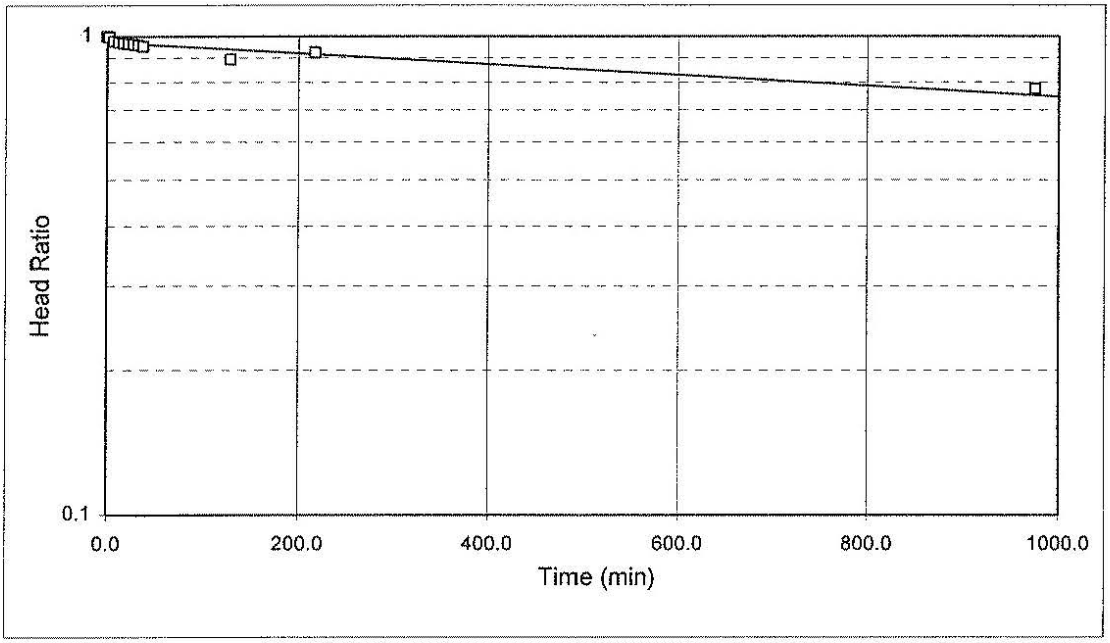
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	14.89
t_1 (min) =	0
t_2 (min) =	1000
h_1/h_0 =	0.97
h_2/h_0 =	0.75

RESULTS

K=	1.27E-07	cm/sec
K=	3.60E-04	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/17/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/9/96

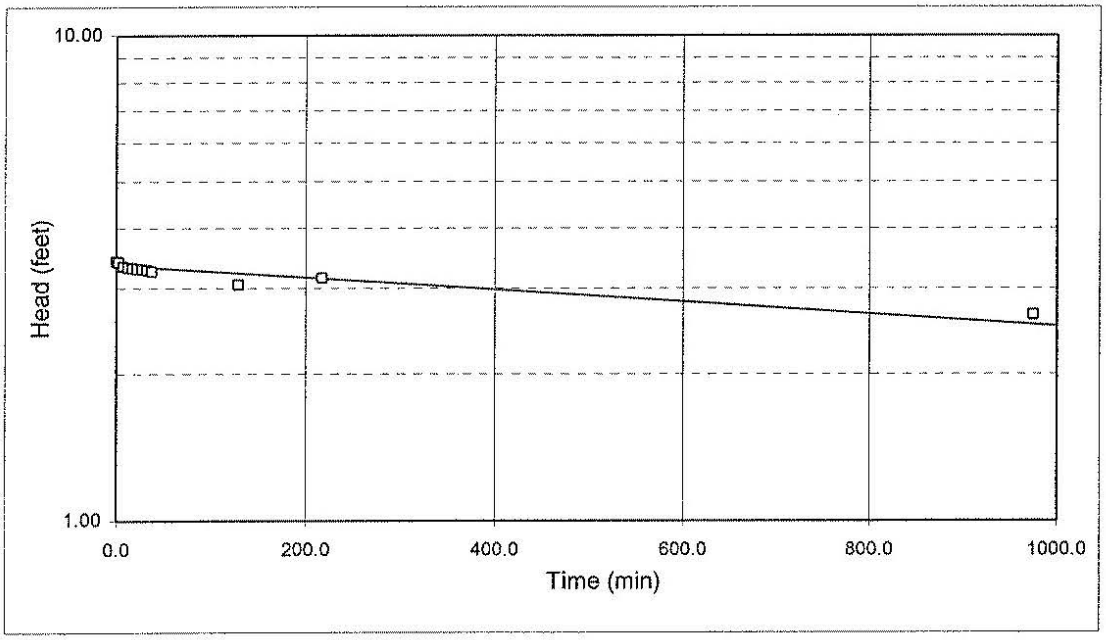
BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-201A-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
r_w =	0.25			
L_e =	14.89	K=	8.34E-08	cm/sec
$\ln(R_e/r_w)$	2.88	K=	2.36E-04	ft/day
y_0 =	3.35			
y_t =	2.51			
t =	1000.0			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/17/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/9/96

FALLING HEAD TEST PZ-202-SS

WELL NO. PZ-202-SS

DATE	7/19/95	
INITAL HEAD ON TRANSDUCER	14.968	FEET H_2O
INITIAL DEPTH TO WATER	36.3	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	40.2	FEET (btoc)
BOTTOM OF OPEN INTERVAL	92.2	FEET (btoc)
SATURATED THICKNESS	210	FEET
WATER TABLE TO BOTTOM OF SCREEN	55.9	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	52	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	0.53	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	200	1517	58	15.503	0.00	35.77	0.53	1.00
1995	200	1517	59	15.454	0.02	35.81	0.49	0.91
1995	200	1518	0	15.296	0.03	35.97	0.33	0.61
1995	200	1518	1	15.212	0.05	36.06	0.24	0.46
1995	200	1518	2	15.153	0.07	36.12	0.19	0.35
1995	200	1518	3	15.107	0.08	36.16	0.14	0.26
1995	200	1518	4	15.067	0.10	36.20	0.10	0.19
1995	200	1518	5	15.054	0.12	36.21	0.09	0.16
1995	200	1518	6	15.026	0.13	36.24	0.06	0.11
1995	200	1518	7	15.02	0.15	36.25	0.05	0.10
1995	200	1518	8	15.023	0.17	36.25	0.05	0.10
1995	200	1518	9	15.015	0.18	36.25	0.05	0.09
1995	200	1518	10	15.003	0.20	36.27	0.03	0.07
1995	200	1518	11	14.997	0.22	36.27	0.03	0.05
1995	200	1518	12	15.01	0.23	36.26	0.04	0.08
1995	200	1518	13	15.008	0.25	36.26	0.04	0.07
1995	200	1518	14	14.994	0.27	36.27	0.03	0.05
1995	200	1518	15	15.008	0.28	36.26	0.04	0.07
1995	200	1518	16	15.007	0.30	36.26	0.04	0.07
1995	200	1518	17	15.009	0.32	36.26	0.04	0.08
1995	200	1518	18	15.005	0.33	36.26	0.04	0.07
1995	200	1518	19	15.006	0.35	36.26	0.04	0.07
1995	200	1518	20	15.004	0.37	36.26	0.04	0.07
1995	200	1518	21	14.991	0.38	36.28	0.02	0.04
1995	200	1518	22	15.003	0.40	36.27	0.03	0.07
1995	200	1518	23	15.005	0.42	36.26	0.04	0.07
1995	200	1518	24	14.991	0.43	36.28	0.02	0.04

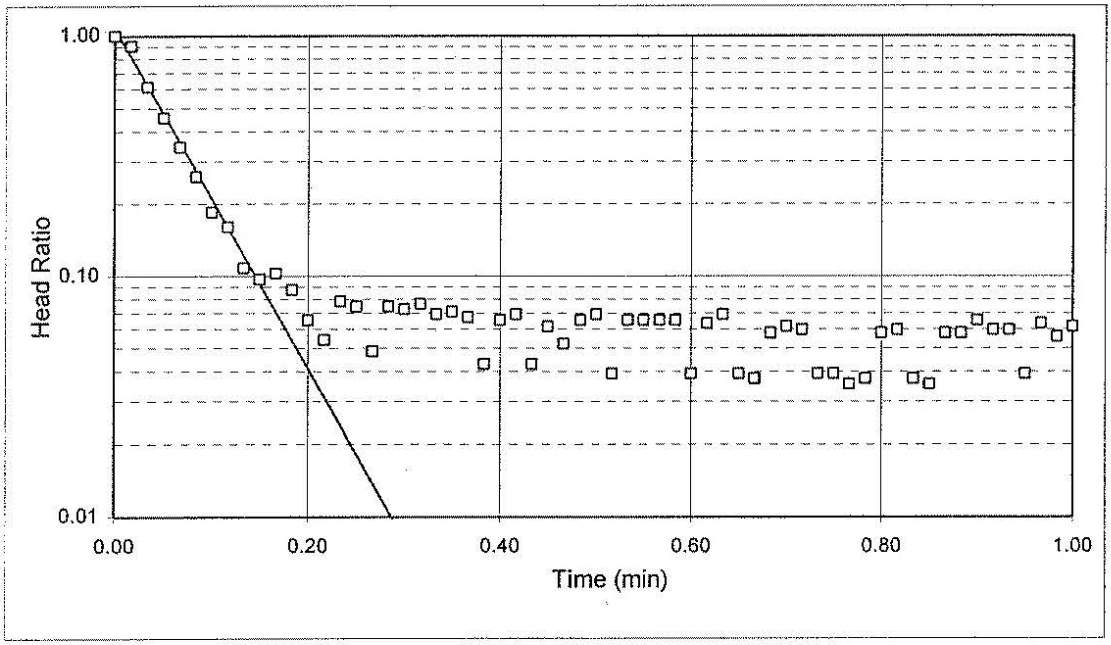
DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	200	1518	25	15.001	0.45	36.27	0.03	0.06
1995	200	1518	26	14.996	0.47	36.27	0.03	0.05
1995	200	1518	27	15.003	0.48	36.27	0.03	0.07
1995	200	1518	28	15.005	0.50	36.26	0.04	0.07
1995	200	1518	29	14.989	0.52	36.28	0.02	0.04
1995	200	1518	30	15.003	0.53	36.27	0.03	0.07
1995	200	1518	31	15.003	0.55	36.27	0.03	0.07
1995	200	1518	32	15.003	0.57	36.27	0.03	0.07
1995	200	1518	33	15.003	0.58	36.27	0.03	0.07
1995	200	1518	34	14.989	0.60	36.28	0.02	0.04
1995	200	1518	35	15.002	0.62	36.27	0.03	0.06
1995	200	1518	36	15.005	0.63	36.26	0.04	0.07
1995	200	1518	37	14.989	0.65	36.28	0.02	0.04
1995	200	1518	38	14.988	0.67	36.28	0.02	0.04
1995	200	1518	39	14.999	0.68	36.27	0.03	0.06
1995	200	1518	40	15.001	0.70	36.27	0.03	0.06
1995	200	1518	41	15	0.72	36.27	0.03	0.06
1995	200	1518	42	14.989	0.73	36.28	0.02	0.04
1995	200	1518	43	14.989	0.75	36.28	0.02	0.04
1995	200	1518	44	14.987	0.77	36.28	0.02	0.04
1995	200	1518	45	14.988	0.78	36.28	0.02	0.04
1995	200	1518	46	14.999	0.80	36.27	0.03	0.06
1995	200	1518	47	15	0.82	36.27	0.03	0.06
1995	200	1518	48	14.988	0.83	36.28	0.02	0.04
1995	200	1518	49	14.987	0.85	36.28	0.02	0.04
1995	200	1518	50	14.999	0.87	36.27	0.03	0.06
1995	200	1518	51	14.999	0.88	36.27	0.03	0.06
1995	200	1518	52	15.003	0.90	36.27	0.03	0.07
1995	200	1518	53	15	0.92	36.27	0.03	0.06
1995	200	1518	54	15	0.93	36.27	0.03	0.06
1995	200	1518	55	14.989	0.95	36.28	0.02	0.04
1995	200	1518	56	15.002	0.97	36.27	0.03	0.06
1995	200	1518	57	14.998	0.98	36.27	0.03	0.06
1995	200	1518	58	15.001	1.00	36.27	0.03	0.06

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-202-SS

$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
R_e =	0.25			
L_e =	52	K=	2.95E-03	cm/sec
t_1 (min) =	0	K=	8.37E+00	ft/day
t_2 (min) =	0.29			
h_1/h_0 =	1.07			
h_2/h_0 =	0.01			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/19/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/9/96

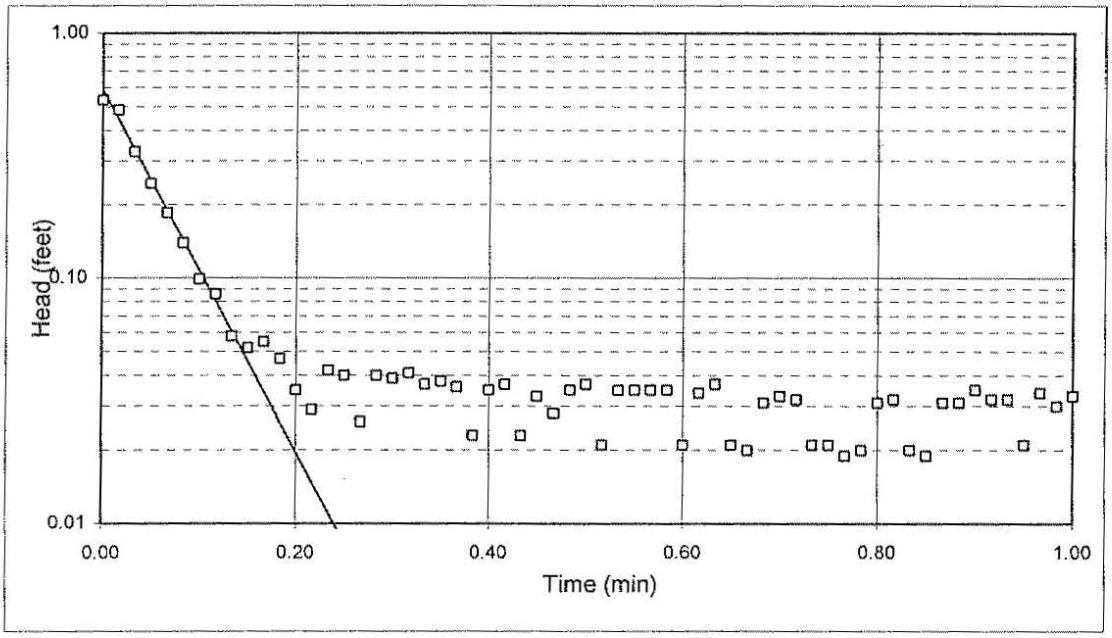
BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-202-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS	
r_c =	0.08		
r_w =	0.25		
L_e =	52	K=	2.51E-03 cm/sec
$\ln(R_e/r_w)$	4.35	K=	7.11E+00 ft/day
y_0 =	0.59		
y_t =	0.01		
t =	0.25		



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/19/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/9/96

RISING HEAD TEST PZ-204-SS

WELL NO. PZ-204-SS

DATE	6/23/95	
INITIAL DEPTH TO WATER	27.35	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	11.1	FEET (btoc)
BOTTOM OF OPEN INTERVAL	92.9	FEET (btoc)
SATURATED THICKNESS	170	FEET
WATER TABLE TO BOTTOM OF SCREEN	65.55	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	65.55	FEET
STATIC IN SCREEN?	Y	
MAX. HEAD CHANGE	1.04	FEET
MAX. HEAD IN SCREEN?	Y	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	758	30	28.39	0.0	1.04	1.00
1	759	30	28.38	1.0	1.03	0.99
1	800	30	28.37	2.0	1.02	0.98
1	801	30	28.37	3.0	1.02	0.98
1	806	30	28.29	8.0	0.94	0.90
1	811	30	28.21	13.0	0.86	0.83
1	816	30	28.15	18.0	0.80	0.77
1	821	30	28.07	23.0	0.72	0.69
1	826	30	28.05	28.0	0.70	0.67
1	831	30	28.01	33.0	0.66	0.63
1	836	30	27.99	38.0	0.64	0.62
1	841	30	27.95	43.0	0.60	0.58
1	846	30	27.89	48.0	0.54	0.52
1	851	30	27.88	53.0	0.53	0.51
1	856	30	27.85	58.0	0.50	0.48
1	901	30	27.83	63.0	0.48	0.46
1	906	30	27.8	68.0	0.45	0.43
1	911	30	27.78	73.0	0.43	0.41
1	916	30	27.77	78.0	0.42	0.40
1	921	30	27.75	83.0	0.40	0.38
1	926	30	27.73	88.0	0.38	0.37
1	931	30	27.72	93.0	0.37	0.36
1	936	30	27.7	98.0	0.35	0.34
1	941	30	27.68	103.0	0.33	0.32
1	946	30	27.66	108.0	0.31	0.30
1	951	30	27.63	113.0	0.28	0.27
1	956	30	27.61	118.0	0.26	0.25
1	1001	30	27.58	123.0	0.23	0.22
1	1006	30	27.58	128.0	0.23	0.22
1	1011	30	27.58	133.0	0.23	0.22
1	1016	30	27.57	138.0	0.22	0.21

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-204-SS

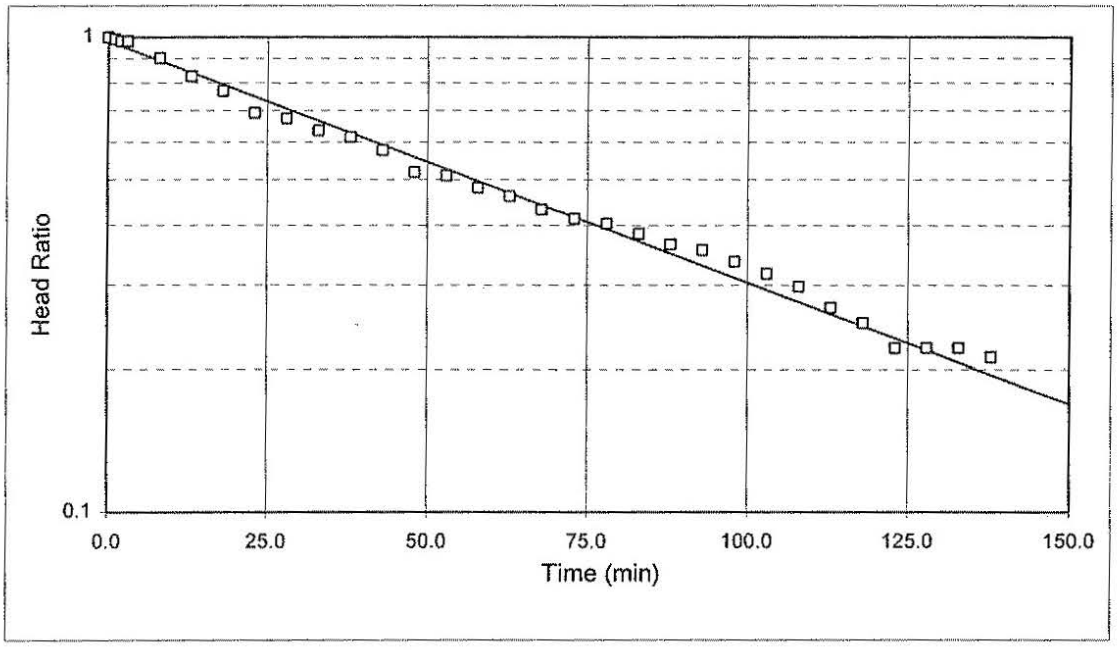
$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where:
- r_c = casing radius (feet)
- R_e = filter pack radius (feet)
- L_e = length of screened interval (feet)
- t = time (seconds)
- h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	65.55
t_1 (min) =	0
t_2 (min) =	150
h_1/h_0 =	0.98
h_2/h_0 =	0.17

RESULTS

K=	1.76E-06	cm/sec
K=	4.98E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 06/23/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/9/96

RISING HEAD TEST PZ-204A-SS

WELL NO. PZ-204A-SS

DATE	7/19/95	
INITIAL DEPTH TO WATER	67.12	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	76.0	FEET (btoc)
BOTTOM OF OPEN INTERVAL	91.5	FEET (btoc)
SATURATED THICKNESS	140	FEET
WATER TABLE TO BOTTOM OF SCREEN	24.38	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	15.5	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.61	FEET
MAX. HEAD IN SCREEN?	N	

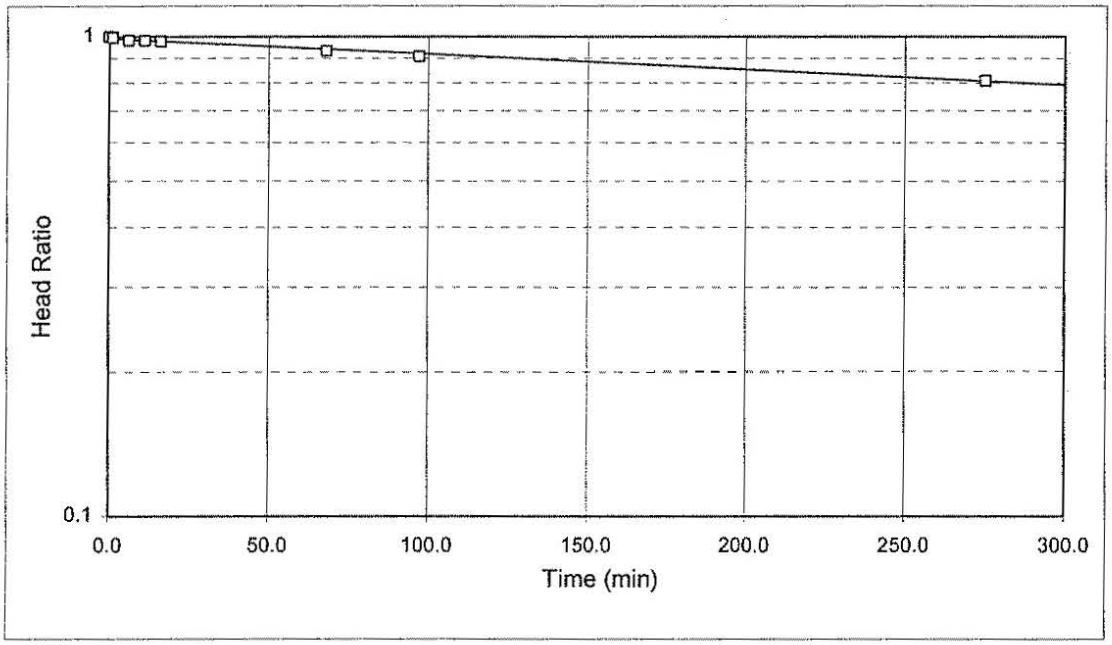
DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1156	0	70.73	0.0	3.61	1.00
1	1157	0	70.72	1.0	3.60	1.00
1	1202	0	70.67	6.0	3.55	0.98
1	1207	0	70.66	11.0	3.54	0.98
1	1212	0	70.65	16.0	3.53	0.98
1	1304	0	70.49	68.0	3.37	0.93
1	1333	0	70.4	97.0	3.28	0.91
1	1631	0	70.04	275.0	2.92	0.81

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-204A-SS

$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
h_t = head at time t (feet)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
R_e =	0.25			
L_e =	15.5	K=	3.48E-07	cm/sec
t_1 (min) =	0	K=	9.87E-04	ft/day
t_2 (min) =	300			
h_1/h_0 =	0.99			
h_2/h_0 =	0.79			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/19/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/9/96

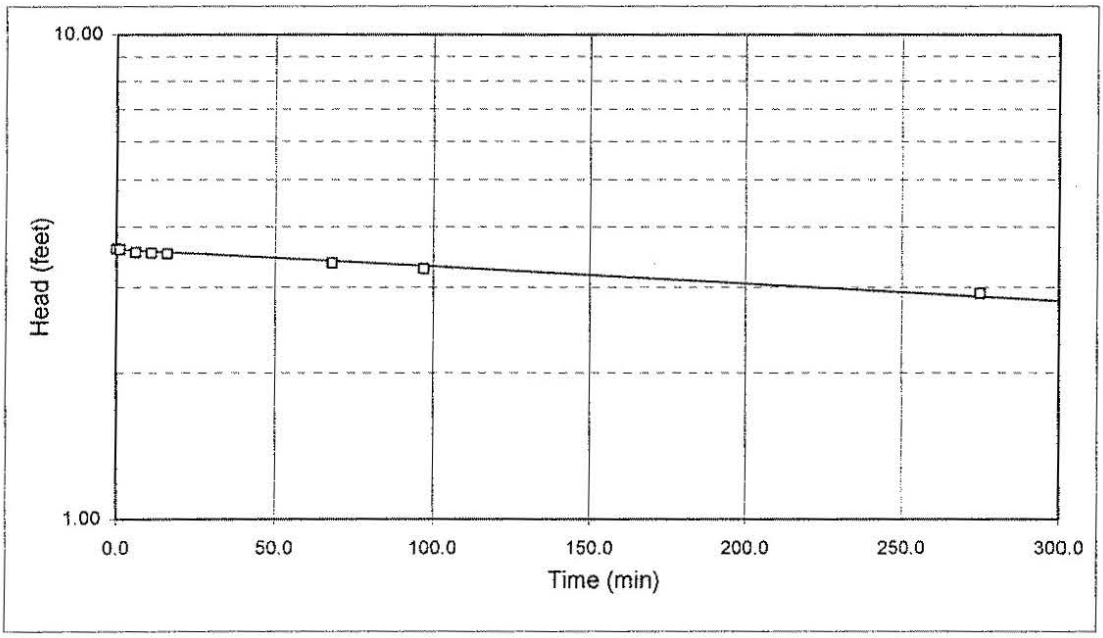
BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-204A-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
r_w =	0.25			
L_e =	15.5	K=	2.26E-07	cm/sec
$\ln(R_e/r_w)$	2.88	K=	6.42E-04	ft/day
y_0 =	3.60			
y_t =	2.82			
t =	300.0			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/19/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/9/96

FALLING HEAD TEST PZ-205-AS

WELL NO. PZ-205-AS

DATE	7/25/95	
INITAL HEAD ON TRANSDUCER	14.92	FEET H_2O
INITIAL DEPTH TO WATER	26.71	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	36.2	FEET (btoc)
BOTTOM OF OPEN INTERVAL	50.7	FEET (btoc)
SATURATED THICKNESS	30	FEET
WATER TABLE TO BOTTOM OF SCREEN	23.99	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	14.5	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	2.80	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	206	1600	4	17.718	0.00	23.91	2.80	1.00
1995	206	1600	6	17.177	0.03	24.45	2.26	0.81
1995	206	1600	7	17.148	0.05	24.48	2.23	0.80
1995	206	1600	8	17.102	0.07	24.53	2.18	0.78
1995	206	1600	9	17.052	0.08	24.58	2.13	0.76
1995	206	1600	10	17.005	0.10	24.63	2.09	0.75
1995	206	1600	11	16.961	0.12	24.67	2.04	0.73
1995	206	1600	12	16.917	0.13	24.71	2.00	0.71
1995	206	1600	13	16.874	0.15	24.76	1.95	0.70
1995	206	1600	14	16.83	0.17	24.80	1.91	0.68
1995	206	1600	15	16.791	0.18	24.84	1.87	0.67
1995	206	1600	16	16.755	0.20	24.88	1.84	0.66
1995	206	1600	17	16.717	0.22	24.91	1.80	0.64
1995	206	1600	18	16.677	0.23	24.95	1.76	0.63
1995	206	1600	19	16.643	0.25	24.99	1.72	0.62
1995	206	1600	20	16.606	0.27	25.02	1.69	0.60
1995	206	1600	21	16.57	0.28	25.06	1.65	0.59
1995	206	1600	22	16.537	0.30	25.09	1.62	0.58
1995	206	1600	23	16.501	0.32	25.13	1.58	0.57
1995	206	1600	24	16.471	0.33	25.16	1.55	0.55
1995	206	1600	25	16.434	0.35	25.20	1.51	0.54
1995	206	1600	26	16.406	0.37	25.22	1.49	0.53
1995	206	1600	27	16.376	0.38	25.25	1.46	0.52
1995	206	1600	28	16.346	0.40	25.28	1.43	0.51
1995	206	1600	29	16.318	0.42	25.31	1.40	0.50
1995	206	1600	30	16.289	0.43	25.34	1.37	0.49
1995	206	1600	31	16.259	0.45	25.37	1.34	0.48

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	206	1600	32	16.233	0.47	25.40	1.31	0.47
1995	206	1600	33	16.202	0.48	25.43	1.28	0.46
1995	206	1600	34	16.18	0.50	25.45	1.26	0.45
1995	206	1600	35	16.152	0.52	25.48	1.23	0.44
1995	206	1600	36	16.128	0.53	25.50	1.21	0.43
1995	206	1600	37	16.101	0.55	25.53	1.18	0.42
1995	206	1600	38	16.079	0.57	25.55	1.16	0.41
1995	206	1600	39	16.053	0.58	25.58	1.13	0.40
1995	206	1600	40	16.03	0.60	25.60	1.11	0.40
1995	206	1600	41	16.01	0.62	25.62	1.09	0.39
1995	206	1600	42	15.986	0.63	25.64	1.07	0.38
1995	206	1600	43	15.965	0.65	25.67	1.05	0.37
1995	206	1600	44	15.944	0.67	25.69	1.02	0.37
1995	206	1600	45	15.921	0.68	25.71	1.00	0.36
1995	206	1600	46	15.903	0.70	25.73	0.98	0.35
1995	206	1600	47	15.88	0.72	25.75	0.96	0.34
1995	206	1600	48	15.863	0.73	25.77	0.94	0.34
1995	206	1600	49	15.843	0.75	25.79	0.92	0.33
1995	206	1600	50	15.824	0.77	25.81	0.90	0.32
1995	206	1600	51	15.806	0.78	25.82	0.89	0.32
1995	206	1600	52	15.787	0.80	25.84	0.87	0.31
1995	206	1600	53	15.77	0.82	25.86	0.85	0.30
1995	206	1600	54	15.753	0.83	25.88	0.83	0.30
1995	206	1600	55	15.735	0.85	25.90	0.81	0.29
1995	206	1600	56	15.718	0.87	25.91	0.80	0.29
1995	206	1600	57	15.701	0.88	25.93	0.78	0.28
1995	206	1600	58	15.684	0.90	25.95	0.76	0.27
1995	206	1600	59	15.668	0.92	25.96	0.75	0.27
1995	206	1601	0	15.652	0.93	25.98	0.73	0.26
1995	206	1601	1	15.638	0.95	25.99	0.72	0.26
1995	206	1601	2	15.621	0.97	26.01	0.70	0.25
1995	206	1601	3	15.606	0.98	26.02	0.69	0.25
1995	206	1601	4	15.592	1.00	26.04	0.67	0.24
1995	206	1601	5	15.577	1.02	26.05	0.66	0.23
1995	206	1601	6	15.562	1.03	26.07	0.64	0.23
1995	206	1601	7	15.551	1.05	26.08	0.63	0.23
1995	206	1601	8	15.539	1.07	26.09	0.62	0.22
1995	206	1601	9	15.524	1.08	26.11	0.60	0.22
1995	206	1601	10	15.511	1.10	26.12	0.59	0.21
1995	206	1601	11	15.501	1.12	26.13	0.58	0.21
1995	206	1601	12	15.488	1.13	26.14	0.57	0.20
1995	206	1601	13	15.475	1.15	26.16	0.56	0.20
1995	206	1601	14	15.464	1.17	26.17	0.54	0.19
1995	206	1601	15	15.452	1.18	26.18	0.53	0.19
1995	206	1601	16	15.441	1.20	26.19	0.52	0.19

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	206	1601	17	15.431	1.22	26.20	0.51	0.18
1995	206	1601	18	15.417	1.23	26.21	0.50	0.18
1995	206	1601	19	15.41	1.25	26.22	0.49	0.18
1995	206	1601	20	15.398	1.27	26.23	0.48	0.17
1995	206	1601	21	15.386	1.28	26.24	0.47	0.17
1995	206	1601	22	15.377	1.30	26.25	0.46	0.16
1995	206	1601	23	15.364	1.32	26.27	0.44	0.16
1995	206	1601	24	15.356	1.33	26.27	0.44	0.16
1995	206	1601	25	15.347	1.35	26.28	0.43	0.15
1995	206	1601	26	15.34	1.37	26.29	0.42	0.15
1995	206	1601	27	15.33	1.38	26.30	0.41	0.15
1995	206	1601	28	15.32	1.40	26.31	0.40	0.14
1995	206	1601	29	15.311	1.42	26.32	0.39	0.14
1995	206	1601	30	15.302	1.43	26.33	0.38	0.14
1995	206	1601	31	15.296	1.45	26.33	0.38	0.13
1995	206	1601	32	15.287	1.47	26.34	0.37	0.13
1995	206	1601	33	15.278	1.48	26.35	0.36	0.13
1995	206	1601	34	15.268	1.50	26.36	0.35	0.12
1995	206	1601	35	15.26	1.52	26.37	0.34	0.12
1995	206	1601	36	15.253	1.53	26.38	0.33	0.12
1995	206	1601	37	15.246	1.55	26.38	0.33	0.12
1995	206	1601	38	15.24	1.57	26.39	0.32	0.11
1995	206	1601	39	15.232	1.58	26.40	0.31	0.11
1995	206	1601	40	15.226	1.60	26.40	0.31	0.11
1995	206	1601	41	15.217	1.62	26.41	0.30	0.11
1995	206	1601	42	15.21	1.63	26.42	0.29	0.10
1995	206	1601	43	15.204	1.65	26.43	0.28	0.10
1995	206	1601	44	15.197	1.67	26.43	0.28	0.10
1995	206	1601	45	15.189	1.68	26.44	0.27	0.10
1995	206	1601	46	15.183	1.70	26.45	0.26	0.09
1995	206	1601	47	15.18	1.72	26.45	0.26	0.09
1995	206	1601	48	15.171	1.73	26.46	0.25	0.09
1995	206	1601	49	15.169	1.75	26.46	0.25	0.09
1995	206	1601	50	15.16	1.77	26.47	0.24	0.09
1995	206	1601	51	15.152	1.78	26.48	0.23	0.08
1995	206	1601	52	15.151	1.80	26.48	0.23	0.08
1995	206	1601	53	15.145	1.82	26.49	0.23	0.08
1995	206	1601	54	15.14	1.83	26.49	0.22	0.08
1995	206	1601	55	15.133	1.85	26.50	0.21	0.08
1995	206	1601	56	15.128	1.87	26.50	0.21	0.07
1995	206	1601	57	15.125	1.88	26.51	0.20	0.07
1995	206	1601	58	15.12	1.90	26.51	0.20	0.07
1995	206	1601	59	15.113	1.92	26.52	0.19	0.07
1995	206	1602	0	15.108	1.93	26.52	0.19	0.07
1995	206	1602	1	15.105	1.95	26.53	0.19	0.07

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	206	1602	2	15.102	1.97	26.53	0.18	0.07
1995	206	1602	3	15.097	1.98	26.53	0.18	0.06
1995	206	1602	4	15.092	2.00	26.54	0.17	0.06
1995	206	1602	5	15.086	2.02	26.54	0.17	0.06
1995	206	1602	6	15.082	2.03	26.55	0.16	0.06
1995	206	1602	7	15.076	2.05	26.55	0.16	0.06
1995	206	1602	8	15.075	2.07	26.56	0.16	0.06
1995	206	1602	9	15.07	2.08	26.56	0.15	0.05
1995	206	1602	10	15.067	2.10	26.56	0.15	0.05
1995	206	1602	11	15.063	2.12	26.57	0.14	0.05
1995	206	1602	12	15.059	2.13	26.57	0.14	0.05
1995	206	1602	13	15.054	2.15	26.58	0.13	0.05
1995	206	1602	14	15.052	2.17	26.58	0.13	0.05
1995	206	1602	15	15.048	2.18	26.58	0.13	0.05
1995	206	1602	16	15.045	2.20	26.59	0.13	0.04
1995	206	1602	17	15.042	2.22	26.59	0.12	0.04
1995	206	1602	18	15.04	2.23	26.59	0.12	0.04
1995	206	1602	19	15.035	2.25	26.60	0.12	0.04
1995	206	1602	20	15.032	2.27	26.60	0.11	0.04
1995	206	1602	21	15.029	2.28	26.60	0.11	0.04
1995	206	1602	22	15.025	2.30	26.61	0.11	0.04
1995	206	1602	23	15.02	2.32	26.61	0.10	0.04
1995	206	1602	24	15.018	2.33	26.61	0.10	0.04
1995	206	1602	25	15.017	2.35	26.61	0.10	0.03
1995	206	1602	26	15.013	2.37	26.62	0.09	0.03
1995	206	1602	27	15.012	2.38	26.62	0.09	0.03
1995	206	1602	28	15.009	2.40	26.62	0.09	0.03
1995	206	1602	29	15.007	2.42	26.62	0.09	0.03
1995	206	1602	30	15.004	2.43	26.63	0.08	0.03
1995	206	1602	31	14.998	2.45	26.63	0.08	0.03
1995	206	1602	32	14.995	2.47	26.64	0.07	0.03
1995	206	1602	33	14.993	2.48	26.64	0.07	0.03
1995	206	1602	34	14.995	2.50	26.64	0.07	0.03
1995	206	1602	35	14.992	2.52	26.64	0.07	0.03
1995	206	1602	36	14.988	2.53	26.64	0.07	0.02
1995	206	1602	37	14.985	2.55	26.65	0.06	0.02
1995	206	1602	38	14.984	2.57	26.65	0.06	0.02
1995	206	1602	39	14.982	2.58	26.65	0.06	0.02
1995	206	1602	40	14.981	2.60	26.65	0.06	0.02
1995	206	1602	41	14.979	2.62	26.65	0.06	0.02
1995	206	1602	42	14.972	2.63	26.66	0.05	0.02
1995	206	1602	43	14.974	2.65	26.66	0.05	0.02
1995	206	1602	44	14.971	2.67	26.66	0.05	0.02
1995	206	1602	45	14.969	2.68	26.66	0.05	0.02
1995	206	1602	46	14.968	2.70	26.66	0.05	0.02

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	206	1602	47	14.966	2.72	26.66	0.05	0.02
1995	206	1602	48	14.965	2.73	26.67	0.05	0.02
1995	206	1602	49	14.962	2.75	26.67	0.04	0.02
1995	206	1602	50	14.96	2.77	26.67	0.04	0.01
1995	206	1602	51	14.957	2.78	26.67	0.04	0.01
1995	206	1602	52	14.954	2.80	26.68	0.03	0.01
1995	206	1602	53	14.956	2.82	26.67	0.04	0.01
1995	206	1602	54	14.951	2.83	26.68	0.03	0.01
1995	206	1602	55	14.951	2.85	26.68	0.03	0.01
1995	206	1602	56	14.953	2.87	26.68	0.03	0.01
1995	206	1602	57	14.95	2.88	26.68	0.03	0.01
1995	206	1602	58	14.945	2.90	26.69	0.02	0.01
1995	206	1602	59	14.943	2.92	26.69	0.02	0.01
1995	206	1603	0	14.943	2.93	26.69	0.02	0.01
1995	206	1603	1	14.945	2.95	26.69	0.02	0.01
1995	206	1603	2	14.942	2.97	26.69	0.02	0.01
1995	206	1603	3	14.94	2.98	26.69	0.02	0.01
1995	206	1603	4	14.939	3.00	26.69	0.02	0.01
1995	206	1603	5	14.938	3.02	26.69	0.02	0.01

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-205-AS

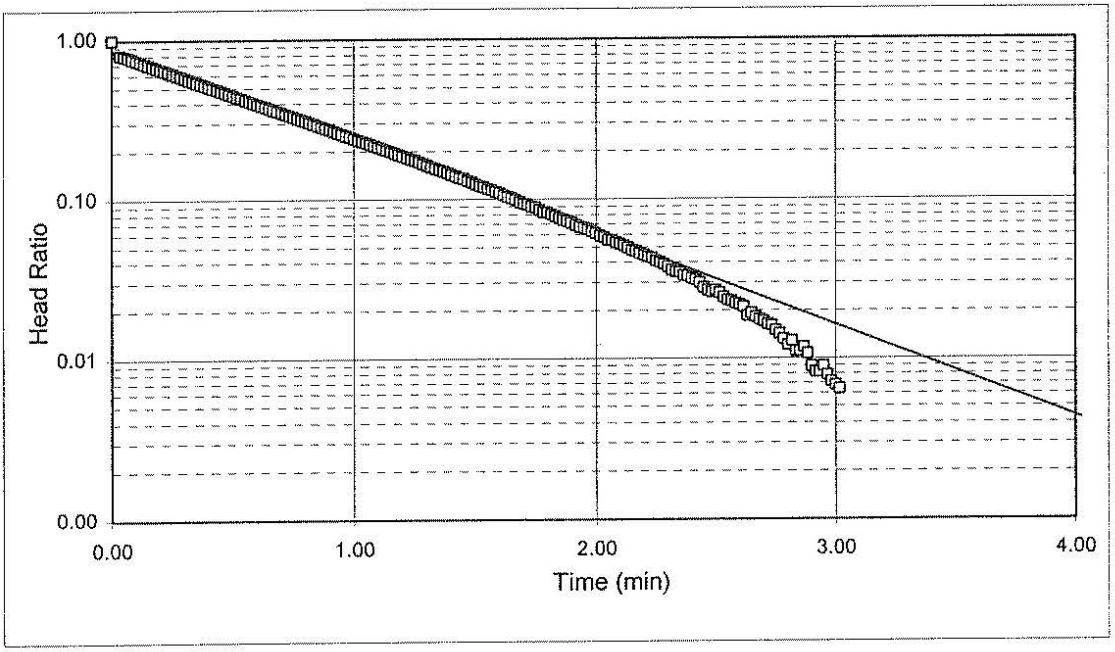
$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.34
L_e =	14.5
t_1 (min) =	0
t_2 (min) =	4.03
h_1/h_0 =	0.87
h_2/h_0 =	0.00

RESULTS

K=	6.03E-04	cm/sec
K=	1.71E+00	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/9/96

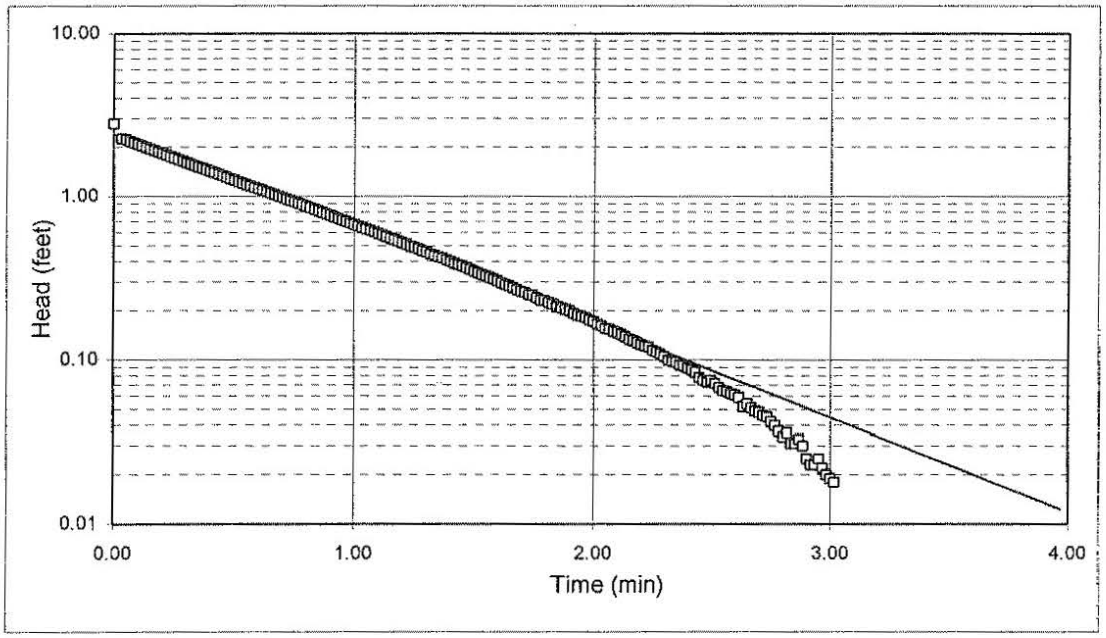
BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-205-AS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
r_w =	0.34			
L_e =	14.5	K=	4.36E-04	cm/sec
$\ln(R_e/r_w)$	2.70	K=	1.23E+00	ft/day
y_0 =	2.40			
y_t =	0.01			
t =	3.97			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/9/96

FALLING HEAD TEST PZ-205-SS

WELL NO. PZ-205-SS

DATE	7/18/95	
INITAL HEAD ON TRANSDUCER	10.86	FEET H_2O
INITIAL DEPTH TO WATER	37.66	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	86.2	FEET (btoc)
BOTTOM OF OPEN INTERVAL	100.7	FEET (btoc)
SATURATED THICKNESS	170	FEET
WATER TABLE TO BOTTOM OF SCREEN	63.04	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	14.5	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	2.34	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	199	856	0	13.195	0.0	35.33	2.34	1.000
1995	199	856	5	13.189	0.1	35.33	2.33	0.997
1995	199	856	10	13.173	0.2	35.35	2.31	0.991
1995	199	856	15	13.176	0.3	35.34	2.32	0.992
1995	199	856	20	13.161	0.3	35.36	2.30	0.985
1995	199	856	25	13.172	0.4	35.35	2.31	0.990
1995	199	856	30	13.174	0.5	35.35	2.31	0.991
1995	199	856	35	13.171	0.6	35.35	2.31	0.990
1995	199	856	40	13.172	0.7	35.35	2.31	0.990
1995	199	856	45	13.173	0.8	35.35	2.31	0.991
1995	199	856	50	13.171	0.8	35.35	2.31	0.990
1995	199	856	55	13.171	0.9	35.35	2.31	0.990
1995	199	857	0	13.171	1.0	35.35	2.31	0.990
1995	199	857	5	13.17	1.1	35.35	2.31	0.989
1995	199	857	10	13.17	1.2	35.35	2.31	0.989
1995	199	857	15	13.168	1.2	35.35	2.31	0.988
1995	199	857	20	13.169	1.3	35.35	2.31	0.989
1995	199	857	25	13.17	1.4	35.35	2.31	0.989
1995	199	857	30	13.096	1.5	35.42	2.24	0.958
1995	199	857	35	13.101	1.6	35.42	2.24	0.960
1995	199	857	40	13.103	1.7	35.42	2.24	0.961
1995	199	857	45	13.103	1.7	35.42	2.24	0.961
1995	199	857	50	13.104	1.8	35.42	2.24	0.961
1995	199	857	55	13.103	1.9	35.42	2.24	0.961
1995	199	858	0	13.103	2.0	35.42	2.24	0.961
1995	199	858	5	13.102	2.1	35.42	2.24	0.960
1995	199	858	10	13.104	2.2	35.42	2.24	0.961

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	199	858	15	13.103	2.2	35.42	2.24	0.961
1995	199	858	20	13.103	2.3	35.42	2.24	0.961
1995	199	858	25	13.102	2.4	35.42	2.24	0.960
1995	199	858	30	13.102	2.5	35.42	2.24	0.960
1995	199	858	35	13.102	2.6	35.42	2.24	0.960
1995	199	858	40	13.103	2.7	35.42	2.24	0.961
1995	199	858	45	13.102	2.7	35.42	2.24	0.960
1995	199	858	50	13.102	2.8	35.42	2.24	0.960
1995	199	858	55	13.101	2.9	35.42	2.24	0.960
1995	199	859	0	13.102	3.0	35.42	2.24	0.960
1995	199	859	5	13.101	3.1	35.42	2.24	0.960
1995	199	859	10	13.1	3.2	35.42	2.24	0.959
1995	199	859	15	13.101	3.2	35.42	2.24	0.960
1995	199	859	20	13.101	3.3	35.42	2.24	0.960
1995	199	859	25	13.103	3.4	35.42	2.24	0.961
1995	199	859	30	13.102	3.5	35.42	2.24	0.960
1995	199	859	35	13.102	3.6	35.42	2.24	0.960
1995	199	859	40	13.101	3.7	35.42	2.24	0.960
1995	199	859	45	13.101	3.7	35.42	2.24	0.960
1995	199	859	50	13.102	3.8	35.42	2.24	0.960
1995	199	859	55	13.101	3.9	35.42	2.24	0.960
1995	199	900	0	13.101	4.0	35.42	2.24	0.960
1995	199	900	5	13.101	4.1	35.42	2.24	0.960
1995	199	900	10	13.1	4.2	35.42	2.24	0.959
1995	199	900	15	13.1	4.2	35.42	2.24	0.959
1995	199	900	20	13.1	4.3	35.42	2.24	0.959
1995	199	900	25	13.099	4.4	35.42	2.24	0.959
1995	199	900	30	13.1	4.5	35.42	2.24	0.959
1995	199	900	35	13.099	4.6	35.42	2.24	0.959
1995	199	900	40	13.099	4.7	35.42	2.24	0.959
1995	199	900	45	13.1	4.7	35.42	2.24	0.959
1995	199	900	50	13.101	4.8	35.42	2.24	0.960
1995	199	900	55	13.102	4.9	35.42	2.24	0.960
1995	199	901	0	13.101	5.0	35.42	2.24	0.960
1995	199	901	5	13.1	5.1	35.42	2.24	0.959
1995	199	901	10	13.101	5.2	35.42	2.24	0.960
1995	199	901	15	13.101	5.2	35.42	2.24	0.960
1995	199	901	20	13.1	5.3	35.42	2.24	0.959
1995	199	901	25	13.1	5.4	35.42	2.24	0.959
1995	199	901	30	13.1	5.5	35.42	2.24	0.959
1995	199	901	35	13.1	5.6	35.42	2.24	0.959
1995	199	901	40	13.099	5.7	35.42	2.24	0.959
1995	199	901	45	13.098	5.7	35.42	2.24	0.958
1995	199	901	50	13.099	5.8	35.42	2.24	0.959
1995	199	901	55	13.098	5.9	35.42	2.24	0.958

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	199	902	0	13.098	6.0	35.42	2.24	0.958
1995	199	902	5	13.098	6.1	35.42	2.24	0.958
1995	199	902	10	13.098	6.2	35.42	2.24	0.958
1995	199	902	15	13.099	6.2	35.42	2.24	0.959
1995	199	902	20	13.098	6.3	35.42	2.24	0.958
1995	199	902	25	13.098	6.4	35.42	2.24	0.958
1995	199	902	30	13.097	6.5	35.42	2.24	0.958
1995	199	902	35	13.098	6.6	35.42	2.24	0.958
1995	199	902	40	13.098	6.7	35.42	2.24	0.958
1995	199	902	45	13.096	6.7	35.42	2.24	0.958
1995	199	902	50	13.095	6.8	35.43	2.24	0.957
1995	199	905	0	13.089	9.0	35.43	2.23	0.955
1995	199	910	0	13.077	14.0	35.44	2.22	0.949
1995	199	915	0	13.065	19.0	35.46	2.21	0.944
1995	199	920	0	13.054	24.0	35.47	2.19	0.940
1995	199	925	0	13.045	29.0	35.48	2.19	0.936
1995	199	930	0	13.035	34.0	35.49	2.18	0.931
1995	199	935	0	13.025	39.0	35.50	2.17	0.927
1995	199	940	0	13.016	44.0	35.50	2.16	0.923
1995	199	945	0	13.008	49.0	35.51	2.15	0.920
1995	199	950	0	12.998	54.0	35.52	2.14	0.916
1995	199	955	0	12.991	59.0	35.53	2.13	0.913
1995	199	1000	0	12.985	64.0	35.54	2.13	0.910
1995	199	1005	0	12.977	69.0	35.54	2.12	0.907
1995	199	1010	0	12.97	74.0	35.55	2.11	0.904
1995	199	1015	0	12.961	79.0	35.56	2.10	0.900
1995	199	1020	0	12.952	84.0	35.57	2.09	0.896
1995	199	1025	0	12.946	89.0	35.57	2.09	0.893
1995	199	1030	0	12.938	94.0	35.58	2.08	0.890
1995	199	1035	0	12.928	99.0	35.59	2.07	0.886
1995	199	1040	0	12.922	104.0	35.60	2.06	0.883
1995	199	1045	0	12.917	109.0	35.60	2.06	0.881
1995	199	1050	0	12.908	114.0	35.61	2.05	0.877
1995	199	1055	0	12.9	119.0	35.62	2.04	0.874
1995	199	1100	0	12.893	124.0	35.63	2.03	0.871
1995	199	1105	0	12.885	129.0	35.64	2.03	0.867
1995	199	1110	0	12.879	134.0	35.64	2.02	0.865
1995	199	1115	0	12.87	139.0	35.65	2.01	0.861
1995	199	1120	0	12.861	144.0	35.66	2.00	0.857
1995	199	1125	0	12.853	149.0	35.67	1.99	0.854
1995	199	1130	0	12.844	154.0	35.68	1.98	0.850
1995	199	1135	0	12.837	159.0	35.68	1.98	0.847
1995	199	1140	0	12.828	164.0	35.69	1.97	0.843
1995	199	1145	0	12.82	169.0	35.70	1.96	0.839
1995	199	1150	0	12.813	174.0	35.71	1.95	0.836

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
1995	199	1155	0	12.805	179.0	35.72	1.95	0.833
1995	199	1200	0	12.795	184.0	35.73	1.94	0.829
1995	199	1205	0	12.789	189.0	35.73	1.93	0.826
1995	199	1210	0	12.78	194.0	35.74	1.92	0.822
1995	199	1215	0	12.771	199.0	35.75	1.91	0.818
1995	199	1220	0	12.765	204.0	35.76	1.91	0.816
1995	199	1225	0	12.755	209.0	35.77	1.90	0.812
1995	199	1230	0	12.745	214.0	35.78	1.89	0.807
1995	199	1235	0	12.737	219.0	35.78	1.88	0.804
1995	199	1240	0	12.728	224.0	35.79	1.87	0.800
1995	199	1245	0	12.718	229.0	35.80	1.86	0.796
1995	199	1250	0	12.71	234.0	35.81	1.85	0.792
1995	199	1255	0	12.704	239.0	35.82	1.84	0.790
1995	199	1300	0	12.697	244.0	35.82	1.84	0.787
1995	199	1305	0	12.689	249.0	35.83	1.83	0.783
1995	199	1310	0	12.681	254.0	35.84	1.82	0.780
1995	199	1315	0	12.671	259.0	35.85	1.81	0.776
1995	199	1320	0	12.665	264.0	35.86	1.81	0.773
1995	199	1325	0	12.657	269.0	35.86	1.80	0.770
1995	199	1330	0	12.647	274.0	35.87	1.79	0.765
1995	199	1335	0	12.637	279.0	35.88	1.78	0.761
1995	199	1340	0	12.631	284.0	35.89	1.77	0.758
1995	199	1345	0	12.62	289.0	35.90	1.76	0.754
1995	199	1350	0	12.614	294.0	35.91	1.75	0.751
1995	199	1355	0	12.608	299.0	35.91	1.75	0.749
1995	199	1400	0	12.595	304.0	35.93	1.74	0.743
1995	199	1405	0	12.591	309.0	35.93	1.73	0.741
1995	199	1410	0	12.578	314.0	35.94	1.72	0.736
1995	199	1415	0	12.569	319.0	35.95	1.71	0.732
1995	199	1420	0	12.562	324.0	35.96	1.70	0.729
1995	199	1425	0	12.555	329.0	35.97	1.70	0.726
1995	199	1430	0	12.549	334.0	35.97	1.69	0.723
1995	199	1435	0	12.539	339.0	35.98	1.68	0.719
1995	199	1440	0	12.53	344.0	35.99	1.67	0.715
1995	199	1445	0	12.522	349.0	36.00	1.66	0.712
1995	199	1450	0	12.514	354.0	36.01	1.65	0.708
1995	199	1455	0	12.507	359.0	36.01	1.65	0.705
1995	199	1500	0	12.503	364.0	36.02	1.64	0.704
1995	199	1505	0	12.492	369.0	36.03	1.63	0.699

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-205-SS

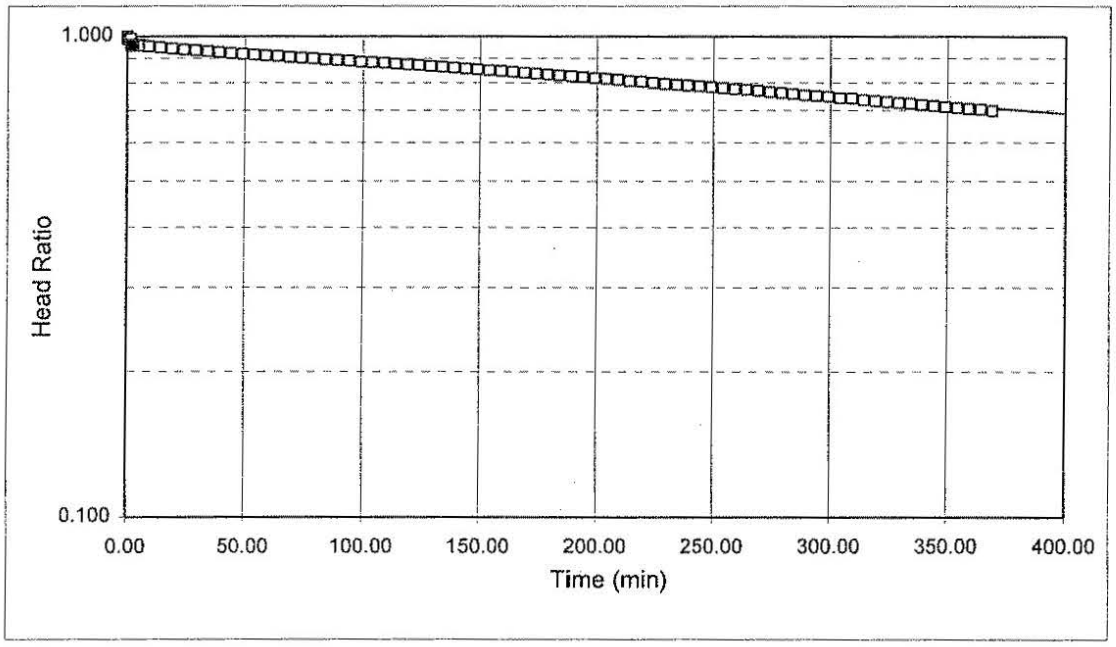
$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	14.5
t_1 (min) =	0
t_2 (min) =	400.00
h_1/h_0 =	0.98
h_2/h_0 =	0.69

RESULTS

K=	4.36E-07	cm/sec
K=	1.23E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/18/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/9/96

BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-205-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

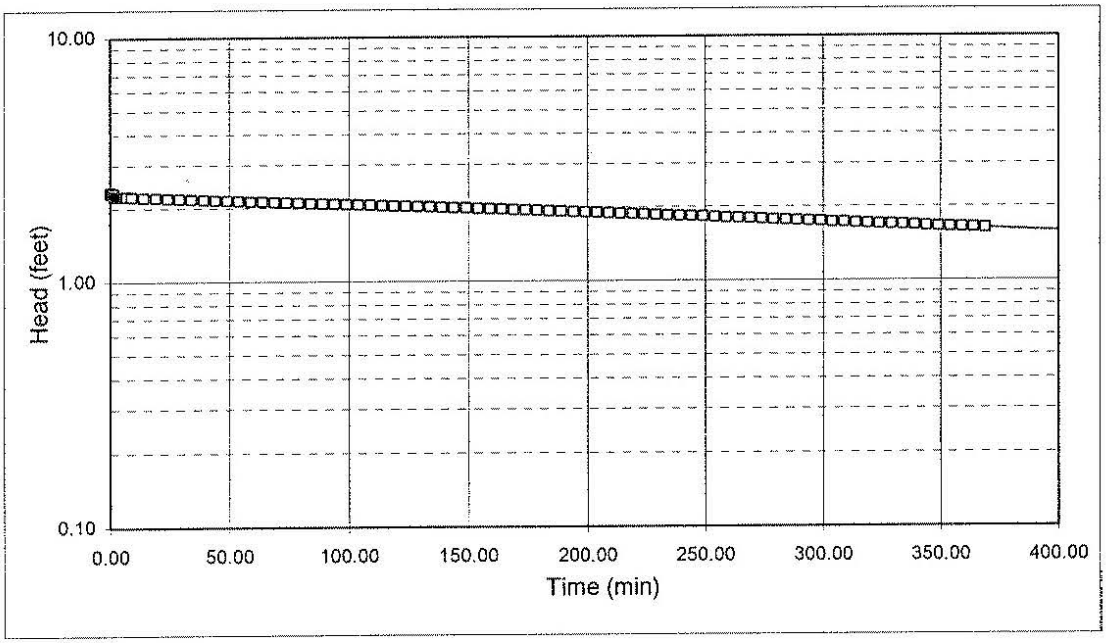
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.25
L_e =	14.5
$\ln(R_e/r_w)$	3.43
y_0 =	2.30
y_t =	1.58
t =	400.00

RESULTS

K=	3.88E-07	cm/sec
K=	1.10E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/18/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/9/96

RISING HEAD TEST PZ-206-SS

WELL NO. PZ-206-SS

DATE	6/23/95	
INITIAL DEPTH TO WATER	40.14	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	112.9	FEET (btoc)
BOTTOM OF OPEN INTERVAL	127.3	FEET (btoc)
SATURATED THICKNESS	160	FEET
WATER TABLE TO BOTTOM OF SCREEN	87.16	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	14.4	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	5.60	FEET
MAX. HEAD IN SCREEN?	N	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1152	0	45.74	0.0	5.60	1.00
1	1154	0	45.2	2.0	5.06	0.90
1	1155	0	44.96	3.0	4.82	0.86
1	1155	30	44.84	3.5	4.70	0.84
1	1156	0	44.75	4.0	4.61	0.82
1	1157	0	44.62	5.0	4.48	0.80
1	1157	30	44.49	5.5	4.35	0.78
1	1158	30	44.29	6.5	4.15	0.74
1	1159	0	44.16	7.0	4.02	0.72
1	1159	30	44.11	7.5	3.97	0.71
1	1200	0	44.04	8.0	3.90	0.70
1	1201	0	43.89	9.0	3.75	0.67
1	1201	30	43.8	9.5	3.66	0.65
1	1202	0	43.73	10.0	3.59	0.64
1	1202	30	43.67	10.5	3.53	0.63
1	1203	0	43.61	11.0	3.47	0.62
1	1203	30	43.54	11.5	3.40	0.61
1	1204	0	43.47	12.0	3.33	0.59
1	1204	30	43.39	12.5	3.25	0.58
1	1205	0	43.35	13.0	3.21	0.57
1	1205	30	43.28	13.5	3.14	0.56
1	1206	0	43.24	14.0	3.10	0.55
1	1207	0	43.13	15.0	2.99	0.53
1	1208	0	43.01	16.0	2.87	0.51

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1209	0	42.91	17.0	2.77	0.49
1	1210	0	42.81	18.0	2.67	0.48
1	1211	0	42.71	19.0	2.57	0.46
1	1212	0	42.62	20.0	2.48	0.44
1	1213	0	42.54	21.0	2.40	0.43
1	1214	0	42.46	22.0	2.32	0.41
1	1215	0	42.39	23.0	2.25	0.40
1	1220	0	42.02	28.0	1.88	0.34
1	1221	0	41.96	29.0	1.82	0.33
1	1222	0	41.9	30.0	1.76	0.31
1	1223	0	41.82	31.0	1.68	0.30
1	1224	0	41.78	32.0	1.64	0.29
1	1225	0	41.74	33.0	1.60	0.29
1	1226	0	41.68	34.0	1.54	0.28
1	1227	0	41.64	35.0	1.50	0.27
1	1228	0	41.58	36.0	1.44	0.26
1	1229	0	41.52	37.0	1.38	0.25
1	1230	0	41.48	38.0	1.34	0.24
1	1235	0	41.29	43.0	1.15	0.21
1	1240	0	41.09	48.0	0.95	0.17
1	1245	0	40.96	53.0	0.82	0.15
1	1250	0	40.84	58.0	0.70	0.13
1	1255	0	40.71	63.0	0.57	0.10

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-206-SS

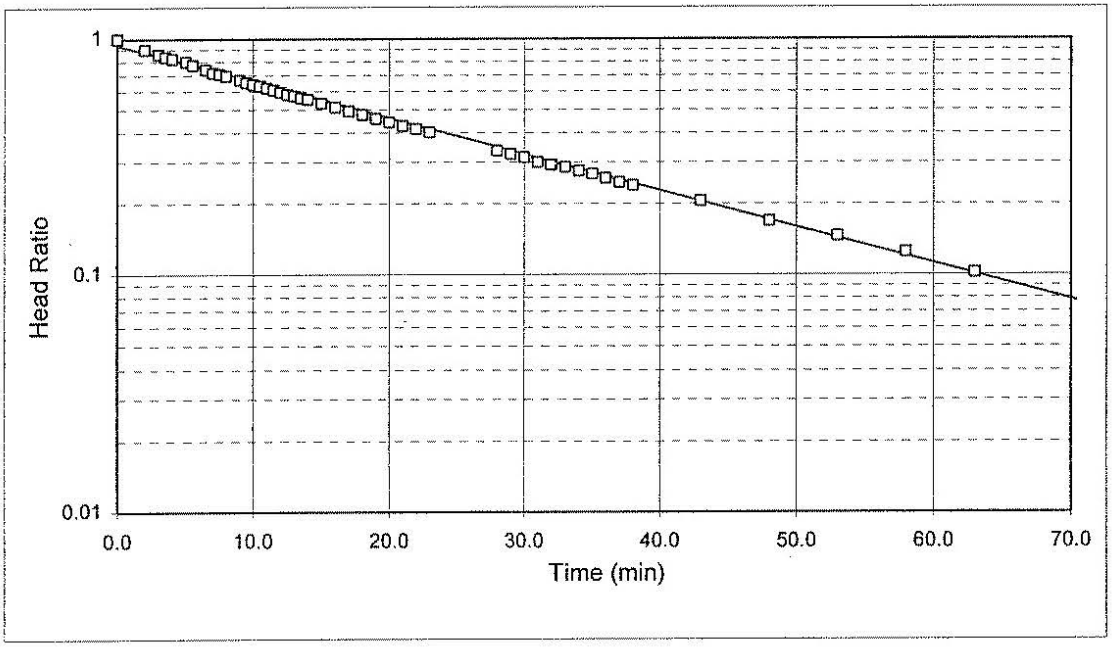
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where:
r_c = casing radius (feet)
R_e = filter pack radius (feet)
L_e = length of screened interval (feet)
t = time (seconds)
h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	14.4
t_1 (min) =	0
t_2 (min) =	70.4
h_1/h_0 =	0.94
h_2/h_0 =	0.08

RESULTS

K=	1.76E-05	cm/sec
K=	4.99E-02	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 06/23/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/10/96

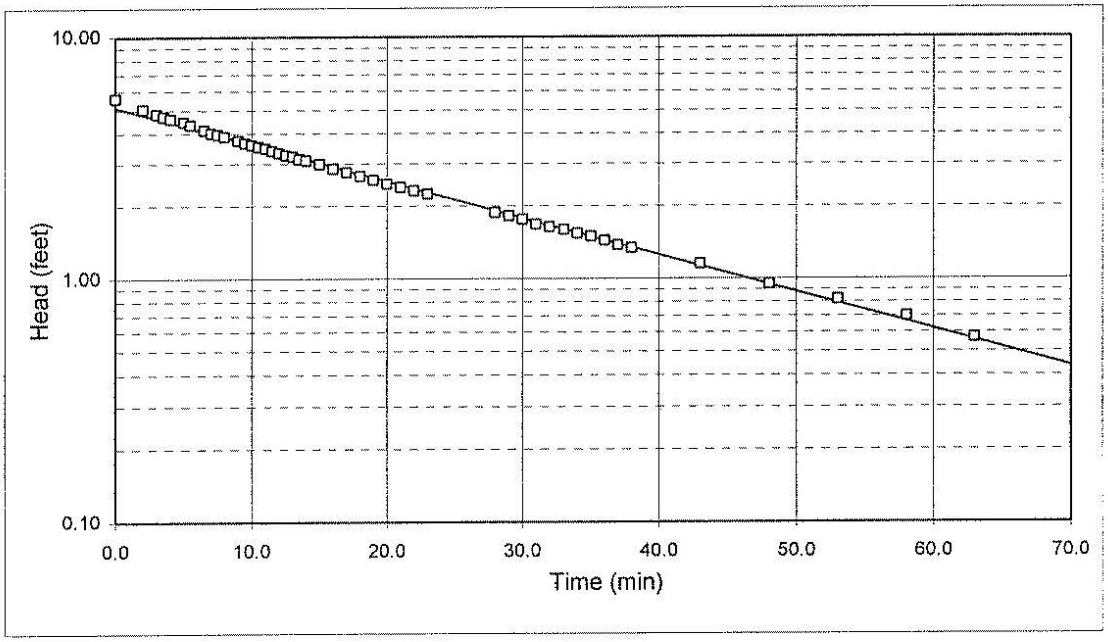
BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-206-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
r_w =	0.25			
L_e =	14.4	K=	1.13E-05	cm/sec
$\ln(R_e/r_w)$	3.41	K=	3.19E-02	ft/day
y_0 =	5.13			
y_t =	0.44			
t =	70.0			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 06/23/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/10/96

RISING HEAD TEST PZ-207-AS

WELL NO. PZ-207-AS

DATE	7/21/95	
INITAL HEAD ON TRANSDUCER	10.316	FEET H_2O
INITIAL DEPTH TO WATER	28.06	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	33.7	FEET (btoc)
BOTTOM OF OPEN INTERVAL	41.7	FEET (btoc)
SATURATED THICKNESS	120	FEET
WATER TABLE TO BOTTOM OF SCREEN	13.64	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	8	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	1.25	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	202	1127	32	9.063	0.00	29.31	1.25	1.00
305	202	1127	33	9.3334	0.02	29.04	0.98	0.78
305	202	1127	34	9.5265	0.03	28.85	0.79	0.63
305	202	1127	35	9.6731	0.05	28.70	0.64	0.51
305	202	1127	36	9.7758	0.07	28.60	0.54	0.43
305	202	1127	37	9.8567	0.08	28.52	0.46	0.37
305	202	1127	38	9.9132	0.10	28.46	0.40	0.32
305	202	1127	39	9.9567	0.12	28.42	0.36	0.29
305	202	1127	40	9.9925	0.13	28.38	0.32	0.26
305	202	1127	41	10.017	0.15	28.36	0.30	0.24
305	202	1127	42	10.034	0.17	28.34	0.28	0.23
305	202	1127	43	10.17	0.18	28.21	0.15	0.12
305	202	1127	44	10.184	0.20	28.19	0.13	0.11
305	202	1127	45	10.193	0.22	28.18	0.12	0.10
305	202	1127	46	10.197	0.23	28.18	0.12	0.09
305	202	1127	47	10.204	0.25	28.17	0.11	0.09
305	202	1127	48	10.208	0.27	28.17	0.11	0.09
305	202	1127	49	10.209	0.28	28.17	0.11	0.09
305	202	1127	50	10.214	0.30	28.16	0.10	0.08
305	202	1127	51	10.215	0.32	28.16	0.10	0.08
305	202	1127	52	10.216	0.33	28.16	0.10	0.08
305	202	1127	53	10.218	0.35	28.16	0.10	0.08
305	202	1127	54	10.22	0.37	28.16	0.10	0.08
305	202	1127	55	10.221	0.38	28.16	0.10	0.08

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	202	1127	56	10.221	0.40	28.16	0.10	0.08
305	202	1127	57	10.222	0.42	28.15	0.09	0.08
305	202	1127	58	10.223	0.43	28.15	0.09	0.07
305	202	1127	59	10.224	0.45	28.15	0.09	0.07
305	202	1128	0	10.223	0.47	28.15	0.09	0.07
305	202	1128	1	10.224	0.48	28.15	0.09	0.07
305	202	1128	2	10.225	0.50	28.15	0.09	0.07
305	202	1128	3	10.226	0.52	28.15	0.09	0.07
305	202	1128	4	10.225	0.53	28.15	0.09	0.07
305	202	1128	5	10.225	0.55	28.15	0.09	0.07
305	202	1128	6	10.226	0.57	28.15	0.09	0.07
305	202	1128	7	10.225	0.58	28.15	0.09	0.07
305	202	1128	8	10.226	0.60	28.15	0.09	0.07
305	202	1128	9	10.228	0.62	28.15	0.09	0.07
305	202	1128	10	10.226	0.63	28.15	0.09	0.07
305	202	1128	11	10.226	0.65	28.15	0.09	0.07
305	202	1128	12	10.226	0.67	28.15	0.09	0.07
305	202	1128	13	10.226	0.68	28.15	0.09	0.07
305	202	1128	14	10.226	0.70	28.15	0.09	0.07
305	202	1128	15	10.226	0.72	28.15	0.09	0.07
305	202	1128	16	10.227	0.73	28.15	0.09	0.07
305	202	1128	17	10.228	0.75	28.15	0.09	0.07
305	202	1128	18	10.226	0.77	28.15	0.09	0.07
305	202	1128	19	10.228	0.78	28.15	0.09	0.07
305	202	1128	20	10.228	0.80	28.15	0.09	0.07
305	202	1128	21	10.227	0.82	28.15	0.09	0.07
305	202	1128	22	10.229	0.83	28.15	0.09	0.07
305	202	1128	23	10.227	0.85	28.15	0.09	0.07
305	202	1128	24	10.227	0.87	28.15	0.09	0.07
305	202	1128	25	10.227	0.88	28.15	0.09	0.07
305	202	1128	26	10.229	0.90	28.15	0.09	0.07
305	202	1128	27	10.228	0.92	28.15	0.09	0.07
305	202	1128	28	10.228	0.93	28.15	0.09	0.07
305	202	1128	29	10.227	0.95	28.15	0.09	0.07
305	202	1128	30	10.228	0.97	28.15	0.09	0.07
305	202	1128	31	10.228	0.98	28.15	0.09	0.07
305	202	1128	32	10.228	1.00	28.15	0.09	0.07
305	202	1128	33	10.229	1.02	28.15	0.09	0.07
305	202	1128	34	10.228	1.03	28.15	0.09	0.07
305	202	1128	35	10.229	1.05	28.15	0.09	0.07
305	202	1128	36	10.228	1.07	28.15	0.09	0.07
305	202	1128	37	10.228	1.08	28.15	0.09	0.07

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	202	1128	38	10.228	1.10	28.15	0.09	0.07
305	202	1128	39	10.229	1.12	28.15	0.09	0.07
305	202	1128	40	10.228	1.13	28.15	0.09	0.07
305	202	1128	41	10.229	1.15	28.15	0.09	0.07
305	202	1128	42	10.229	1.17	28.15	0.09	0.07
305	202	1128	43	10.23	1.18	28.15	0.09	0.07
305	202	1128	44	10.229	1.20	28.15	0.09	0.07
305	202	1128	45	10.229	1.22	28.15	0.09	0.07
305	202	1128	46	10.228	1.23	28.15	0.09	0.07
305	202	1128	47	10.231	1.25	28.15	0.09	0.07
305	202	1128	48	10.239	1.27	28.14	0.08	0.06
305	202	1128	49	10.239	1.28	28.14	0.08	0.06
305	202	1128	50	10.239	1.30	28.14	0.08	0.06
305	202	1128	51	10.239	1.32	28.14	0.08	0.06
305	202	1128	52	10.24	1.33	28.14	0.08	0.06
305	202	1128	53	10.241	1.35	28.14	0.07	0.06
305	202	1128	54	10.24	1.37	28.14	0.08	0.06
305	202	1128	55	10.24	1.38	28.14	0.08	0.06
305	202	1128	56	10.239	1.40	28.14	0.08	0.06
305	202	1128	57	10.242	1.42	28.13	0.07	0.06
305	202	1128	58	10.24	1.43	28.14	0.08	0.06
305	202	1128	59	10.241	1.45	28.14	0.07	0.06
305	202	1129	0	10.24	1.47	28.14	0.08	0.06
305	202	1129	1	10.24	1.48	28.14	0.08	0.06
305	202	1129	2	10.24	1.50	28.14	0.08	0.06
305	202	1129	3	10.24	1.52	28.14	0.08	0.06
305	202	1129	4	10.24	1.53	28.14	0.08	0.06
305	202	1129	5	10.242	1.55	28.13	0.07	0.06
305	202	1129	6	10.242	1.57	28.13	0.07	0.06
305	202	1129	7	10.242	1.58	28.13	0.07	0.06
305	202	1129	8	10.239	1.60	28.14	0.08	0.06
305	202	1129	9	10.241	1.62	28.14	0.07	0.06
305	202	1129	10	10.241	1.63	28.14	0.07	0.06
305	202	1129	11	10.241	1.65	28.14	0.07	0.06
305	202	1129	12	10.241	1.67	28.14	0.07	0.06
305	202	1129	13	10.242	1.68	28.13	0.07	0.06
305	202	1129	14	10.243	1.70	28.13	0.07	0.06

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-207-AS

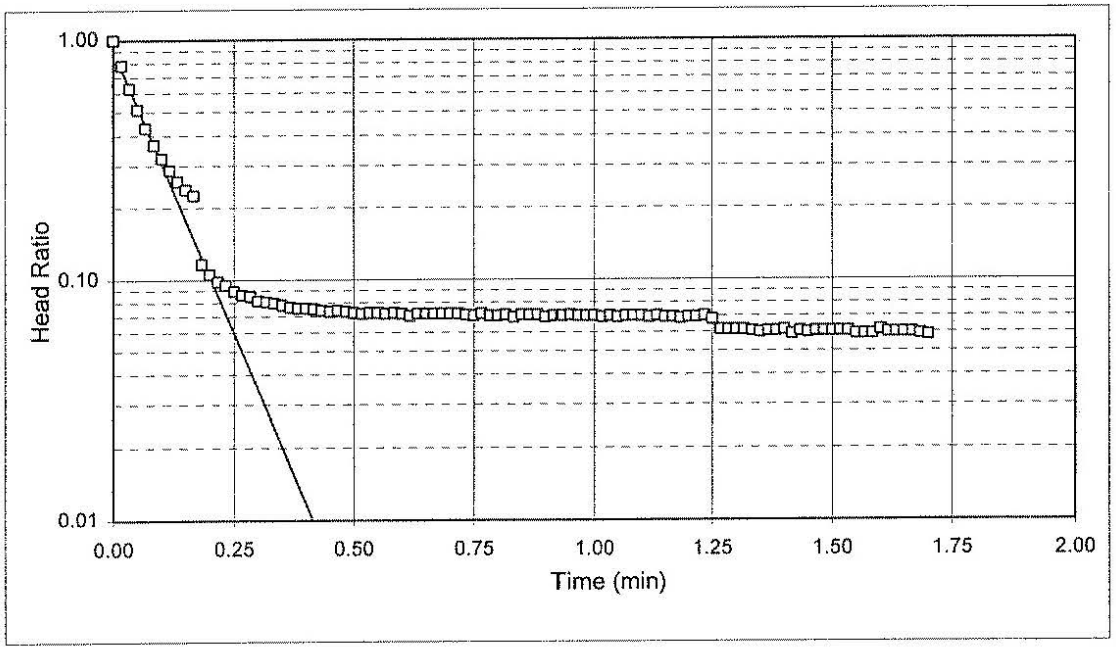
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.34
L_e =	8
t_1 (min) =	0.013
t_2 (min) =	0.41
h_1/h_0 =	0.79
h_2/h_0 =	0.01

RESULTS

K=	7.55E-03	cm/sec
K=	2.14E+01	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/21/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/10/96

BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-207-AS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

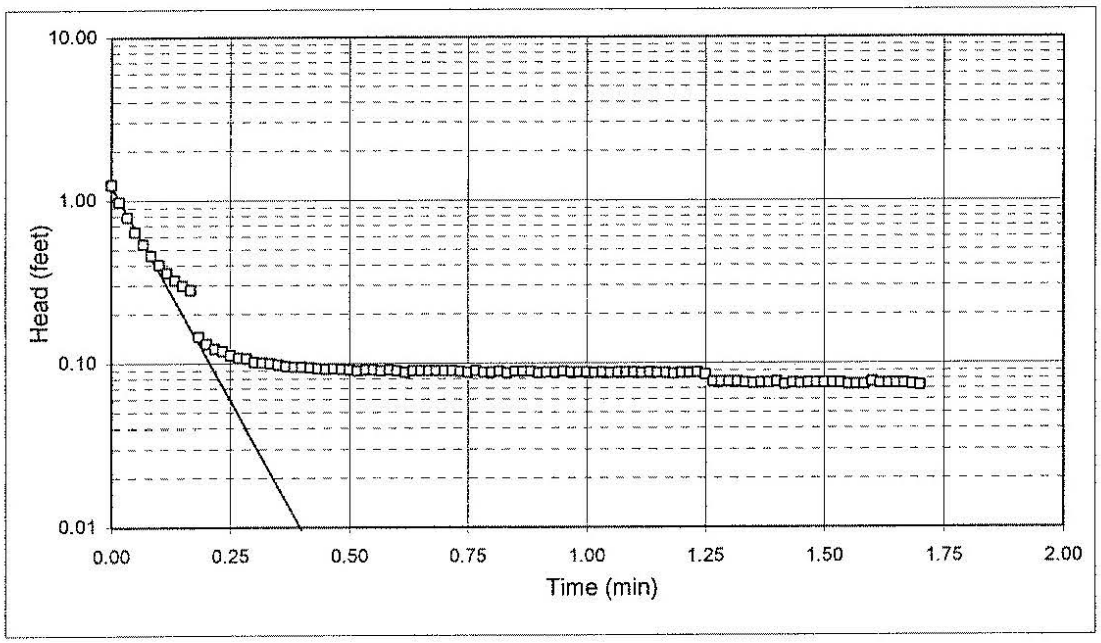
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.34
L_e =	8
$\ln(R_e/r_w)$	1.78
y_0 =	1.23
y_t =	0.01
t =	0.40

RESULTS

K=	4.76E-03	cm/sec
K=	1.35E+01	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/21/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/10/96

RISING HEAD TEST PZ-208-SS

WELL NO. PZ-208-SS

DATE	7/25/95	
INITIAL DEPTH TO WATER	37.81	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	85.6	FEET (btoc)
BOTTOM OF OPEN INTERVAL	100.9	FEET (btoc)
SATURATED THICKNESS	190	FEET
WATER TABLE TO BOTTOM OF SCREEN	63.09	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	15.3	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	1.92	FEET
MAX. HEAD IN SCREEN?	N	

DAY	HR-MIN	SEC	DEPTH TO WATER (FEET)	ELAPSED TIME (MIN)	HEAD (FEET)	HEAD RATIO
1	1003	0	39.73	0.0	1.92	1.00
1	1004	0	39.71	1.0	1.90	0.99
1	1005	0	39.71	2.0	1.90	0.99
1	1010	0	39.7	7.0	1.89	0.98
1	1018	0	39.69	15.0	1.88	0.98
1	1155	0	39.49	112.0	1.68	0.88
1	1751	0	39.14	468.0	1.33	0.69
2	1241	0	38.42	1598.0	0.61	0.32
2	1627	0	38.29	1824.0	0.48	0.25
3	720	0	37.97	2717.0	0.16	0.08
3	1350	0	37.88	3107.0	0.07	0.04

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-208-SS

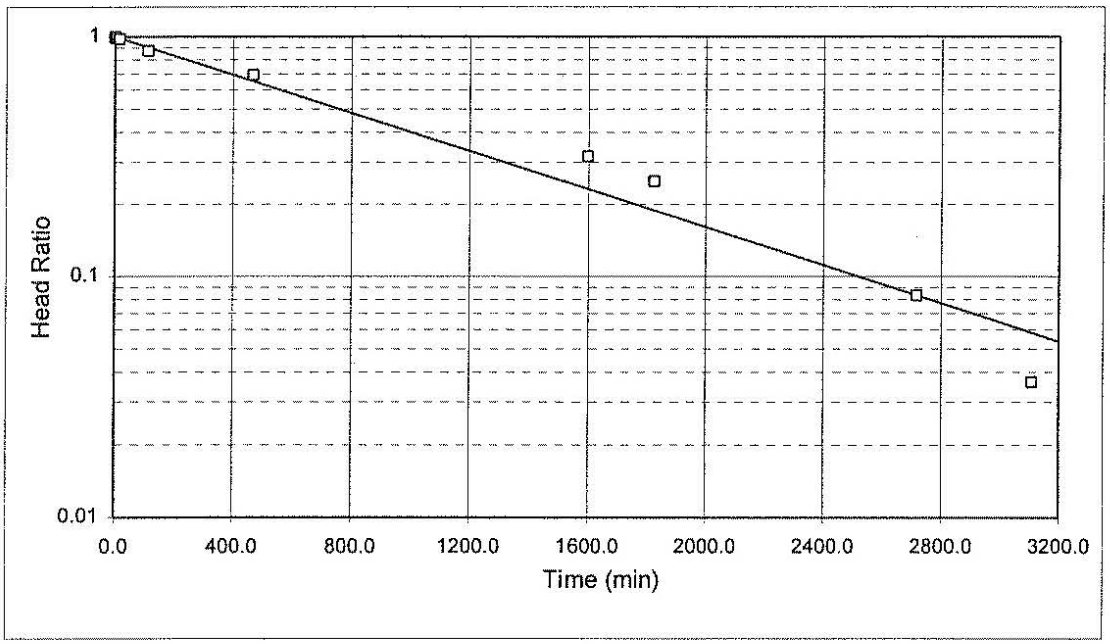
$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where:
- r_c = casing radius (feet)
- R_e = filter pack radius (feet)
- L_e = length of screened interval (feet)
- t = time (seconds)
- h_t = head at time t (feet)

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	15.3
t_1 (min) =	0
t_2 (min) =	3200
h_1/h_0 =	1.00
h_2/h_0 =	0.05

RESULTS

K=	4.33E-07	cm/sec
K=	1.23E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/10/96

BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-208-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

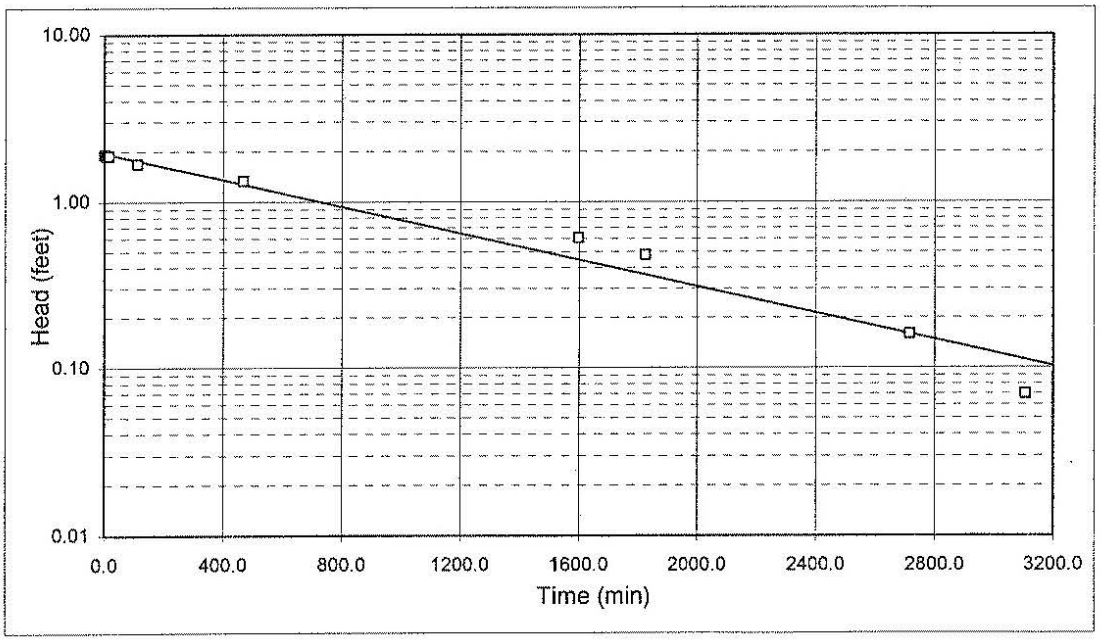
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.25
L_e =	15.3
$\ln(R_e/r_w)$	3.26
y_0 =	1.95
y_t =	0.10
t =	3200.0

RESULTS

K=	2.73E-07	cm/sec
K=	7.73E-04	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 07/25/95

Analysis By: CVK
Checked By: DSL
Analysis Date: 1/10/96

FALLING HEAD TEST PZ-300-AS

WELL NO. PZ-300-AS

DATE	10/21/95	
INITAL HEAD ON TRANSDUCER	6.69	FEET H_2O
INITIAL DEPTH TO WATER	14.48	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	8.46	FEET (btoc)
BOTTOM OF OPEN INTERVAL	22.16	FEET (btoc)
SATURATED THICKNESS	30	FEET
WATER TABLE TO BOTTOM OF SCREEN	7.68	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	7.68	FEET
STATIC IN SCREEN?	Y	
MAX. HEAD CHANGE	0.25	FEET
MAX. HEAD IN SCREEN?	Y	

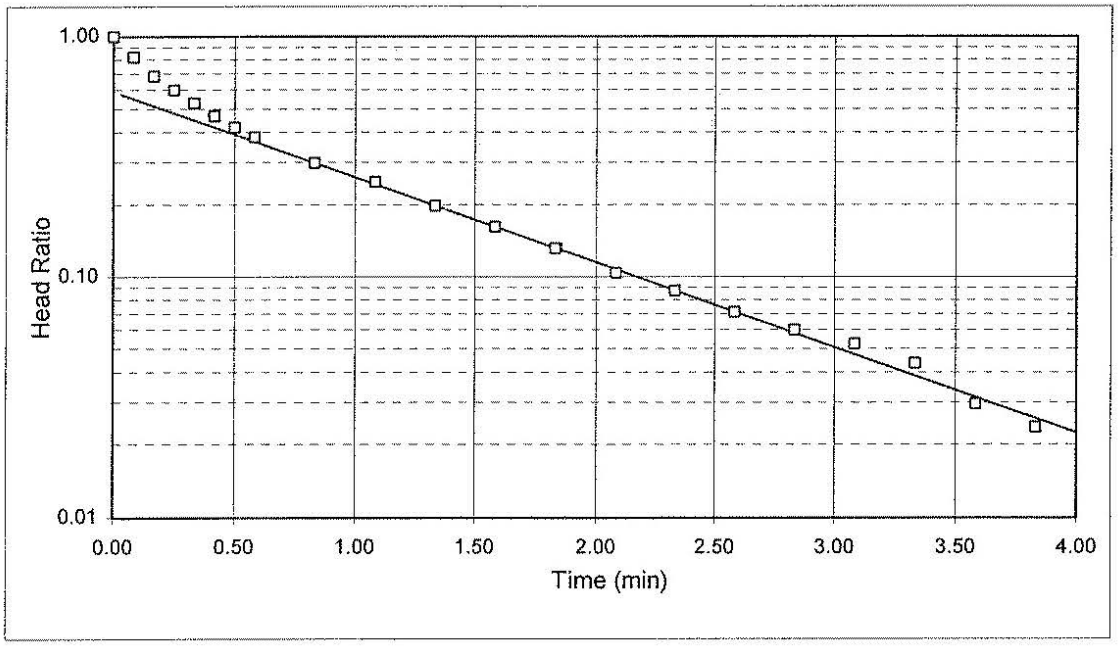
DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
307	295	1135	36	6.9399	0.00	14.23	0.25	1.00
307	295	1135	41	6.895	0.08	14.28	0.20	0.82
307	295	1135	46	6.8614	0.17	14.31	0.17	0.69
307	295	1135	51	6.8398	0.25	14.33	0.15	0.60
307	295	1135	56	6.8222	0.33	14.35	0.13	0.53
307	295	1136	1	6.807	0.42	14.36	0.12	0.47
307	295	1136	6	6.7949	0.50	14.38	0.10	0.42
307	295	1136	11	6.7854	0.58	14.38	0.10	0.38
307	295	1136	26	6.7646	0.83	14.41	0.07	0.30
307	295	1136	41	6.7522	1.08	14.42	0.06	0.25
307	295	1136	56	6.7395	1.33	14.43	0.05	0.20
307	295	1137	11	6.7304	1.58	14.44	0.04	0.16
307	295	1137	26	6.7229	1.83	14.45	0.03	0.13
307	295	1137	41	6.7159	2.08	14.45	0.03	0.10
307	295	1137	56	6.7118	2.33	14.46	0.02	0.09
307	295	1138	11	6.7078	2.58	14.46	0.02	0.07
307	295	1138	26	6.705	2.83	14.47	0.02	0.06
307	295	1138	41	6.7031	3.08	14.47	0.01	0.05
307	295	1138	56	6.7009	3.33	14.47	0.01	0.04
307	295	1139	11	6.6974	3.58	14.47	0.01	0.03
307	295	1139	26	6.6959	3.83	14.47	0.01	0.02

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-300-AS

$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
R_e =	0.34			
L_e =	7.68	K=	5.83E-04	cm/sec
t_1 (min) =	0.03	K=	1.65E+00	ft/day
t_2 (min) =	4.00			
h_1/h_0 =	0.58			
h_2/h_0 =	0.02			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/21/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

FALLING HEAD TEST PZ-303-AS

WELL NO. PZ-303-AS

DATE	10/31/95	
INITAL HEAD ON TRANSDUCER	6.3	FEET H_2O
INITIAL DEPTH TO WATER	20.96	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	10.25	INCHES
TOP OF OPEN INTERVAL	14.2	FEET (btoc)
BOTTOM OF OPEN INTERVAL	28.9	FEET (btoc)
SATURATED THICKNESS	130	FEET
WATER TABLE TO BOTTOM OF SCREEN	7.92	FEET
EQUIVALENT DIAMETER	5.86	INCHES
OPEN INTERVAL LENGTH	7.92	FEET
STATIC IN SCREEN?	Y	
MAX. HEAD CHANGE	0.62	FEET
MAX. HEAD IN SCREEN?	Y	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	305	1145	17	6.9176	0.00	20.34	0.62	1.00
305	305	1145	18	6.8904	0.02	20.37	0.59	0.96
305	305	1145	19	6.7545	0.03	20.51	0.45	0.74
305	305	1145	20	6.8514	0.05	20.41	0.55	0.89
305	305	1145	21	6.7295	0.07	20.53	0.43	0.70
305	305	1145	22	6.7046	0.08	20.56	0.40	0.66
305	305	1145	23	6.6789	0.10	20.58	0.38	0.61
305	305	1145	24	6.6451	0.12	20.61	0.35	0.56
305	305	1145	25	6.633	0.13	20.63	0.33	0.54
305	305	1145	26	6.6206	0.15	20.64	0.32	0.52
305	305	1145	27	6.6191	0.17	20.64	0.32	0.52
305	305	1145	28	6.6088	0.18	20.65	0.31	0.50
305	305	1145	29	6.6027	0.20	20.66	0.30	0.49
305	305	1145	30	6.5975	0.22	20.66	0.30	0.48
305	305	1145	31	6.5928	0.23	20.67	0.29	0.47
305	305	1145	32	6.5846	0.25	20.68	0.28	0.46
305	305	1145	33	6.5853	0.27	20.67	0.29	0.46
305	305	1145	34	6.5764	0.28	20.68	0.28	0.45
305	305	1145	35	6.5711	0.30	20.69	0.27	0.44
305	305	1145	36	6.5672	0.32	20.69	0.27	0.43
305	305	1145	37	6.5631	0.33	20.70	0.26	0.43
305	305	1145	38	6.5586	0.35	20.70	0.26	0.42
305	305	1145	39	6.5554	0.37	20.70	0.26	0.41
305	305	1145	40	6.5495	0.38	20.71	0.25	0.40
305	305	1145	41	6.5459	0.40	20.71	0.25	0.40
305	305	1145	42	6.5439	0.42	20.72	0.24	0.39
305	305	1145	43	6.5392	0.43	20.72	0.24	0.39

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	305	1145	44	6.5352	0.45	20.72	0.24	0.38
305	305	1145	45	6.5311	0.47	20.73	0.23	0.37
305	305	1145	46	6.5272	0.48	20.73	0.23	0.37
305	305	1145	47	6.5248	0.50	20.74	0.22	0.36
305	305	1145	48	6.5178	0.52	20.74	0.22	0.35
305	305	1145	49	6.5121	0.53	20.75	0.21	0.34
305	305	1145	50	6.5118	0.55	20.75	0.21	0.34
305	305	1145	51	6.5109	0.57	20.75	0.21	0.34
305	305	1145	52	6.5093	0.58	20.75	0.21	0.34
305	305	1145	53	6.5075	0.60	20.75	0.21	0.34
305	305	1145	54	6.5053	0.62	20.75	0.21	0.33
305	305	1145	55	6.5022	0.63	20.76	0.20	0.33
305	305	1145	56	6.5	0.65	20.76	0.20	0.32
305	305	1145	57	6.4975	0.67	20.76	0.20	0.32
305	305	1145	58	6.4947	0.68	20.77	0.19	0.32
305	305	1145	59	6.4922	0.70	20.77	0.19	0.31
305	305	1146	0	6.4907	0.72	20.77	0.19	0.31
305	305	1146	1	6.4879	0.73	20.77	0.19	0.30
305	305	1146	2	6.489	0.75	20.77	0.19	0.31
305	305	1146	3	6.485	0.77	20.78	0.19	0.30
305	305	1146	4	6.4871	0.78	20.77	0.19	0.30
305	305	1146	5	6.3968	0.80	20.86	0.10	0.16
305	305	1146	6	6.4968	0.82	20.76	0.20	0.32
305	305	1146	7	6.4873	0.83	20.77	0.19	0.30
305	305	1146	8	6.4824	0.85	20.78	0.18	0.30
305	305	1146	9	6.4792	0.87	20.78	0.18	0.29
305	305	1146	10	6.4767	0.88	20.78	0.18	0.29
305	305	1146	11	6.4737	0.90	20.79	0.17	0.28
305	305	1146	12	6.4714	0.92	20.79	0.17	0.28
305	305	1146	13	6.4687	0.93	20.79	0.17	0.27
305	305	1146	14	6.4673	0.95	20.79	0.17	0.27
305	305	1146	15	6.4659	0.97	20.79	0.17	0.27
305	305	1146	16	6.4643	0.98	20.80	0.16	0.27
305	305	1146	17	6.4666	1.00	20.79	0.17	0.27
305	305	1146	18	6.465	1.02	20.80	0.16	0.27
305	305	1146	19	6.4608	1.03	20.80	0.16	0.26
305	305	1146	20	6.4656	1.05	20.79	0.17	0.27
305	305	1146	21	6.4583	1.07	20.80	0.16	0.26
305	305	1146	22	6.4613	1.08	20.80	0.16	0.26
305	305	1146	23	6.4606	1.10	20.80	0.16	0.26
305	305	1146	24	6.4562	1.12	20.80	0.16	0.25
305	305	1146	25	6.4551	1.13	20.80	0.16	0.25
305	305	1146	26	6.4573	1.15	20.80	0.16	0.25
305	305	1146	27	6.4571	1.17	20.80	0.16	0.25
305	305	1146	28	6.4521	1.18	20.81	0.15	0.25

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	305	1146	29	6.4508	1.20	20.81	0.15	0.24
305	305	1146	30	6.4507	1.22	20.81	0.15	0.24
305	305	1146	31	6.4527	1.23	20.81	0.15	0.25
305	305	1146	32	6.4513	1.25	20.81	0.15	0.24
305	305	1146	33	6.4476	1.27	20.81	0.15	0.24
305	305	1146	34	6.4488	1.28	20.81	0.15	0.24
305	305	1146	35	6.4485	1.30	20.81	0.15	0.24
305	305	1146	36	6.4466	1.32	20.81	0.15	0.24
305	305	1146	37	6.4463	1.33	20.81	0.15	0.24
305	305	1146	38	6.4403	1.35	20.82	0.14	0.23
305	305	1146	39	6.4402	1.37	20.82	0.14	0.23
305	305	1146	40	6.4422	1.38	20.82	0.14	0.23
305	305	1146	41	6.4373	1.40	20.82	0.14	0.22
305	305	1146	42	6.4396	1.42	20.82	0.14	0.23
305	305	1146	43	6.4381	1.43	20.82	0.14	0.22
305	305	1146	44	6.4349	1.45	20.83	0.13	0.22
305	305	1146	45	6.4393	1.47	20.82	0.14	0.23
305	305	1146	46	6.4363	1.48	20.82	0.14	0.22
305	305	1146	47	6.4352	1.50	20.82	0.14	0.22
305	305	1146	48	6.4338	1.52	20.83	0.13	0.22
305	305	1146	49	6.4337	1.53	20.83	0.13	0.22
305	305	1146	50	6.4314	1.55	20.83	0.13	0.21
305	305	1146	51	6.4319	1.57	20.83	0.13	0.21
305	305	1146	52	6.4306	1.58	20.83	0.13	0.21
305	305	1146	53	6.4283	1.60	20.83	0.13	0.21
305	305	1146	54	6.4248	1.62	20.84	0.12	0.20
305	305	1146	55	6.419	1.63	20.84	0.12	0.19
305	305	1146	56	6.4194	1.65	20.84	0.12	0.19
305	305	1146	57	6.4257	1.67	20.83	0.13	0.20
305	305	1146	58	6.4207	1.68	20.84	0.12	0.20
305	305	1146	59	6.4191	1.70	20.84	0.12	0.19
305	305	1147	0	6.4169	1.72	20.84	0.12	0.19
305	305	1147	1	6.4102	1.73	20.85	0.11	0.18
305	305	1147	2	6.4092	1.75	20.85	0.11	0.18
305	305	1147	3	6.4131	1.77	20.85	0.11	0.18

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-303-AS

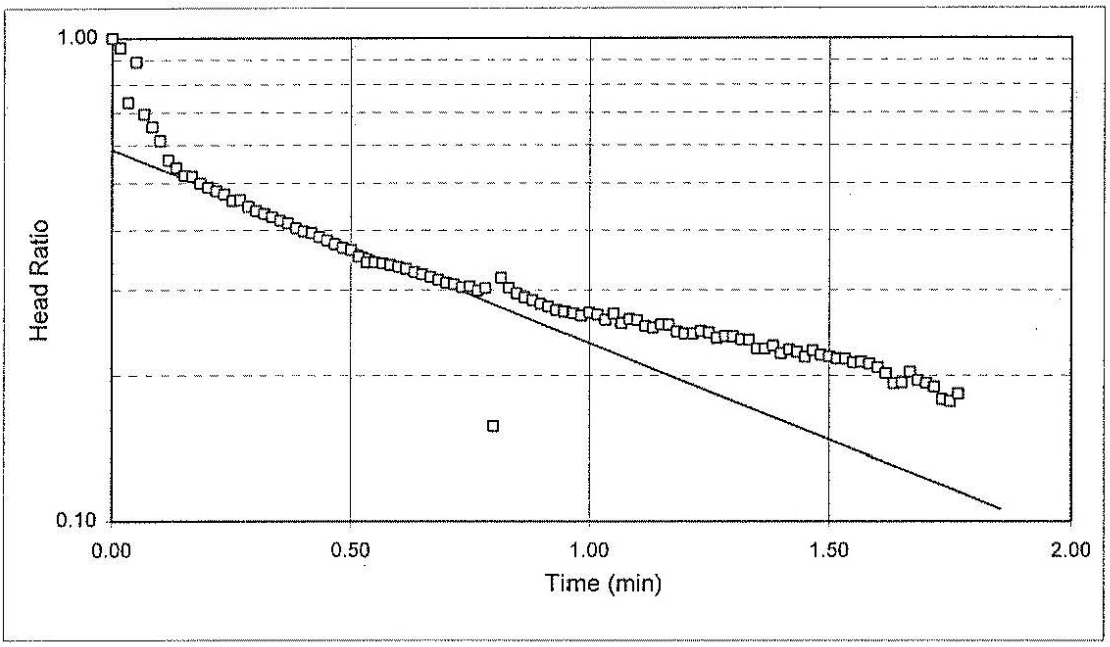
$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.43
L_e =	7.92
t_1 (min) =	0
t_2 (min) =	1.86
h_1/h_0 =	0.59
h_2/h_0 =	0.11

RESULTS

K=	6.00E-04	cm/sec
K=	1.70E+00	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/31/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

RISING HEAD TEST PZ-300-AS

WELL NO. PZ-300-AS

DATE	10/21/95	
INITAL HEAD ON TRANSDUCER	6.69	FEET H_2O
INITIAL DEPTH TO WATER	14.48	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	8.5	FEET (btoc)
BOTTOM OF OPEN INTERVAL	22.2	FEET (btoc)
SATURATED THICKNESS	30	FEET
WATER TABLE TO BOTTOM OF SCREEN	7.68	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	7.68	FEET
STATIC IN SCREEN?	Y	
MAX. HEAD CHANGE	0.95	FEET
MAX. HEAD IN SCREEN?	Y	

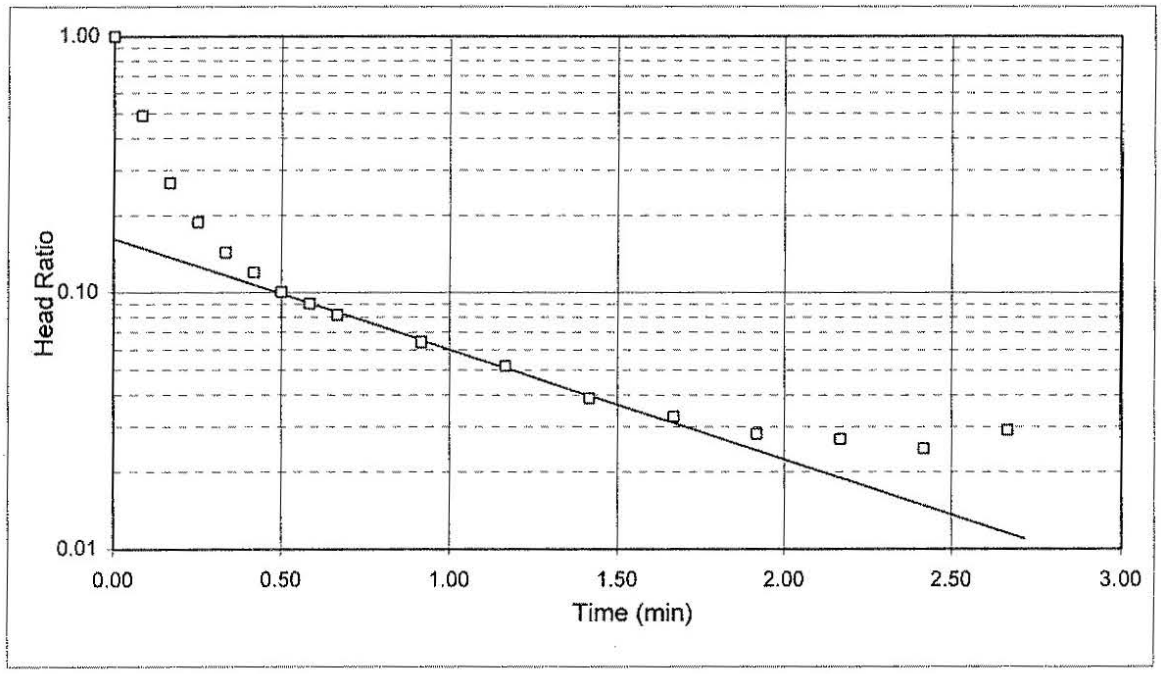
DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
307	295	1143	12	5.7409	0.00	15.43	0.95	1.00
307	295	1143	17	6.2245	0.08	14.95	0.47	0.49
307	295	1143	22	6.4359	0.17	14.73	0.25	0.27
307	295	1143	27	6.511	0.25	14.66	0.18	0.19
307	295	1143	32	6.5537	0.33	14.62	0.14	0.14
307	295	1143	37	6.576	0.42	14.59	0.11	0.12
307	295	1143	42	6.5945	0.50	14.58	0.10	0.10
307	295	1143	47	6.6042	0.58	14.57	0.09	0.09
307	295	1143	52	6.6124	0.67	14.56	0.08	0.08
307	295	1144	7	6.6291	0.92	14.54	0.06	0.06
307	295	1144	22	6.6406	1.17	14.53	0.05	0.05
307	295	1144	37	6.6531	1.42	14.52	0.04	0.04
307	295	1144	52	6.6587	1.67	14.51	0.03	0.03
307	295	1145	7	6.6633	1.92	14.51	0.03	0.03
307	295	1145	22	6.6645	2.17	14.51	0.03	0.03
307	295	1145	37	6.6666	2.42	14.50	0.02	0.02
307	295	1145	52	6.6623	2.67	14.51	0.03	0.03

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-300-AS

$$K = \frac{r_c^{\,2}}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
R_e =	0.34			
L_e =	7.68	K=	7.07E-04	cm/sec
t_1 (min) =	0	K=	2.00E+00	ft/day
t_2 (min) =	2.72			
h_1/h_0 =	0.16			
h_2/h_0 =	0.01			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/21/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

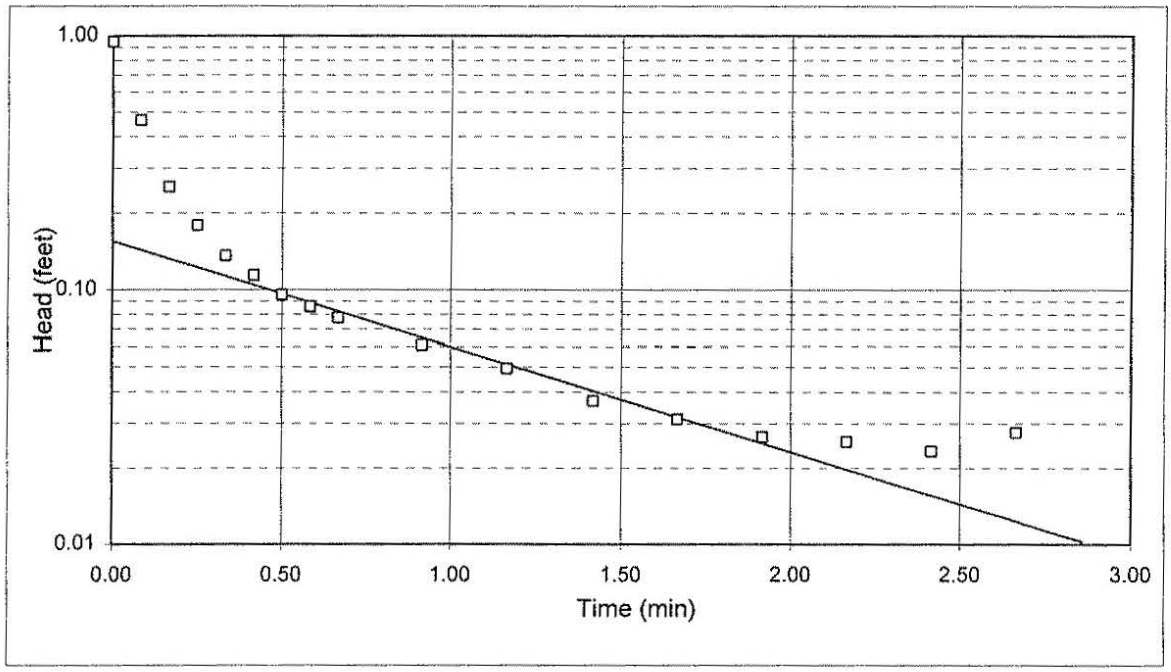
BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-300-AS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.20			
r_w =	0.34			
L_e =	7.68	K=	2.13E-03	cm/sec
$\ln(R_e/r_w)$	1.68	K=	6.04E+00	ft/day
y_0 =	0.15			
y_t =	0.01			
t =	2.86			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/21/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

FALLING HEAD TEST PZ-300-AD

WELL NO. PZ-300-AD

DATE	10/21/95	
INITAL HEAD ON TRANSDUCER	9.93	FEET H_2O
INITIAL DEPTH TO WATER	16.55	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	35.1	FEET (btoc)
BOTTOM OF OPEN INTERVAL	43.7	FEET (btoc)
SATURATED THICKNESS	30	FEET
WATER TABLE TO BOTTOM OF SCREEN	27.17	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	8.62	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	2.55	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	295	841	48	12.475	0.00	14.01	2.55	1.00
305	295	841	50	12.417	0.03	14.06	2.49	0.98
305	295	841	52	12.363	0.07	14.12	2.43	0.96
305	295	841	54	12.317	0.10	14.16	2.39	0.94
305	295	841	56	12.27	0.13	14.21	2.34	0.92
305	295	841	58	12.221	0.17	14.26	2.29	0.90
305	295	842	0	12.176	0.20	14.30	2.25	0.88
305	295	842	2	12.133	0.23	14.35	2.20	0.87
305	295	842	4	12.09	0.27	14.39	2.16	0.85
305	295	842	6	12.047	0.30	14.43	2.12	0.83
305	295	842	8	12.005	0.33	14.48	2.08	0.82
305	295	842	10	11.969	0.37	14.51	2.04	0.80
305	295	842	12	11.926	0.40	14.55	2.00	0.78
305	295	842	14	11.888	0.43	14.59	1.96	0.77
305	295	842	16	11.855	0.47	14.63	1.93	0.76
305	295	842	18	11.816	0.50	14.66	1.89	0.74
305	295	842	20	11.785	0.53	14.70	1.86	0.73
305	295	842	22	11.745	0.57	14.74	1.82	0.71
305	295	842	24	11.712	0.60	14.77	1.78	0.70
305	295	842	26	11.683	0.63	14.80	1.75	0.69
305	295	842	28	11.65	0.67	14.83	1.72	0.68
305	295	842	30	11.62	0.70	14.86	1.69	0.66
305	295	842	32	11.592	0.73	14.89	1.66	0.65
305	295	842	34	11.563	0.77	14.92	1.63	0.64

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	295	842	36	11.532	0.80	14.95	1.60	0.63
305	295	842	38	11.502	0.83	14.98	1.57	0.62
305	295	842	40	11.477	0.87	15.00	1.55	0.61
305	295	842	42	11.447	0.90	15.03	1.52	0.60
305	295	842	44	11.422	0.93	15.06	1.49	0.59
305	295	842	46	11.396	0.97	15.08	1.47	0.58
305	295	842	48	11.366	1.00	15.11	1.44	0.56
305	295	842	50	11.344	1.03	15.14	1.41	0.56
305	295	842	52	11.318	1.07	15.16	1.39	0.55
305	295	842	54	11.29	1.10	15.19	1.36	0.53
305	295	842	56	11.264	1.13	15.22	1.33	0.52
305	295	842	58	11.241	1.17	15.24	1.31	0.52
305	295	843	0	11.22	1.20	15.26	1.29	0.51
305	295	843	2	11.195	1.23	15.29	1.27	0.50
305	295	843	4	11.174	1.27	15.31	1.24	0.49
305	295	843	6	11.152	1.30	15.33	1.22	0.48
305	295	843	20	11.004	1.53	15.48	1.07	0.42
305	295	843	30	10.912	1.70	15.57	0.98	0.39
305	295	843	40	10.822	1.87	15.66	0.89	0.35
305	295	843	50	10.746	2.03	15.73	0.82	0.32
305	295	844	0	10.672	2.20	15.81	0.74	0.29
305	295	844	10	10.608	2.37	15.87	0.68	0.27
305	295	844	20	10.55	2.53	15.93	0.62	0.24
305	295	844	30	10.496	2.70	15.98	0.57	0.22
305	295	844	40	10.439	2.87	16.04	0.51	0.20
305	295	844	50	10.394	3.03	16.09	0.46	0.18
305	295	845	0	10.354	3.20	16.13	0.42	0.17
305	295	845	10	10.314	3.37	16.17	0.38	0.15
305	295	845	20	10.277	3.53	16.20	0.35	0.14
305	295	845	30	10.251	3.70	16.23	0.32	0.13
305	295	845	40	10.212	3.87	16.27	0.28	0.11
305	295	845	50	10.192	4.03	16.29	0.26	0.10
305	295	846	0	10.167	4.20	16.31	0.24	0.09
305	295	846	10	10.145	4.37	16.34	0.22	0.08
305	295	846	20	10.123	4.53	16.36	0.19	0.08
305	295	846	30	10.104	4.70	16.38	0.17	0.07
305	295	846	40	10.089	4.87	16.39	0.16	0.06
305	295	846	50	10.071	5.03	16.41	0.14	0.06
305	295	847	0	10.058	5.20	16.42	0.13	0.05
305	295	847	10	10.045	5.37	16.44	0.11	0.05
305	295	847	20	10.031	5.53	16.45	0.10	0.04
305	295	847	30	10.021	5.70	16.46	0.09	0.04

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	295	847	40	10.011	5.87	16.47	0.08	0.03
305	295	847	50	10.004	6.03	16.48	0.07	0.03
305	295	848	0	9.994	6.20	16.49	0.06	0.03
305	295	848	10	9.9889	6.37	16.49	0.06	0.02
305	295	848	20	9.9813	6.53	16.50	0.05	0.02
305	295	848	30	9.9767	6.70	16.50	0.05	0.02
305	295	848	40	9.9688	6.87	16.51	0.04	0.02
305	295	848	50	9.9641	7.03	16.52	0.03	0.01
305	295	849	0	9.9593	7.20	16.52	0.03	0.01
305	295	849	10	9.9588	7.37	16.52	0.03	0.01
305	295	849	20	9.9523	7.53	16.53	0.02	0.01
305	295	849	30	9.9478	7.70	16.53	0.02	0.01
305	295	849	40	9.9475	7.87	16.53	0.02	0.01
305	295	849	50	9.9463	8.03	16.53	0.02	0.01
305	295	850	0	9.9377	8.20	16.54	0.01	0.00
305	295	850	30	9.933	8.70	16.55	0.00	0.00
305	295	850	44	9.9316	8.93	16.55	0.00	0.00
305	295	850	46	9.9311	8.97	16.55	0.00	0.00
305	295	850	48	9.931	9.00	16.55	0.00	0.00
305	295	850	50	9.9279	9.03	16.55	0.00	0.00
305	295	850	52	9.9295	9.07	16.55	0.00	0.00
305	295	850	54	9.9298	9.10	16.55	0.00	0.00
305	295	850	56	9.9297	9.13	16.55	0.00	0.00
305	295	850	58	9.929	9.17	16.55	0.00	0.00

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-300-AD

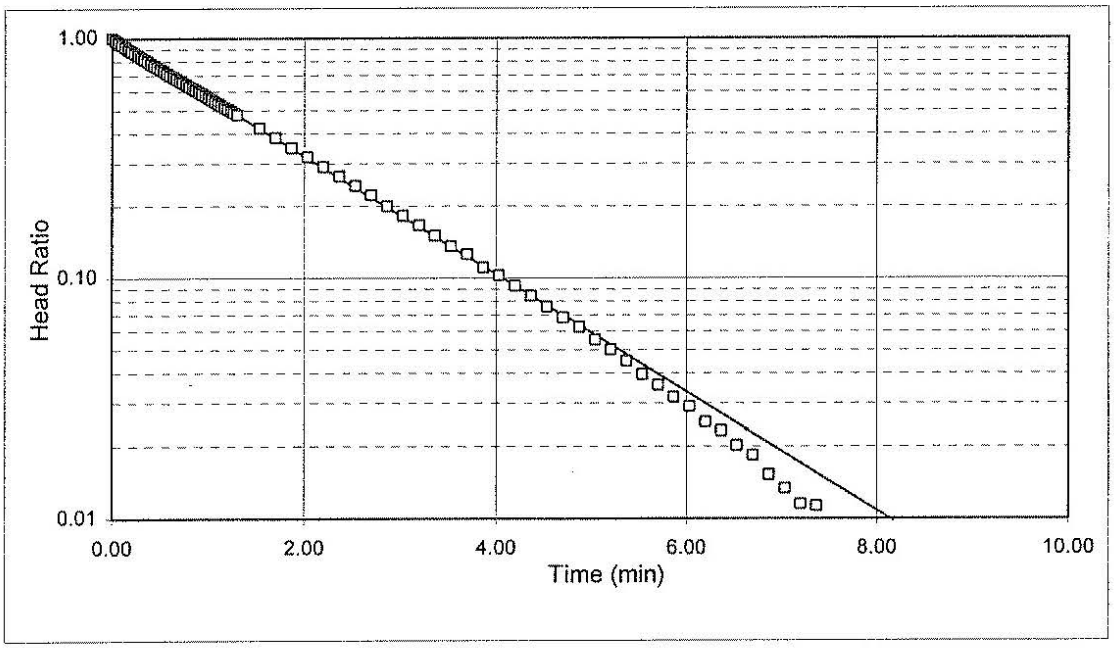
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.34
L_e =	8.62
t_1 (min) =	0
t_2 (min) =	8.18
h_1/h_0 =	1.00
h_2/h_0 =	0.01

RESULTS

K=	3.73E-04	cm/sec
K=	1.06E+00	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/21/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

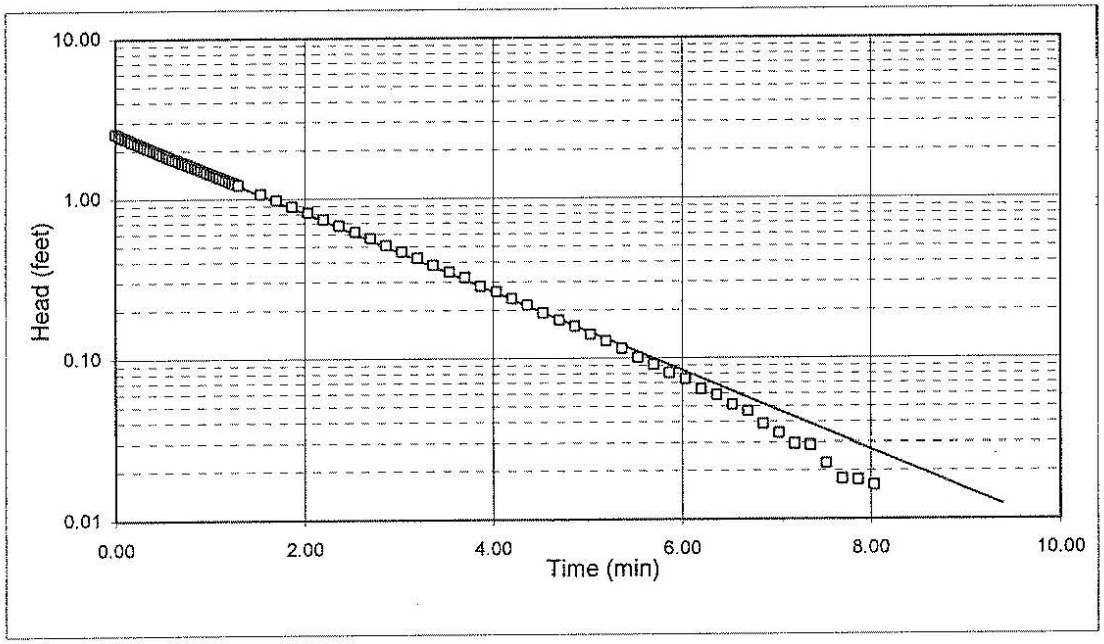
BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-300-AD

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
r_w =	0.34			
L_e =	8.62	K=	2.72E-04	cm/sec
$\ln(R_e/r_w)$	2.35	K=	7.72E-01	ft/day
y_0 =	2.51			
y_t =	0.01			
t =	9.40			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/21/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

RISING HEAD TEST PZ-300-AD

WELL NO. PZ-300-AD

DATE	10/21/95	
INITAL HEAD ON TRANSDUCER	9.93	FEET H_2O
INITIAL DEPTH TO WATER	16.55	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	35.1	FEET (btoc)
BOTTOM OF OPEN INTERVAL	43.7	FEET (btoc)
SATURATED THICKNESS	30	FEET
WATER TABLE TO BOTTOM OF SCREEN	27.15	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	8.6	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	3.13	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	295	851	2	6.8026	0.00	19.68	3.13	1.00
305	295	851	4	6.8462	0.03	19.63	3.08	0.99
305	295	851	6	6.9483	0.07	19.53	2.98	0.95
305	295	851	8	6.9944	0.10	19.49	2.94	0.94
305	295	851	10	7.0197	0.13	19.46	2.91	0.93
305	295	851	12	7.0565	0.17	19.42	2.87	0.92
305	295	851	14	7.0863	0.20	19.39	2.84	0.91
305	295	851	16	7.1148	0.23	19.37	2.82	0.90
305	295	851	18	7.1418	0.27	19.34	2.79	0.89
305	295	851	20	7.1667	0.30	19.31	2.76	0.88
305	295	851	22	7.1922	0.33	19.29	2.74	0.88
305	295	851	24	7.2145	0.37	19.27	2.72	0.87
305	295	851	26	7.2381	0.40	19.24	2.69	0.86
305	295	851	28	7.2621	0.43	19.22	2.67	0.85
305	295	851	30	7.2825	0.47	19.20	2.65	0.85
305	295	851	32	7.3067	0.50	19.17	2.62	0.84
305	295	851	34	7.3281	0.53	19.15	2.60	0.83
305	295	851	36	7.3481	0.57	19.13	2.58	0.83
305	295	851	38	7.3735	0.60	19.11	2.56	0.82
305	295	851	40	7.3843	0.63	19.10	2.55	0.81
305	295	851	42	7.4092	0.67	19.07	2.52	0.81
305	295	851	44	7.427	0.70	19.05	2.50	0.80
305	295	851	46	7.4521	0.73	19.03	2.48	0.79
305	295	851	48	7.4716	0.77	19.01	2.46	0.79
305	295	851	50	7.4888	0.80	18.99	2.44	0.78
305	295	851	52	7.5094	0.83	18.97	2.42	0.77
305	295	851	54	7.5276	0.87	18.95	2.40	0.77
305	295	851	56	7.5449	0.90	18.94	2.39	0.76
305	295	851	58	7.5651	0.93	18.91	2.36	0.76
305	295	852	0	7.5779	0.97	18.90	2.35	0.75

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	295	852	2	7.5964	1.00	18.88	2.33	0.75
305	295	852	4	7.6172	1.03	18.86	2.31	0.74
305	295	852	6	7.634	1.07	18.85	2.30	0.73
305	295	852	8	7.6503	1.10	18.83	2.28	0.73
305	295	852	10	7.6672	1.13	18.81	2.26	0.72
305	295	852	12	7.6855	1.17	18.79	2.24	0.72
305	295	852	14	7.702	1.20	18.78	2.23	0.71
305	295	852	16	7.7187	1.23	18.76	2.21	0.71
305	295	852	18	7.7351	1.27	18.74	2.19	0.70
305	295	852	20	7.7513	1.30	18.73	2.18	0.70
305	295	852	22	7.7683	1.33	18.71	2.16	0.69
305	295	852	24	7.7829	1.37	18.70	2.15	0.69
305	295	852	26	7.7991	1.40	18.68	2.13	0.68
305	295	852	28	7.8145	1.43	18.67	2.12	0.68
305	295	852	30	7.8298	1.47	18.65	2.10	0.67
305	295	852	32	7.8455	1.50	18.63	2.08	0.67
305	295	852	34	7.8606	1.53	18.62	2.07	0.66
305	295	852	36	7.8794	1.57	18.60	2.05	0.66
305	295	852	38	7.8948	1.60	18.59	2.04	0.65
305	295	852	40	7.9108	1.63	18.57	2.02	0.65
305	295	852	42	7.9243	1.67	18.56	2.01	0.64
305	295	852	44	7.9407	1.70	18.54	1.99	0.64
305	295	852	46	7.9525	1.73	18.53	1.98	0.63
305	295	852	48	7.9703	1.77	18.51	1.96	0.63
305	295	852	50	7.9841	1.80	18.50	1.95	0.62
305	295	852	52	7.9973	1.83	18.48	1.93	0.62
305	295	852	54	8.0127	1.87	18.47	1.92	0.61
305	295	852	56	8.0307	1.90	18.45	1.90	0.61
305	295	852	58	8.044	1.93	18.44	1.89	0.60
305	295	853	0	8.052	1.97	18.43	1.88	0.60
305	295	853	2	8.0681	2.00	18.41	1.86	0.60
305	295	853	10	8.1272	2.13	18.35	1.80	0.58
305	295	853	20	8.1926	2.30	18.29	1.74	0.56
305	295	853	30	8.2542	2.47	18.23	1.68	0.54
305	295	853	40	8.3159	2.63	18.16	1.61	0.52
305	295	853	50	8.3751	2.80	18.10	1.55	0.50
305	295	854	0	8.4301	2.97	18.05	1.50	0.48
305	295	854	10	8.4846	3.13	18.00	1.45	0.46
305	295	854	20	8.5435	3.30	17.94	1.39	0.44
305	295	854	30	8.5945	3.47	17.89	1.34	0.43
305	295	854	40	8.6398	3.63	17.84	1.29	0.41
305	295	854	50	8.6851	3.80	17.79	1.24	0.40
305	295	855	0	8.7309	3.97	17.75	1.20	0.38
305	295	855	10	8.7786	4.13	17.70	1.15	0.37
305	295	855	20	8.8196	4.30	17.66	1.11	0.36
305	295	855	30	8.8617	4.47	17.62	1.07	0.34
305	295	855	40	8.9019	4.63	17.58	1.03	0.33
305	295	855	50	8.9404	4.80	17.54	0.99	0.32

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	295	856	0	8.9782	4.97	17.50	0.95	0.30
305	295	856	10	9.0138	5.13	17.47	0.92	0.29
305	295	856	20	9.0454	5.30	17.43	0.88	0.28
305	295	856	30	9.0792	5.47	17.40	0.85	0.27
305	295	856	40	9.1093	5.63	17.37	0.82	0.26
305	295	856	50	9.1488	5.80	17.33	0.78	0.25
305	295	857	0	9.1761	5.97	17.30	0.75	0.24
305	295	857	10	9.2054	6.13	17.27	0.72	0.23
305	295	857	20	9.2345	6.30	17.25	0.70	0.22
305	295	857	30	9.2554	6.47	17.22	0.67	0.22
305	295	857	40	9.2843	6.63	17.20	0.65	0.21
305	295	857	50	9.3116	6.80	17.17	0.62	0.20
305	295	858	0	9.3325	6.97	17.15	0.60	0.19
305	295	858	10	9.3577	7.13	17.12	0.57	0.18
305	295	858	20	9.3798	7.30	17.10	0.55	0.18
305	295	858	30	9.4009	7.47	17.08	0.53	0.17
305	295	858	40	9.4203	7.63	17.06	0.51	0.16
305	295	858	50	9.4399	7.80	17.04	0.49	0.16
305	295	859	0	9.459	7.97	17.02	0.47	0.15
305	295	859	10	9.4773	8.13	17.00	0.45	0.14
305	295	859	20	9.4948	8.30	16.99	0.44	0.14
305	295	859	30	9.5117	8.47	16.97	0.42	0.13
305	295	859	40	9.5297	8.63	16.95	0.40	0.13
305	295	859	50	9.5437	8.80	16.94	0.39	0.12
305	295	900	0	9.5594	8.97	16.92	0.37	0.12
305	295	900	30	9.6053	9.47	16.87	0.32	0.10
305	295	901	0	9.644	9.97	16.84	0.29	0.09
305	295	901	30	9.6756	10.47	16.80	0.25	0.08
305	295	902	0	9.7028	10.97	16.78	0.23	0.07
305	295	902	30	9.7316	11.47	16.75	0.20	0.06
305	295	903	0	9.7594	11.97	16.72	0.17	0.05
305	295	903	30	9.7817	12.47	16.70	0.15	0.05
305	295	904	0	9.7995	12.97	16.68	0.13	0.04
305	295	904	30	9.8121	13.47	16.67	0.12	0.04
305	295	905	0	9.8268	13.97	16.65	0.10	0.03
305	295	905	30	9.8384	14.47	16.64	0.09	0.03
305	295	906	0	9.85	14.97	16.63	0.08	0.03
305	295	906	30	9.8624	15.47	16.62	0.07	0.02
305	295	907	0	9.8725	15.97	16.61	0.06	0.02
305	295	907	30	9.8824	16.47	16.60	0.05	0.02
305	295	908	0	9.8892	16.97	16.59	0.04	0.01
305	295	908	30	9.8959	17.47	16.58	0.03	0.01
305	295	909	0	9.8989	17.97	16.58	0.03	0.01
305	295	909	30	9.9022	18.47	16.58	0.03	0.01
305	295	910	0	9.9109	18.97	16.57	0.02	0.01
305	295	910	30	9.9113	19.47	16.57	0.02	0.01

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-300-AD

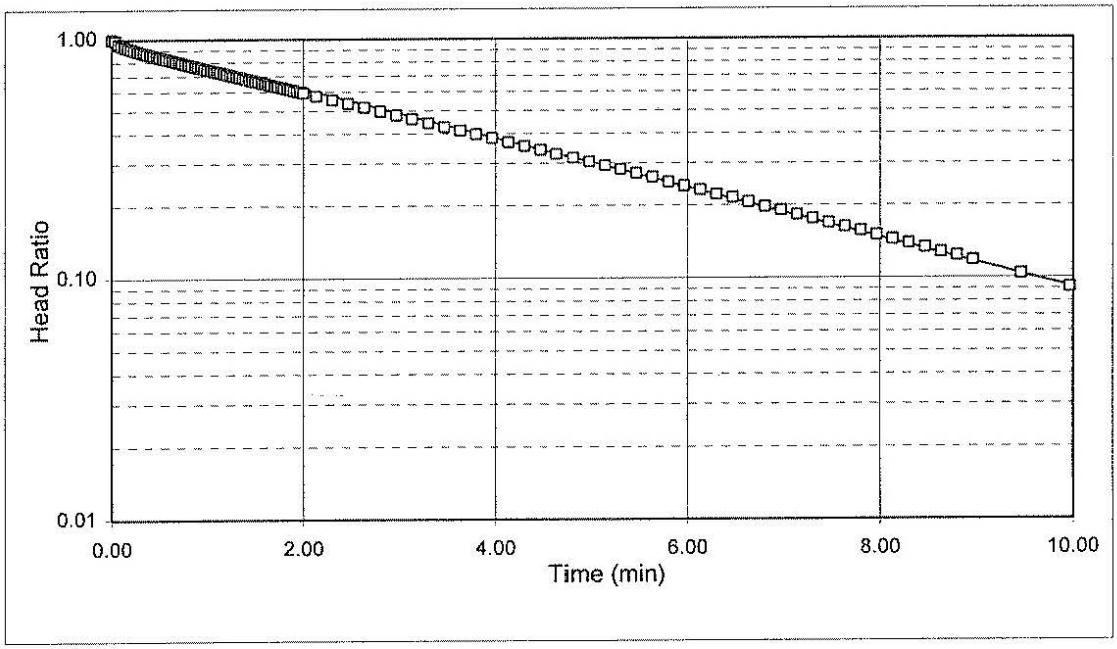
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.34
L_e =	8.6
t_1 (win) =	0
t_2 (win) =	10.00
h_1/h_0 =	1.00
h_2/h_0 =	0.09

RESULTS

K=	1.58E-04	cm/sec
K=	4.48E-01	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/21/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

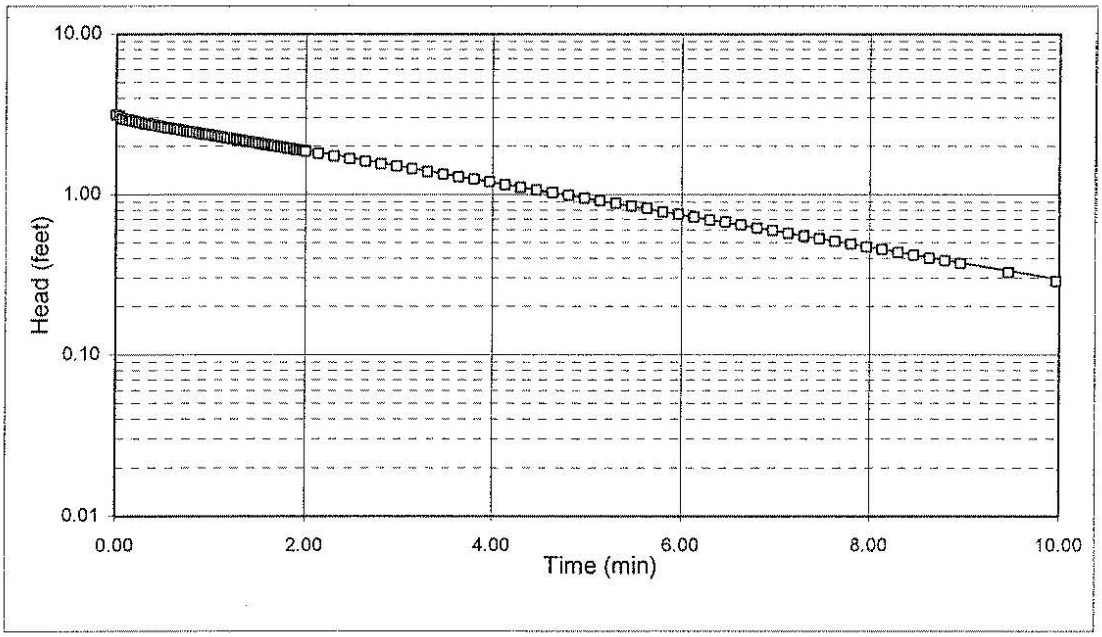
BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-300-AD

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS	
r_c =	0.08		
r_w =	0.34		
L_e =	8.6	K=	1.12E-04 cm/sec
$\ln(R_e/r_w)$	2.35	K=	3.18E-01 ft/day
y_0 =	3.02		
y_t =	0.30		
t =	10.00		



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/21/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

FALLING HEAD TEST PZ-300-SS

WELL NO. PZ-300-SS

DATE	10/21/95	
INITAL HEAD ON TRANSDUCER	9.81	FEET H_2O
INITIAL DEPTH TO WATER	21.1	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	81.7	FEET (btoc)
BOTTOM OF OPEN INTERVAL	95.7	FEET (btoc)
SATURATED THICKNESS	160	FEET
WATER TABLE TO BOTTOM OF SCREEN	74.6	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	14	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	4.22	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	295	1407	34	14.032	0.00	16.88	4.22	1.00
305	295	1407	36	13.028	0.03	17.88	3.22	0.76
305	295	1407	38	12.925	0.07	17.99	3.12	0.74
305	295	1407	40	12.913	0.10	18.00	3.10	0.73
305	295	1407	42	12.902	0.13	18.01	3.09	0.73
305	295	1407	44	12.891	0.17	18.02	3.08	0.73
305	295	1407	46	12.879	0.20	18.03	3.07	0.73
305	295	1407	48	12.868	0.23	18.04	3.06	0.72
305	295	1407	50	12.861	0.27	18.05	3.05	0.72
305	295	1407	52	12.849	0.30	18.06	3.04	0.72
305	295	1407	54	12.843	0.33	18.07	3.03	0.72
305	295	1407	56	12.833	0.37	18.08	3.02	0.72
305	295	1407	58	12.824	0.40	18.09	3.01	0.71
305	295	1408	0	12.816	0.43	18.09	3.01	0.71
305	295	1408	2	12.807	0.47	18.10	3.00	0.71
305	295	1408	4	12.799	0.50	18.11	2.99	0.71
305	295	1408	6	12.791	0.53	18.12	2.98	0.71
305	295	1408	8	12.783	0.57	18.13	2.97	0.70
305	295	1408	10	12.778	0.60	18.13	2.97	0.70
305	295	1408	12	12.767	0.63	18.14	2.96	0.70
305	295	1408	14	12.762	0.67	18.15	2.95	0.70
305	295	1408	16	12.753	0.70	18.16	2.94	0.70
305	295	1408	18	12.747	0.73	18.16	2.94	0.70
305	295	1408	20	12.739	0.77	18.17	2.93	0.69
305	295	1408	22	12.732	0.80	18.18	2.92	0.69
305	295	1408	24	12.727	0.83	18.18	2.92	0.69
305	295	1408	26	12.716	0.87	18.19	2.91	0.69
305	295	1408	28	12.714	0.90	18.20	2.90	0.69
305	295	1408	30	12.709	0.93	18.20	2.90	0.69
305	295	1408	32	12.702	0.97	18.21	2.89	0.68

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	295	1408	34	12.696	1.00	18.21	2.89	0.68
305	295	1408	36	12.69	1.03	18.22	2.88	0.68
305	295	1408	38	12.684	1.07	18.23	2.87	0.68
305	295	1408	40	12.677	1.10	18.23	2.87	0.68
305	295	1408	42	12.669	1.13	18.24	2.86	0.68
305	295	1408	44	12.663	1.17	18.25	2.85	0.68
305	295	1408	46	12.655	1.20	18.26	2.85	0.67
305	295	1408	48	12.649	1.23	18.26	2.84	0.67
305	295	1408	50	12.643	1.27	18.27	2.83	0.67
305	295	1408	52	12.637	1.30	18.27	2.83	0.67
305	295	1409	0	12.616	1.43	18.29	2.81	0.66
305	295	1409	10	12.598	1.60	18.31	2.79	0.66
305	295	1409	20	12.568	1.77	18.34	2.76	0.65
305	295	1409	30	12.544	1.93	18.37	2.73	0.65
305	295	1409	40	12.529	2.10	18.38	2.72	0.64
305	295	1409	50	12.521	2.27	18.39	2.71	0.64
305	295	1410	0	12.505	2.43	18.41	2.70	0.64
305	295	1410	10	12.495	2.60	18.42	2.69	0.64
305	295	1410	20	12.479	2.77	18.43	2.67	0.63
305	295	1410	30	12.47	2.93	18.44	2.66	0.63
305	295	1410	40	12.46	3.10	18.45	2.65	0.63
305	295	1410	50	12.456	3.27	18.45	2.65	0.63
305	295	1411	0	12.45	3.43	18.46	2.64	0.63
305	295	1412	0	12.425	4.43	18.49	2.62	0.62
305	295	1413	0	12.403	5.43	18.51	2.59	0.61
305	295	1414	0	12.38	6.43	18.53	2.57	0.61
305	295	1415	0	12.361	7.43	18.55	2.55	0.60
305	295	1416	0	12.338	8.43	18.57	2.53	0.60
305	295	1417	0	12.317	9.43	18.59	2.51	0.59
305	295	1418	0	12.296	10.43	18.61	2.49	0.59
305	295	1419	0	12.278	11.43	18.63	2.47	0.58
305	295	1420	0	12.261	12.43	18.65	2.45	0.58
305	295	1421	0	12.244	13.43	18.67	2.43	0.58
305	295	1422	0	12.228	14.43	18.68	2.42	0.57
305	295	1423	0	12.21	15.43	18.70	2.40	0.57
305	295	1424	0	12.197	16.43	18.71	2.39	0.57
305	295	1425	0	12.18	17.43	18.73	2.37	0.56
305	295	1426	0	12.169	18.43	18.74	2.36	0.56
305	295	1427	0	12.148	19.43	18.76	2.34	0.55
305	295	1430	0	12.109	22.43	18.80	2.30	0.54
305	295	1440	0	12	32.43	18.91	2.19	0.52
305	295	1450	0	11.907	42.43	19.00	2.10	0.50
305	295	1500	0	11.822	52.43	19.09	2.01	0.48
305	295	1510	0	11.746	62.43	19.16	1.94	0.46
305	295	1519	40	11.678	72.10	19.23	1.87	0.44
305	295	1519	50	11.682	72.27	19.23	1.87	0.44
305	295	1520	0	11.683	72.43	19.23	1.87	0.44
305	295	1520	10	11.68	72.60	19.23	1.87	0.44

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	295	1520	20	11.681	72.77	19.23	1.87	0.44
305	295	1520	30	11.68	72.93	19.23	1.87	0.44
305	295	1520	40	11.677	73.10	19.23	1.87	0.44
305	295	1520	50	11.679	73.27	19.23	1.87	0.44
305	295	1521	0	11.675	73.43	19.24	1.87	0.44
305	295	1521	10	11.67	73.60	19.24	1.86	0.44
305	295	1521	20	11.671	73.77	19.24	1.86	0.44
305	295	1521	30	11.67	73.93	19.24	1.86	0.44
305	295	1521	40	11.669	74.10	19.24	1.86	0.44
305	295	1521	50	11.672	74.27	19.24	1.86	0.44
305	295	1522	0	11.672	74.43	19.24	1.86	0.44
305	295	1522	10	11.67	74.60	19.24	1.86	0.44
305	295	1522	20	11.668	74.77	19.24	1.86	0.44
305	295	1522	30	11.667	74.93	19.24	1.86	0.44
305	295	1522	40	11.666	75.10	19.24	1.86	0.44
305	295	1522	50	11.666	75.27	19.24	1.86	0.44
305	295	1523	0	11.664	75.43	19.25	1.85	0.44
305	295	1523	10	11.662	75.60	19.25	1.85	0.44
305	295	1523	20	11.662	75.77	19.25	1.85	0.44
305	295	1523	30	11.66	75.93	19.25	1.85	0.44
305	295	1523	40	11.659	76.10	19.25	1.85	0.44
305	295	1523	50	11.658	76.27	19.25	1.85	0.44
305	295	1524	0	11.657	76.43	19.25	1.85	0.44
305	295	1524	10	11.656	76.60	19.25	1.85	0.44
305	295	1524	20	11.655	76.77	19.26	1.85	0.44
305	295	1524	30	11.653	76.93	19.26	1.84	0.44
305	295	1524	40	11.652	77.10	19.26	1.84	0.44
305	295	1524	50	11.65	77.27	19.26	1.84	0.44
305	295	1525	0	11.65	77.43	19.26	1.84	0.44
305	295	1525	10	11.649	77.60	19.26	1.84	0.44
305	295	1525	20	11.647	77.77	19.26	1.84	0.44
305	295	1525	30	11.646	77.93	19.26	1.84	0.43
305	295	1525	40	11.645	78.10	19.27	1.84	0.43
305	295	1525	50	11.644	78.27	19.27	1.83	0.43
305	295	1526	0	11.644	78.43	19.27	1.83	0.43
305	295	1526	10	11.641	78.60	19.27	1.83	0.43
305	295	1526	20	11.64	78.77	19.27	1.83	0.43
305	295	1526	30	11.639	78.93	19.27	1.83	0.43
305	295	1526	40	11.637	79.10	19.27	1.83	0.43
305	295	1526	50	11.636	79.27	19.27	1.83	0.43
305	295	1527	0	11.636	79.43	19.27	1.83	0.43
305	295	1527	10	11.636	79.60	19.27	1.83	0.43
305	295	1527	20	11.637	79.77	19.27	1.83	0.43
305	295	1527	30	11.633	79.93	19.28	1.82	0.43
305	295	1527	40	11.631	80.10	19.28	1.82	0.43
305	295	1527	50	11.632	80.27	19.28	1.82	0.43
305	295	1528	0	11.631	80.43	19.28	1.82	0.43
305	295	1528	10	11.629	80.60	19.28	1.82	0.43

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	295	1528	20	11.625	80.77	19.29	1.82	0.43
305	295	1528	30	11.628	80.93	19.28	1.82	0.43
305	295	1528	40	11.624	81.10	19.29	1.81	0.43
305	295	1528	50	11.624	81.27	19.29	1.81	0.43
305	295	1529	0	11.624	81.43	19.29	1.81	0.43
305	295	1529	10	11.622	81.60	19.29	1.81	0.43
305	295	1529	20	11.621	81.77	19.29	1.81	0.43
305	295	1529	30	11.621	81.93	19.29	1.81	0.43
305	295	1529	40	11.619	82.10	19.29	1.81	0.43
305	295	1529	50	11.616	82.27	19.29	1.81	0.43
305	295	1530	0	11.617	82.43	19.29	1.81	0.43
305	295	1530	10	11.616	82.60	19.29	1.81	0.43
305	295	1530	20	11.616	82.77	19.29	1.81	0.43
305	295	1600	0	11.46	112.43	19.45	1.65	0.39
305	295	1630	0	11.345	142.43	19.57	1.54	0.36
305	295	1700	0	11.241	172.43	19.67	1.43	0.34
305	295	1730	0	11.146	202.43	19.76	1.34	0.32
305	295	1800	0	11.077	232.43	19.83	1.27	0.30
305	295	1900	0	10.951	292.43	19.96	1.14	0.27
305	295	2000	0	10.832	352.43	20.08	1.02	0.24
305	295	2100	0	10.734	412.43	20.18	0.92	0.22
305	295	2200	0	10.637	472.43	20.27	0.83	0.20
305	295	2300	0	10.557	532.43	20.35	0.75	0.18
305	296	0	0	10.475	592.43	20.44	0.66	0.16
305	296	100	0	10.403	652.43	20.51	0.59	0.14
305	296	200	0	10.361	712.43	20.55	0.55	0.13
305	296	300	0	10.316	772.43	20.59	0.51	0.12
305	296	400	0	10.279	832.43	20.63	0.47	0.11
305	296	500	0	10.258	892.43	20.65	0.45	0.11
305	296	600	0	10.213	952.43	20.70	0.40	0.10
305	296	700	0	10.188	1012.43	20.72	0.38	0.09
305	296	800	0	10.21	1072.43	20.70	0.40	0.09

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-300-SS

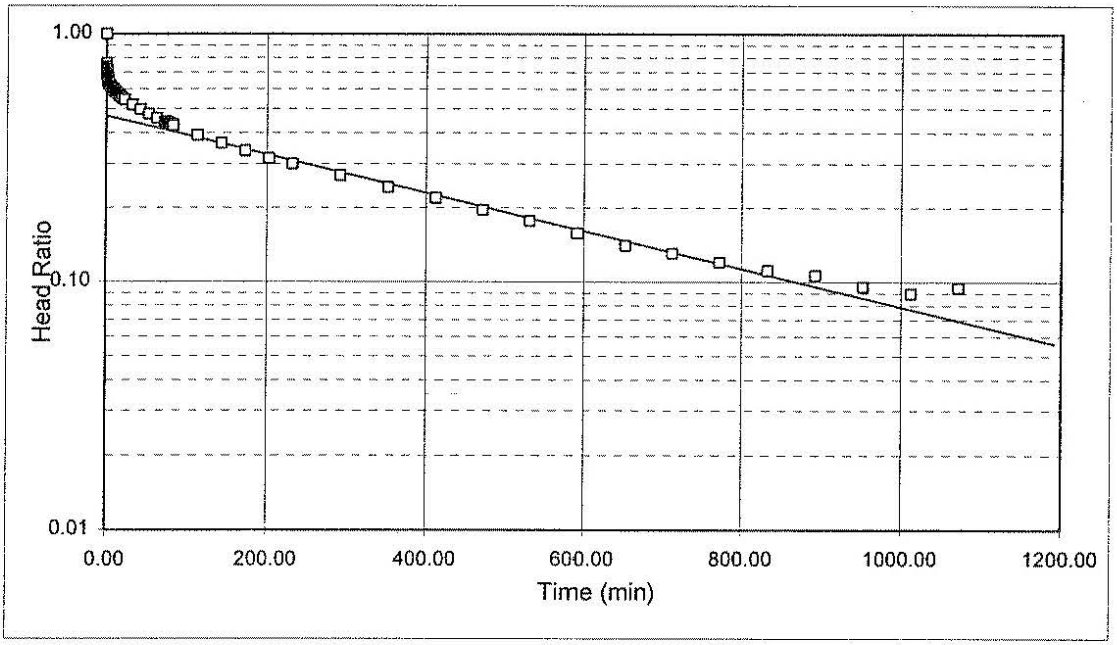
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	14
t_1 (min) =	0
t_2 (min) =	1192.00
h_1/h_0 =	0.47
h_2/h_0 =	0.06

RESULTS

K=	9.01E-07	cm/sec
K=	2.55E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/21/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-300-SS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

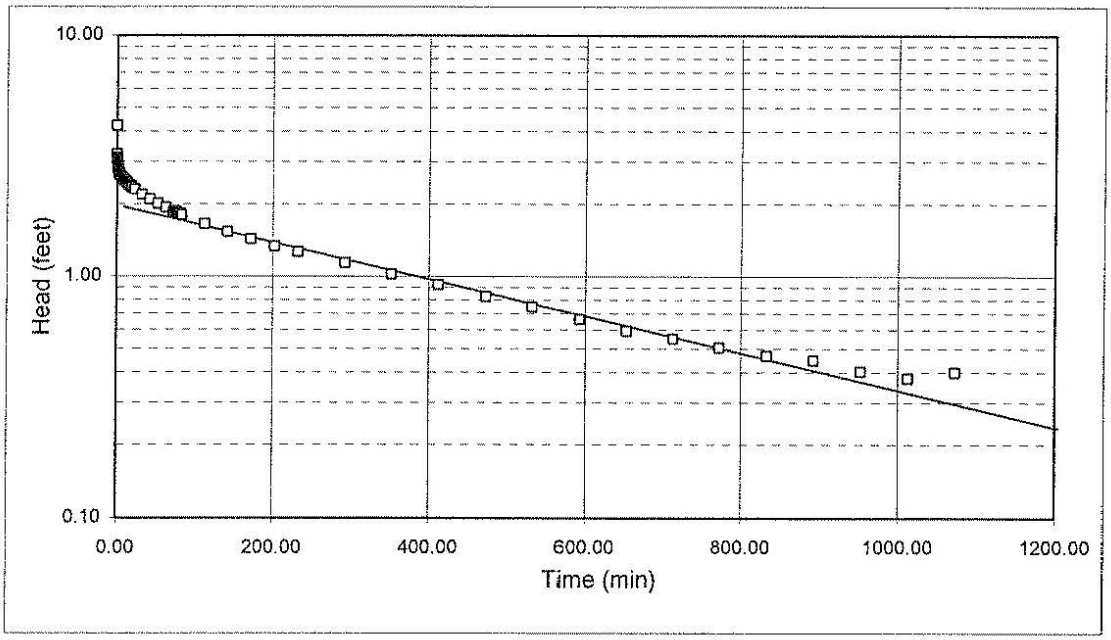
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.25
L_e =	14
$\ln(R_e/r_w)$	3.48
y_0 =	1.96
y_t =	0.23
t =	1204.00

RESULTS

K=	7.73E-07	cm/sec
K=	2.19E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/21/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

RISING HEAD TEST PZ-301-SS

WELL NO. PZ-301-SS

DATE	10/21/95	
INITAL HEAD ON TRANSDUCER	na	FEET H_2O
INITIAL DEPTH TO WATER	157.56	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	6	INCHES
TOP OF OPEN INTERVAL	148.1	FEET (btoc)
BOTTOM OF OPEN INTERVAL	163.1	FEET (btoc)
SATURATED THICKNESS	100	FEET
WATER TABLE TO BOTTOM OF SCREEN	5.54	FEET
EQUIVALENT DIAMETER	3.69	INCHES
OPEN INTERVAL LENGTH	5.54	FEET
STATIC IN SCREEN?	Y	
MAX. HEAD CHANGE	2.11	FEET
MAX. HEAD IN SCREEN?	Y	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	295	1444	0	159.67	0.00	159.67	2.11	1.00
305	295	1444	30	159.16	0.50	159.16	1.60	0.76
305	295	1445	0	159.08	1.00	159.08	1.52	0.72
305	295	1445	30	158.98	1.50	158.98	1.42	0.67
305	295	1446	0	158.93	2.00	158.93	1.37	0.65
305	295	1446	30	158.9	2.50	158.9	1.34	0.64
305	295	1447	0	158.88	3.00	158.88	1.32	0.63
305	295	1447	30	158.84	3.50	158.84	1.28	0.61
305	295	1448	0	158.84	4.00	158.84	1.28	0.61
305	295	1448	30	158.82	4.50	158.82	1.26	0.60
305	295	1449	0	158.8	5.00	158.8	1.24	0.59
305	295	1449	30	158.79	5.50	158.79	1.23	0.58
305	295	1450	0	158.78	6.00	158.78	1.22	0.58
305	295	1451	0	158.78	7.00	158.78	1.22	0.58
305	295	1452	0	158.74	8.00	158.74	1.18	0.56
305	295	1453	0	158.73	9.00	158.73	1.17	0.55
305	295	1454	0	158.71	10.00	158.71	1.15	0.55
305	295	1455	0	158.7	11.00	158.7	1.14	0.54
305	295	1500	0	158.68	16.00	158.68	1.12	0.53
305	295	1552	0	158.56	68.00	158.56	1.00	0.47
305	295	1643	0	158.54	119.00	158.54	0.98	0.46
305	295	1744	0	158.51	180.00	158.51	0.95	0.45
305	295	2023	0	158.46	339.00	158.46	0.90	0.43
305	296	705	0	158.04	981.00	158.04	0.48	0.23

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-301-SS

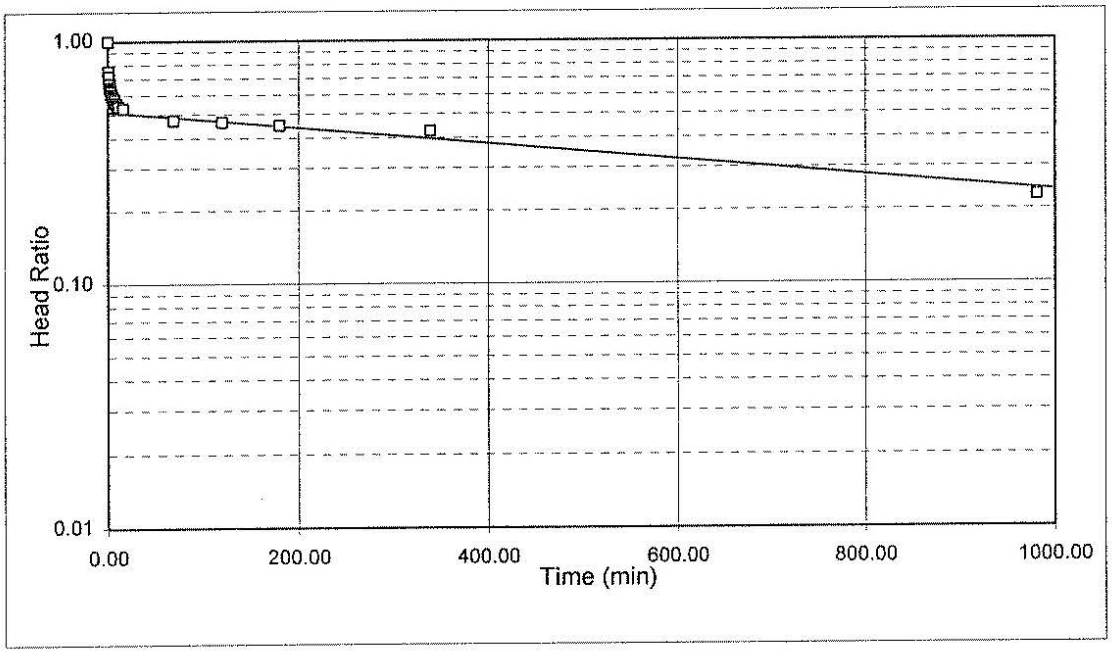
$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.25
L_e =	5.54
t_1 (min) =	0
t_2 (min) =	997.00
h_1/h_0 =	0.51
h_2/h_0 =	0.24

RESULTS

K=	7.52E-07	cm/sec
K=	2.13E-03	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/21/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

FALLING HEAD TEST PZ-302-AS

WELL NO. PZ-302-AS

DATE	10/24/95	
INITAL HEAD ON TRANSDUCER	5.25	FEET H_2O
INITIAL DEPTH TO WATER	18.97	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	10.9	FEET (btoc)
BOTTOM OF OPEN INTERVAL	24.2	FEET (btoc)
SATURATED THICKNESS	90	FEET
WATER TABLE TO BOTTOM OF SCREEN	5.25	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	5.25	FEET
STATIC IN SCREEN?	Y	
MAX. HEAD CHANGE	0.89	FEET
MAX. HEAD IN SCREEN?	Y	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	298	1301	14	6.1448	0.00	18.08	0.89	1.00
305	298	1301	16	6.0465	0.03	18.17	0.80	0.89
305	298	1301	18	6.0451	0.07	18.17	0.80	0.89
305	298	1301	20	6.0416	0.10	18.18	0.79	0.88
305	298	1301	22	6.0347	0.13	18.19	0.78	0.88
305	298	1301	24	6.032	0.17	18.19	0.78	0.87
305	298	1301	26	6.032	0.20	18.19	0.78	0.87
305	298	1301	28	6.028	0.23	18.19	0.78	0.87
305	298	1301	30	6.0219	0.27	18.20	0.77	0.86
305	298	1301	32	6.0193	0.30	18.20	0.77	0.86
305	298	1301	34	6.0163	0.33	18.20	0.77	0.86
305	298	1301	36	6.0116	0.37	18.21	0.76	0.85
305	298	1301	38	6.0074	0.40	18.21	0.76	0.85
305	298	1301	40	6.0035	0.43	18.22	0.75	0.84
305	298	1301	42	5.9986	0.47	18.22	0.75	0.84
305	298	1301	44	5.9934	0.50	18.23	0.74	0.83
305	298	1301	46	5.9895	0.53	18.23	0.74	0.83
305	298	1301	48	5.9852	0.57	18.23	0.74	0.82
305	298	1301	50	5.9795	0.60	18.24	0.73	0.82
305	298	1301	52	5.9767	0.63	18.24	0.73	0.81
305	298	1301	54	5.972	0.67	18.25	0.72	0.81
305	298	1302	0	5.9613	0.77	18.26	0.71	0.79
305	298	1302	10	5.9406	0.93	18.28	0.69	0.77
305	298	1302	20	5.9185	1.10	18.30	0.67	0.75

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	298	1302	30	5.9028	1.27	18.32	0.65	0.73
305	298	1302	40	5.8839	1.43	18.34	0.63	0.71
305	298	1302	50	5.8677	1.60	18.35	0.62	0.69
305	298	1303	0	5.8535	1.77	18.37	0.60	0.67
305	298	1303	10	5.8368	1.93	18.38	0.59	0.66
305	298	1303	20	5.8208	2.10	18.40	0.57	0.64
305	298	1303	30	5.8092	2.27	18.41	0.56	0.62
305	298	1303	40	5.7968	2.43	18.42	0.55	0.61
305	298	1303	50	5.7858	2.60	18.43	0.54	0.60
305	298	1304	30	5.7469	3.27	18.47	0.50	0.56
305	298	1305	0	5.7202	3.77	18.50	0.47	0.53
305	298	1305	30	5.6898	4.27	18.53	0.44	0.49
305	298	1306	0	5.6727	4.77	18.55	0.42	0.47
305	298	1306	30	5.645	5.27	18.58	0.40	0.44
305	298	1307	0	5.6225	5.77	18.60	0.37	0.42
305	298	1307	30	5.6014	6.27	18.62	0.35	0.39
305	298	1308	0	5.5873	6.77	18.63	0.34	0.38
305	298	1308	30	5.5613	7.27	18.66	0.31	0.35
305	298	1309	0	5.541	7.77	18.68	0.29	0.33
305	298	1309	30	5.5296	8.27	18.69	0.28	0.31
305	298	1310	0	5.5112	8.77	18.71	0.26	0.29
305	298	1310	30	5.4965	9.27	18.72	0.25	0.28
305	298	1311	0	5.4883	9.77	18.73	0.24	0.27
305	298	1311	30	5.4754	10.27	18.74	0.23	0.25
305	298	1312	0	5.4562	10.77	18.76	0.21	0.23
305	298	1312	30	5.4405	11.27	18.78	0.19	0.21
305	298	1313	0	5.4343	11.77	18.79	0.18	0.21
305	298	1315	0	5.4005	13.77	18.82	0.15	0.17
305	298	1320	0	5.3411	18.77	18.88	0.09	0.10

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-302-AS

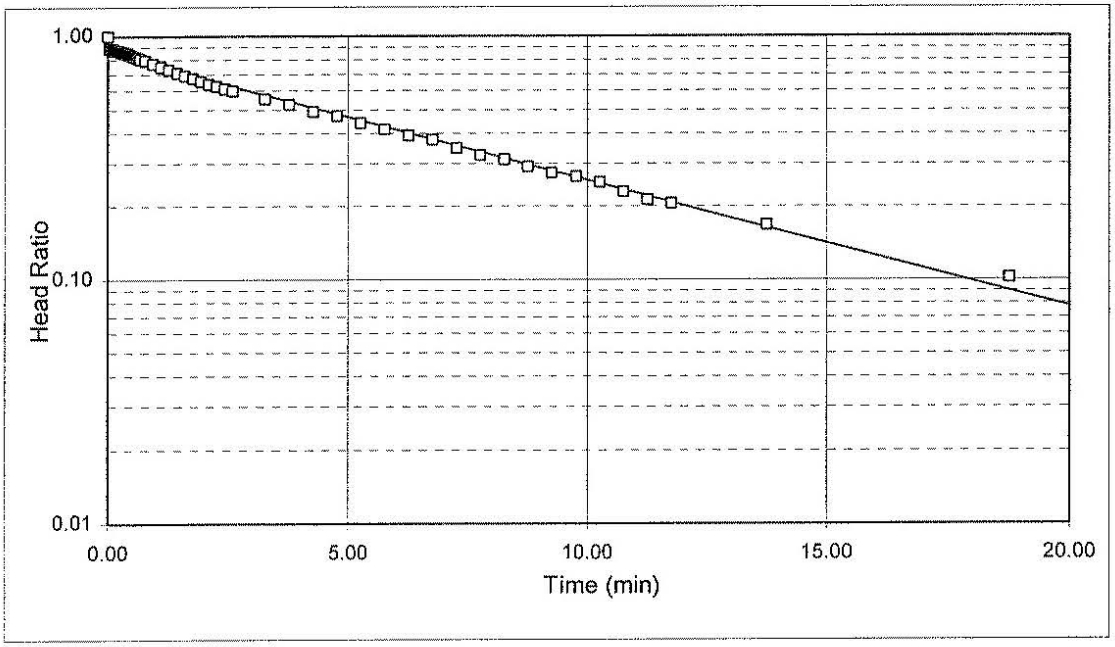
$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.34
L_e =	5.25
t_1 (min) =	0
t_2 (min) =	20.00
h_1/h_0 =	0.85
h_2/h_0 =	0.08

RESULTS

K=	1.10E-04	cm/sec
K=	3.11E-01	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/24/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

RISING HEAD TEST PZ-302-AS

WELL NO. PZ-302-AS

DATE	10/24/95	
INITAL HEAD ON TRANSDUCER	5.25	FEET H_2O
INITIAL DEPTH TO WATER	18.97	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	10.9	FEET (btoc)
BOTTOM OF OPEN INTERVAL	24.2	FEET (btoc)
SATURATED THICKNESS	90	FEET
WATER TABLE TO BOTTOM OF SCREEN	5.25	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	5.25	FEET
STATIC IN SCREEN?	Y	
MAX. HEAD CHANGE	1.98	FEET
MAX. HEAD IN SCREEN?	Y	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	298	1321	2	3.2668	0.00	20.95	1.98	1.00
305	298	1321	4	3.3596	0.03	20.86	1.89	0.95
305	298	1321	6	3.4169	0.07	20.80	1.83	0.92
305	298	1321	8	3.4495	0.10	20.77	1.80	0.91
305	298	1321	10	3.4796	0.13	20.74	1.77	0.89
305	298	1321	12	3.5151	0.17	20.70	1.73	0.87
305	298	1321	14	3.5516	0.20	20.67	1.70	0.86
305	298	1321	16	3.5814	0.23	20.64	1.67	0.84
305	298	1321	18	3.6061	0.27	20.61	1.64	0.83
305	298	1321	20	3.637	0.30	20.58	1.61	0.81
305	298	1321	22	3.6609	0.33	20.56	1.59	0.80
305	298	1321	24	3.6831	0.37	20.54	1.57	0.79
305	298	1321	26	3.7066	0.40	20.51	1.54	0.78
305	298	1321	28	3.731	0.43	20.49	1.52	0.77
305	298	1321	30	3.7522	0.47	20.47	1.50	0.76
305	298	1321	32	3.7779	0.50	20.44	1.47	0.74
305	298	1321	34	3.7976	0.53	20.42	1.45	0.73
305	298	1321	36	3.8146	0.57	20.41	1.44	0.72
305	298	1321	38	3.8337	0.60	20.39	1.42	0.71
305	298	1321	40	3.851	0.63	20.37	1.40	0.71
305	298	1321	42	3.8669	0.67	20.35	1.38	0.70
305	298	1321	44	3.8807	0.70	20.34	1.37	0.69
305	298	1321	46	3.8964	0.73	20.32	1.35	0.68
305	298	1321	48	3.9103	0.77	20.31	1.34	0.68

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	298	1321	50	3.9252	0.80	20.29	1.32	0.67
305	298	1321	52	3.9371	0.83	20.28	1.31	0.66
305	298	1321	54	3.9497	0.87	20.27	1.30	0.66
305	298	1321	56	3.9632	0.90	20.26	1.29	0.65
305	298	1321	58	3.9799	0.93	20.24	1.27	0.64
305	298	1322	0	3.9929	0.97	20.23	1.26	0.63
305	298	1322	2	4.0024	1.00	20.22	1.25	0.63
305	298	1322	4	4.0122	1.03	20.21	1.24	0.62
305	298	1322	6	4.0211	1.07	20.20	1.23	0.62
305	298	1322	8	4.0303	1.10	20.19	1.22	0.62
305	298	1322	20	4.0851	1.30	20.13	1.16	0.59
305	298	1322	30	4.1325	1.47	20.09	1.12	0.56
305	298	1322	40	4.1745	1.63	20.05	1.08	0.54
305	298	1322	50	4.2057	1.80	20.01	1.04	0.53
305	298	1323	0	4.2387	1.97	19.98	1.01	0.51
305	298	1323	10	4.2652	2.13	19.95	0.98	0.50
305	298	1323	20	4.2926	2.30	19.93	0.96	0.48
305	298	1323	30	4.3195	2.47	19.90	0.93	0.47
305	298	1323	40	4.3498	2.63	19.87	0.90	0.45
305	298	1323	50	4.373	2.80	19.85	0.88	0.44
305	298	1324	0	4.3936	2.97	19.83	0.86	0.43
305	298	1324	10	4.4141	3.13	19.81	0.84	0.42
305	298	1325	0	4.5115	3.97	19.71	0.74	0.37
305	298	1326	0	4.6081	4.97	19.61	0.64	0.32
305	298	1327	0	4.6884	5.97	19.53	0.56	0.28
305	298	1328	0	4.7512	6.97	19.47	0.50	0.25
305	298	1329	0	4.814	7.97	19.41	0.44	0.22
305	298	1330	0	4.8557	8.97	19.36	0.39	0.20
305	298	1335	0	4.9976	13.97	19.22	0.25	0.13
305	298	1340	0	5.0548	18.97	19.17	0.20	0.10

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-302-AS

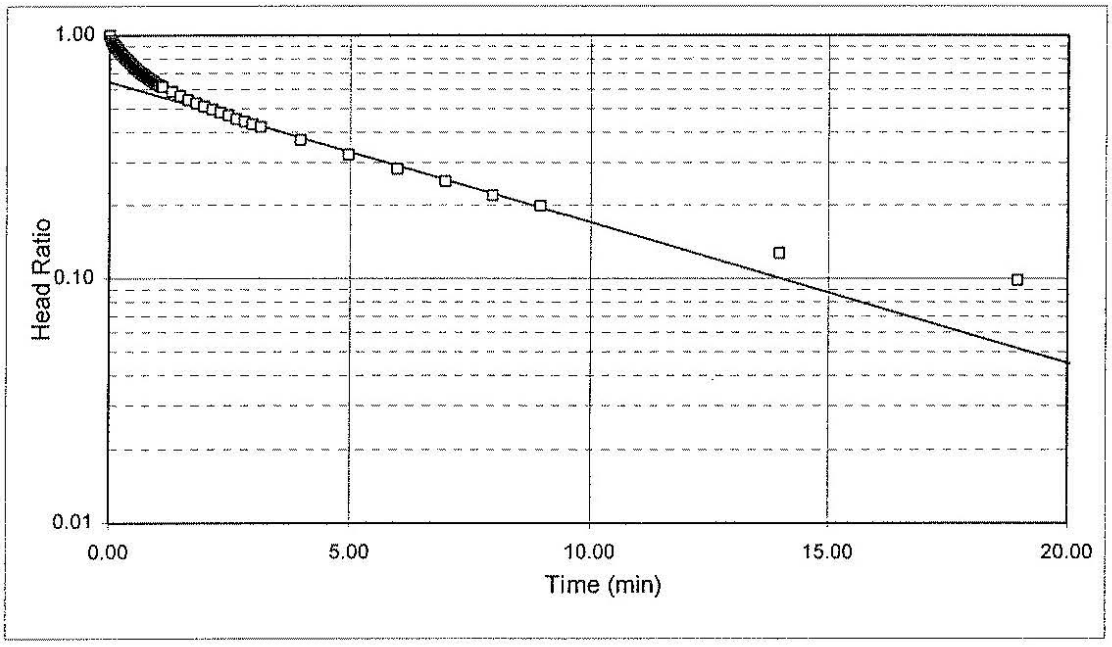
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.34
L_e =	5.25
t_1 (min) =	0
t_2 (min) =	20.06
h_1/h_0 =	0.65
h_2/h_0 =	0.04

RESULTS

K=	1.22E-04	cm/sec
K=	3.46E-01	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/24/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

FALLING HEAD TEST PZ-302-AI

WELL NO. PZ-302-AI

DATE	10/24/95	
INITAL HEAD ON TRANSDUCER	10.1	FEET H_2O
INITIAL DEPTH TO WATER	18.90	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	28.2	FEET (btoc)
BOTTOM OF OPEN INTERVAL	44.2	FEET (btoc)
SATURATED THICKNESS	90	FEET
WATER TABLE TO BOTTOM OF SCREEN	25.25	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	16	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	0.94	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	298	1108	58	11.035	0.00	17.97	0.94	1.00
305	298	1109	0	10.369	0.03	18.63	0.27	0.29
305	298	1109	2	10.203	0.07	18.80	0.10	0.11
305	298	1109	4	10.129	0.10	18.87	0.03	0.03
305	298	1109	6	10.107	0.13	18.89	0.01	0.01
305	298	1109	8	10.09	0.17	18.89	0.01	0.01

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-302-AI

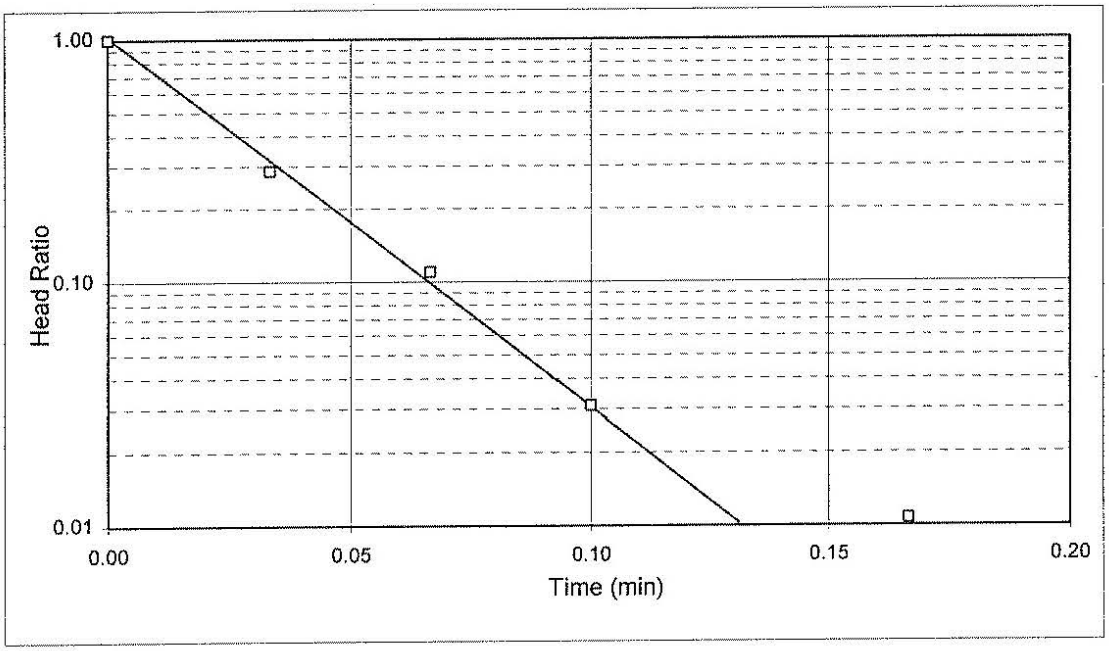
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.34
L_e =	16
t_1 (min) =	0
t_2 (min) =	0.13
h_1/h_0 =	1.02
h_2/h_0 =	0.01

RESULTS

K=	1.48E-02	cm/sec
K=	4.21E+01	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/24/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-302-AI

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

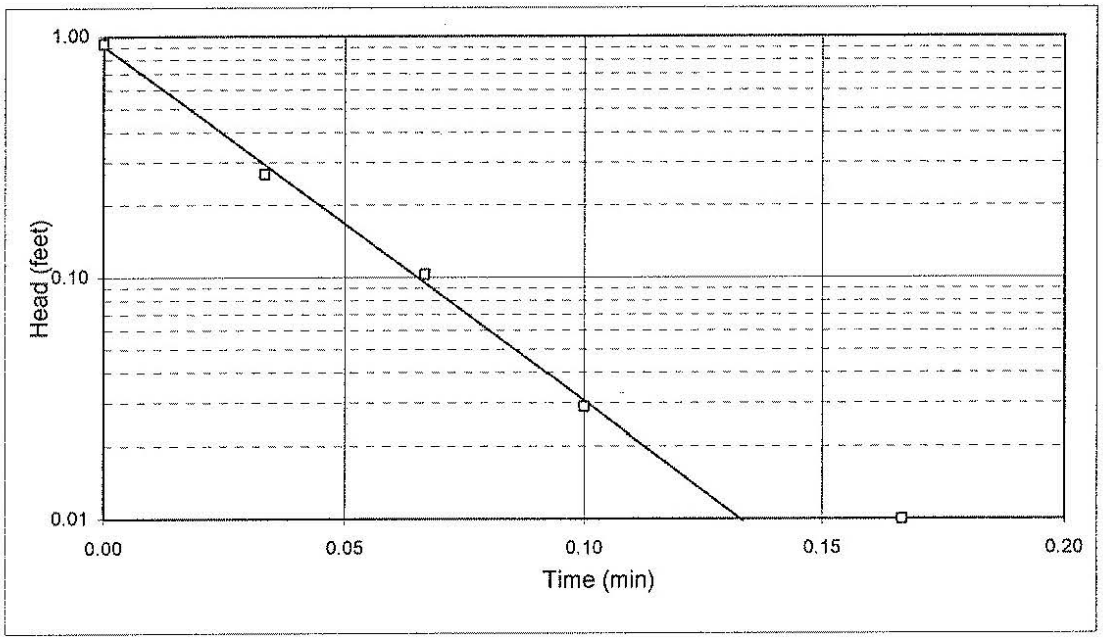
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.34
L_e =	16
$\ln(R_e/r_w)$	2.61
y_0 =	0.91
y_t =	0.01
t =	0.13

RESULTS

K=	9.78E-03	cm/sec
K=	2.77E+01	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/24/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

RISING HEAD TEST PZ-302-AI

WELL NO. PZ-302-AI

DATE	10/24/95	
INITAL HEAD ON TRANSDUCER	10.1	FEET H_2O
INITIAL DEPTH TO WATER	18.90	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	28.2	FEET (btoc)
BOTTOM OF OPEN INTERVAL	44.2	FEET (btoc)
SATURATED THICKNESS	90	FEET
WATER TABLE TO BOTTOM OF SCREEN	25.25	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	16	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	4.59	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	298	1111	28	5.5104	0.00	23.49	4.59	1.00
305	298	1111	30	9.1419	0.03	19.86	0.96	0.21
305	298	1111	32	9.8217	0.07	19.18	0.28	0.06
305	298	1111	34	10.013	0.10	18.99	0.09	0.02
305	298	1111	36	10.071	0.13	18.93	0.03	0.01
305	298	1111	38	10.088	0.17	18.91	0.01	0.00

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-302-AI

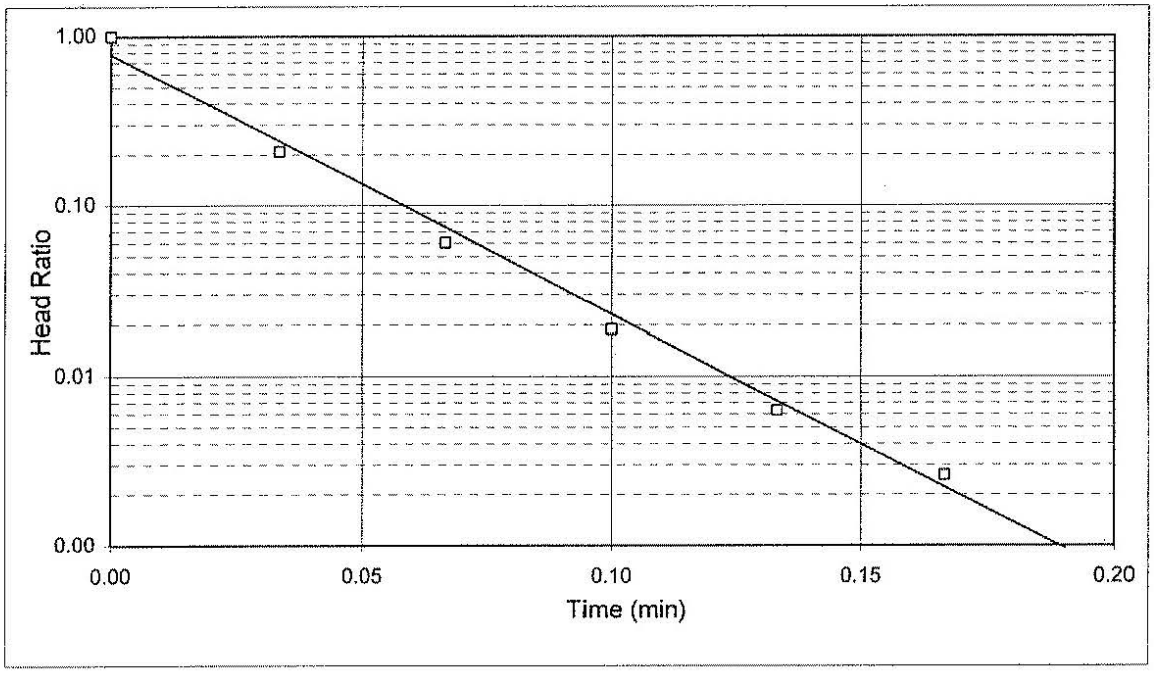
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.34
L_e =	16
t_1 (min) =	0
t_2 (min) =	0.19
h_1/h_0 =	0.78
h_2/h_0 =	0.00

RESULTS

K=	1.49E-02	cm/sec
K=	4.22E+01	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/24/95

Analysis By: CVK
Checked By: FRB
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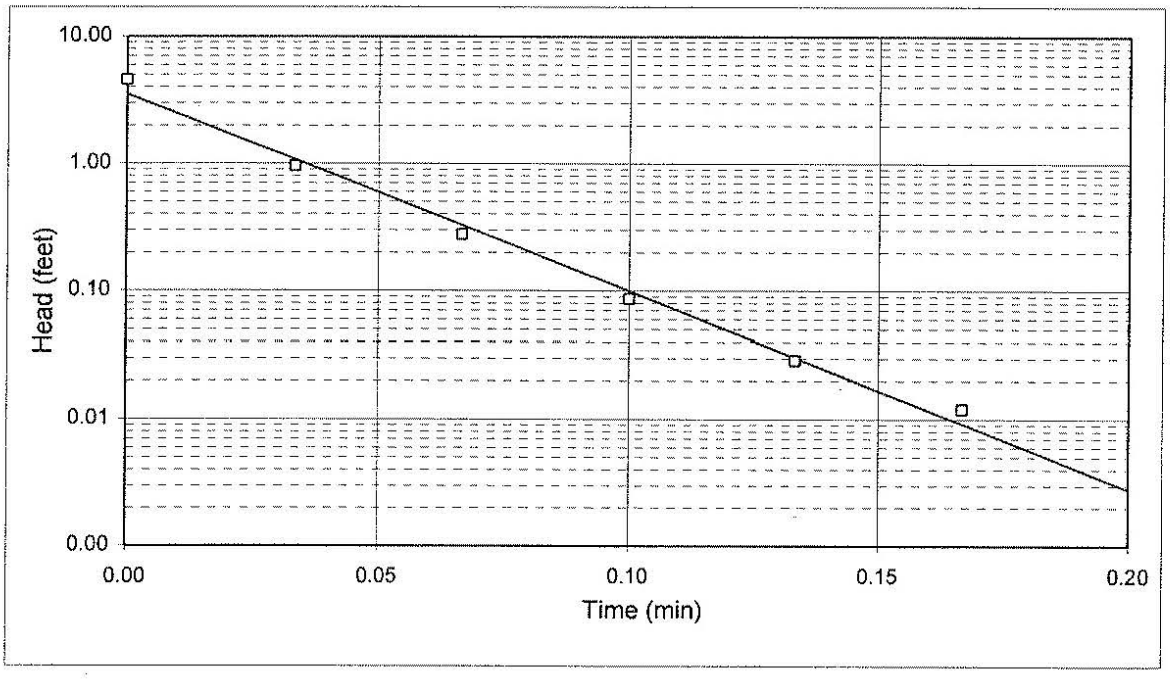
BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-302-AI

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
r_w =	0.34			
L_e =	16	K=	1.03E-02	cm/sec
$\ln(R_e/r_w)$	2.61	K=	2.92E+01	ft/day
y_0 =	3.55			
y_t =	0.00			
t =	0.20			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/24/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

FALLING HEAD TEST PZ-303-AS

WELL NO. PZ-303-AS

DATE	10/31/95	
INITAL HEAD ON TRANSDUCER	6.3	FEET H_2O
INITIAL DEPTH TO WATER	20.96	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	10.25	INCHES
TOP OF OPEN INTERVAL	14.2	FEET (btoc)
BOTTOM OF OPEN INTERVAL	28.9	FEET (btoc)
SATURATED THICKNESS	130	FEET
WATER TABLE TO BOTTOM OF SCREEN	7.92	FEET
EQUIVALENT DIAMETER	5.86	INCHES
OPEN INTERVAL LENGTH	7.92	FEET
STATIC IN SCREEN?	Y	
MAX. HEAD CHANGE	0.71	FEET
MAX. HEAD IN SCREEN?	Y	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	305	1140	28	7.0117	0.00	20.25	0.71	1.00
305	305	1140	29	6.9891	0.02	20.27	0.69	0.97
305	305	1140	30	6.9531	0.03	20.31	0.65	0.92
305	305	1140	31	6.9387	0.05	20.32	0.64	0.90
305	305	1140	32	7.1578	0.07	20.10	0.86	1.21
305	305	1140	33	6.895	0.08	20.37	0.59	0.84
305	305	1140	34	6.886	0.10	20.37	0.59	0.82
305	305	1140	35	6.8729	0.12	20.39	0.57	0.80
305	305	1140	36	6.8633	0.13	20.40	0.56	0.79
305	305	1140	37	6.8573	0.15	20.40	0.56	0.78
305	305	1140	38	6.8517	0.17	20.41	0.55	0.78
305	305	1140	39	6.8446	0.18	20.42	0.54	0.77
305	305	1140	40	6.8373	0.20	20.42	0.54	0.75
305	305	1140	41	6.8337	0.22	20.43	0.53	0.75
305	305	1140	42	6.8085	0.23	20.45	0.51	0.71
305	305	1140	43	6.8229	0.25	20.44	0.52	0.73
305	305	1140	44	6.8224	0.27	20.44	0.52	0.73
305	305	1140	45	6.8238	0.28	20.44	0.52	0.74
305	305	1140	46	6.8204	0.30	20.44	0.52	0.73
305	305	1140	47	6.8155	0.32	20.44	0.52	0.72
305	305	1140	48	6.8113	0.33	20.45	0.51	0.72
305	305	1140	49	6.8054	0.35	20.45	0.51	0.71
305	305	1140	50	6.7971	0.37	20.46	0.50	0.70
305	305	1140	51	6.7896	0.38	20.47	0.49	0.69
305	305	1140	52	6.7825	0.40	20.48	0.48	0.68
305	305	1140	53	6.775	0.42	20.49	0.48	0.67
305	305	1140	54	6.7641	0.43	20.50	0.46	0.65

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	305	1140	55	6.7626	0.45	20.50	0.46	0.65
305	305	1140	56	6.7508	0.47	20.51	0.45	0.63
305	305	1140	57	6.7435	0.48	20.52	0.44	0.62
305	305	1140	58	6.7383	0.50	20.52	0.44	0.62
305	305	1140	59	6.7318	0.52	20.53	0.43	0.61
305	305	1141	0	6.7263	0.53	20.53	0.43	0.60
305	305	1141	1	6.7197	0.55	20.54	0.42	0.59
305	305	1141	2	6.7188	0.57	20.54	0.42	0.59
305	305	1141	3	6.7093	0.58	20.55	0.41	0.58
305	305	1141	4	6.7377	0.60	20.52	0.44	0.62
305	305	1141	5	6.6657	0.62	20.59	0.37	0.51
305	305	1141	6	6.7052	0.63	20.55	0.41	0.57
305	305	1141	7	6.6993	0.65	20.56	0.40	0.56
305	305	1141	8	6.6973	0.67	20.56	0.40	0.56
305	305	1141	9	6.6889	0.68	20.57	0.39	0.55
305	305	1141	10	6.6878	0.70	20.57	0.39	0.54
305	305	1141	11	6.6792	0.72	20.58	0.38	0.53
305	305	1141	12	6.6761	0.73	20.58	0.38	0.53
305	305	1141	13	6.5809	0.75	20.68	0.28	0.39
305	305	1141	14	6.6627	0.77	20.60	0.36	0.51
305	305	1141	15	6.6697	0.78	20.59	0.37	0.52
305	305	1141	16	6.6812	0.80	20.58	0.38	0.54
305	305	1141	17	6.6623	0.82	20.60	0.36	0.51
305	305	1141	18	6.6551	0.83	20.60	0.36	0.50
305	305	1141	19	6.6509	0.85	20.61	0.35	0.49
305	305	1141	20	6.6471	0.87	20.61	0.35	0.49
305	305	1141	21	6.6438	0.88	20.62	0.34	0.48
305	305	1141	22	6.6388	0.90	20.62	0.34	0.48
305	305	1141	23	6.6354	0.92	20.62	0.34	0.47
305	305	1141	24	6.6342	0.93	20.63	0.33	0.47
305	305	1141	25	6.6295	0.95	20.63	0.33	0.46
305	305	1141	26	6.626	0.97	20.63	0.33	0.46
305	305	1141	27	6.6214	0.98	20.64	0.32	0.45
305	305	1141	28	6.6204	1.00	20.64	0.32	0.45
305	305	1141	29	6.6156	1.02	20.64	0.32	0.44
305	305	1141	30	6.6127	1.03	20.65	0.31	0.44
305	305	1141	31	6.6108	1.05	20.65	0.31	0.44
305	305	1141	32	6.6086	1.07	20.65	0.31	0.43
305	305	1141	33	6.6054	1.08	20.65	0.31	0.43
305	305	1141	34	6.6033	1.10	20.66	0.30	0.43
305	305	1141	35	6.6011	1.12	20.66	0.30	0.42
305	305	1141	36	6.599	1.13	20.66	0.30	0.42
305	305	1141	37	6.5973	1.15	20.66	0.30	0.42
305	305	1141	38	6.5935	1.17	20.67	0.29	0.41
305	305	1141	39	6.5912	1.18	20.67	0.29	0.41

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	305	1141	40	6.5877	1.20	20.67	0.29	0.40
305	305	1141	41	6.5863	1.22	20.67	0.29	0.40
305	305	1141	42	6.5828	1.23	20.68	0.28	0.40
305	305	1141	43	6.58	1.25	20.68	0.28	0.39
305	305	1141	44	6.577	1.27	20.68	0.28	0.39
305	305	1141	45	6.578	1.28	20.68	0.28	0.39
305	305	1141	46	6.5716	1.30	20.69	0.27	0.38
305	305	1141	47	6.5696	1.32	20.69	0.27	0.38
305	305	1141	48	6.572	1.33	20.69	0.27	0.38
305	305	1141	49	6.5659	1.35	20.69	0.27	0.37
305	305	1141	50	6.5612	1.37	20.70	0.26	0.37
305	305	1141	51	6.5629	1.38	20.70	0.26	0.37
305	305	1141	52	6.5616	1.40	20.70	0.26	0.37
305	305	1141	53	6.5557	1.42	20.70	0.26	0.36
305	305	1141	54	6.5571	1.43	20.70	0.26	0.36
305	305	1141	55	6.5538	1.45	20.71	0.25	0.36
305	305	1141	56	6.5524	1.47	20.71	0.25	0.35
305	305	1141	57	6.55	1.48	20.71	0.25	0.35
305	305	1141	58	6.5479	1.50	20.71	0.25	0.35
305	305	1141	59	6.5453	1.52	20.71	0.25	0.34
305	305	1142	0	6.5402	1.53	20.72	0.24	0.34
305	305	1142	1	6.5368	1.55	20.72	0.24	0.33
305	305	1142	2	6.5352	1.57	20.72	0.24	0.33
305	305	1142	3	6.5338	1.58	20.73	0.23	0.33
305	305	1142	4	6.5305	1.60	20.73	0.23	0.32
305	305	1142	5	6.529	1.62	20.73	0.23	0.32
305	305	1142	6	6.5257	1.63	20.73	0.23	0.32
305	305	1142	7	6.5235	1.65	20.74	0.22	0.31
305	305	1142	8	6.5211	1.67	20.74	0.22	0.31
305	305	1142	9	6.5197	1.68	20.74	0.22	0.31
305	305	1142	10	6.5164	1.70	20.74	0.22	0.30
305	305	1142	11	6.516	1.72	20.74	0.22	0.30
305	305	1142	12	6.5144	1.73	20.75	0.21	0.30
305	305	1142	13	6.5123	1.75	20.75	0.21	0.30
305	305	1142	14	6.5126	1.77	20.75	0.21	0.30
305	305	1142	15	6.51	1.78	20.75	0.21	0.30
305	305	1142	16	6.5082	1.80	20.75	0.21	0.29
305	305	1142	17	6.5071	1.82	20.75	0.21	0.29
305	305	1142	18	6.505	1.83	20.76	0.20	0.29
305	305	1142	19	6.5032	1.85	20.76	0.20	0.29
305	305	1142	20	6.4996	1.87	20.76	0.20	0.28
305	305	1142	21	6.4979	1.88	20.76	0.20	0.28
305	305	1142	22	6.4969	1.90	20.76	0.20	0.28
305	305	1142	23	6.4955	1.92	20.76	0.20	0.27
305	305	1142	24	6.4939	1.93	20.77	0.19	0.27

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	305	1142	25	6.4926	1.95	20.77	0.19	0.27
305	305	1142	26	6.4912	1.97	20.77	0.19	0.27
305	305	1142	27	6.4895	1.98	20.77	0.19	0.27
305	305	1142	28	6.4883	2.00	20.77	0.19	0.26
305	305	1142	29	6.4871	2.02	20.77	0.19	0.26
305	305	1142	30	6.4858	2.03	20.77	0.19	0.26
305	305	1142	31	6.4844	2.05	20.78	0.18	0.26
305	305	1142	32	6.4839	2.07	20.78	0.18	0.26
305	305	1142	33	6.483	2.08	20.78	0.18	0.26
305	305	1142	34	6.4806	2.10	20.78	0.18	0.25
305	305	1142	35	6.4791	2.12	20.78	0.18	0.25
305	305	1142	36	6.4781	2.13	20.78	0.18	0.25
305	305	1142	37	6.4771	2.15	20.78	0.18	0.25
305	305	1142	38	6.4759	2.17	20.78	0.18	0.25
305	305	1142	39	6.4746	2.18	20.79	0.17	0.25
305	305	1142	40	6.4744	2.20	20.79	0.17	0.25
305	305	1142	41	6.4731	2.22	20.79	0.17	0.24
305	305	1142	42	6.4721	2.23	20.79	0.17	0.24
305	305	1142	43	6.4708	2.25	20.79	0.17	0.24
305	305	1142	44	6.4701	2.27	20.79	0.17	0.24
305	305	1142	45	6.4689	2.28	20.79	0.17	0.24
305	305	1142	46	6.4677	2.30	20.79	0.17	0.24
305	305	1142	47	6.4668	2.32	20.79	0.17	0.23
305	305	1142	48	6.4652	2.33	20.79	0.17	0.23
305	305	1142	49	6.4645	2.35	20.80	0.16	0.23
305	305	1142	50	6.4631	2.37	20.80	0.16	0.23
305	305	1142	51	6.4631	2.38	20.80	0.16	0.23
305	305	1142	52	6.4636	2.40	20.80	0.16	0.23
305	305	1142	53	6.4609	2.42	20.80	0.16	0.23
305	305	1142	54	6.4606	2.43	20.80	0.16	0.23
305	305	1142	55	6.4597	2.45	20.80	0.16	0.22
305	305	1142	56	6.4596	2.47	20.80	0.16	0.22
305	305	1142	57	6.4589	2.48	20.80	0.16	0.22
305	305	1142	58	6.4579	2.50	20.80	0.16	0.22
305	305	1142	59	6.4576	2.52	20.80	0.16	0.22
305	305	1143	0	6.4576	2.53	20.80	0.16	0.22
305	305	1143	1	6.455	2.55	20.81	0.16	0.22
305	305	1143	2	6.4553	2.57	20.80	0.16	0.22
305	305	1143	3	6.4542	2.58	20.81	0.15	0.22
305	305	1143	4	6.4546	2.60	20.81	0.15	0.22
305	305	1143	5	6.4535	2.62	20.81	0.15	0.22
305	305	1143	6	6.4534	2.63	20.81	0.15	0.22
305	305	1143	7	6.4522	2.65	20.81	0.15	0.21
305	305	1143	8	6.4517	2.67	20.81	0.15	0.21
305	305	1143	9	6.4514	2.68	20.81	0.15	0.21

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	305	1143	10	6.4494	2.70	20.81	0.15	0.21
305	305	1143	11	6.4501	2.72	20.81	0.15	0.21
305	305	1143	12	6.4497	2.73	20.81	0.15	0.21
305	305	1143	13	6.4487	2.75	20.81	0.15	0.21
305	305	1143	14	6.4477	2.77	20.81	0.15	0.21
305	305	1143	15	6.4472	2.78	20.81	0.15	0.21
305	305	1143	16	6.4472	2.80	20.81	0.15	0.21
305	305	1143	17	6.4455	2.82	20.81	0.15	0.20
305	305	1143	18	6.4453	2.83	20.81	0.15	0.20
305	305	1143	19	6.4438	2.85	20.82	0.14	0.20
305	305	1143	20	6.4435	2.87	20.82	0.14	0.20
305	305	1143	21	6.4426	2.88	20.82	0.14	0.20
305	305	1143	22	6.4417	2.90	20.82	0.14	0.20
305	305	1143	23	6.4414	2.92	20.82	0.14	0.20
305	305	1143	24	6.4415	2.93	20.82	0.14	0.20
305	305	1143	25	6.4411	2.95	20.82	0.14	0.20
305	305	1143	26	6.4404	2.97	20.82	0.14	0.20
305	305	1143	27	6.4402	2.98	20.82	0.14	0.20
305	305	1143	28	6.4398	3.00	20.82	0.14	0.20
305	305	1143	29	6.4385	3.02	20.82	0.14	0.19
305	305	1143	30	6.4388	3.03	20.82	0.14	0.20
305	305	1143	31	6.4376	3.05	20.82	0.14	0.19
305	305	1143	32	6.4355	3.07	20.82	0.14	0.19
305	305	1143	31	6.4376	3.05	20.82	0.14	0.19
305	305	1143	32	6.4355	3.07	20.82	0.14	0.19

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-303-AS

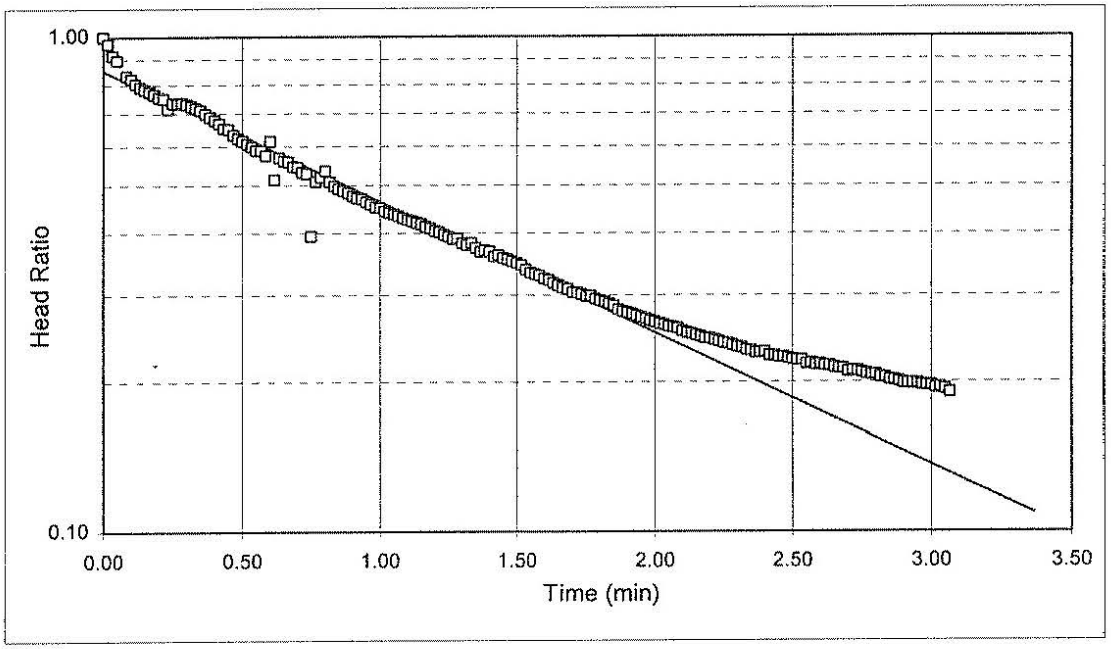
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.43
L_e =	7.92
t_1 (min) =	0
t_2 (min) =	3.37
h_1/h_0 =	0.86
h_2/h_0 =	0.11

RESULTS

K=	3.98E-04	cm/sec
K=	1.13E+00	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/31/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

RISING HEAD TEST PZ-303-AS

WELL NO. PZ-303-AS

DATE	10/31/95	
INITAL HEAD ON TRANSDUCER	6.3	FEET H_2O
INITIAL DEPTH TO WATER	20.96	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	10.25	INCHES
TOP OF OPEN INTERVAL	14.2	FEET (btoc)
BOTTOM OF OPEN INTERVAL	28.9	FEET (btoc)
SATURATED THICKNESS	130	FEET
WATER TABLE TO BOTTOM OF SCREEN	7.92	FEET
EQUIVALENT DIAMETER	5.86	INCHES
OPEN INTERVAL LENGTH	7.92	FEET
STATIC IN SCREEN?	Y	
MAX. HEAD CHANGE	1.24	FEET
MAX. HEAD IN SCREEN?	Y	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	305	1143	34	5.0619	0.00	22.20	1.24	1.00
305	305	1143	35	5.2636	0.02	22.00	1.04	0.84
305	305	1143	36	5.399	0.03	21.86	0.90	0.73
305	305	1143	37	5.4883	0.05	21.77	0.81	0.66
305	305	1143	38	5.5617	0.07	21.70	0.74	0.60
305	305	1143	39	5.6208	0.08	21.64	0.68	0.55
305	305	1143	40	5.6747	0.10	21.59	0.63	0.51
305	305	1143	41	5.7239	0.12	21.54	0.58	0.47
305	305	1143	42	5.7655	0.13	21.49	0.53	0.43
305	305	1143	43	5.8101	0.15	21.45	0.49	0.40
305	305	1143	44	5.8564	0.17	21.40	0.44	0.36
305	305	1143	45	5.8925	0.18	21.37	0.41	0.33
305	305	1143	46	5.9307	0.20	21.33	0.37	0.30
305	305	1143	47	5.9607	0.22	21.30	0.34	0.27
305	305	1143	48	5.9848	0.23	21.28	0.32	0.25
305	305	1143	49	6.0136	0.25	21.25	0.29	0.23
305	305	1143	50	6.0444	0.27	21.22	0.26	0.21
305	305	1143	51	6.0691	0.28	21.19	0.23	0.19
305	305	1143	52	6.0926	0.30	21.17	0.21	0.17
305	305	1143	53	6.1123	0.32	21.15	0.19	0.15
305	305	1143	54	6.1324	0.33	21.13	0.17	0.14
305	305	1143	55	6.1497	0.35	21.11	0.15	0.12
305	305	1143	56	6.1703	0.37	21.09	0.13	0.10
305	305	1143	57	6.1853	0.38	21.07	0.11	0.09

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	305	1143	58	6.2013	0.40	21.06	0.10	0.08
305	305	1143	59	6.2144	0.42	21.05	0.09	0.07
305	305	1144	0	6.2249	0.43	21.04	0.08	0.06
305	305	1144	1	6.2366	0.45	21.02	0.06	0.05
305	305	1144	2	6.2443	0.47	21.02	0.06	0.04
305	305	1144	3	6.2565	0.48	21.00	0.04	0.04
305	305	1144	4	6.2603	0.50	21.00	0.04	0.03
305	305	1144	5	6.2707	0.52	20.99	0.03	0.02
305	305	1144	6	6.2768	0.53	20.98	0.02	0.02
305	305	1144	7	6.2828	0.55	20.98	0.02	0.01
305	305	1144	8	6.2889	0.57	20.97	0.01	0.01

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-303-AS

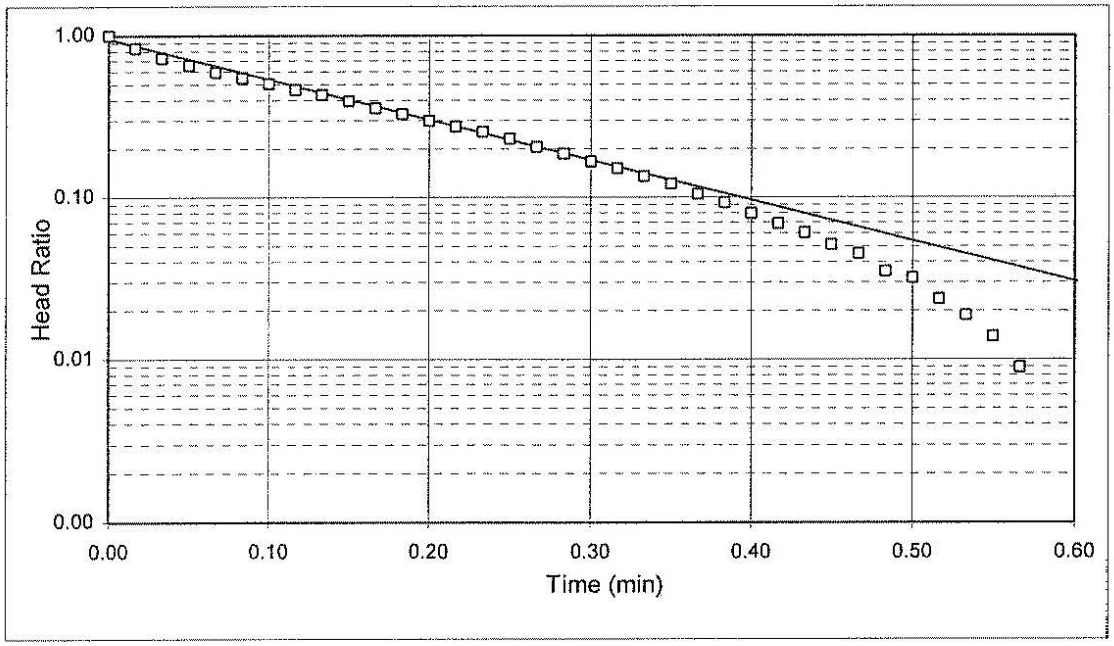
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.43
L_e =	7.92
t_1 (min) =	0
t_2 (min) =	0.60
h_1/h_0 =	0.95
h_2/h_0 =	0.03

RESULTS

K=	3.73E-03	cm/sec
K=	1.06E+01	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/31/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

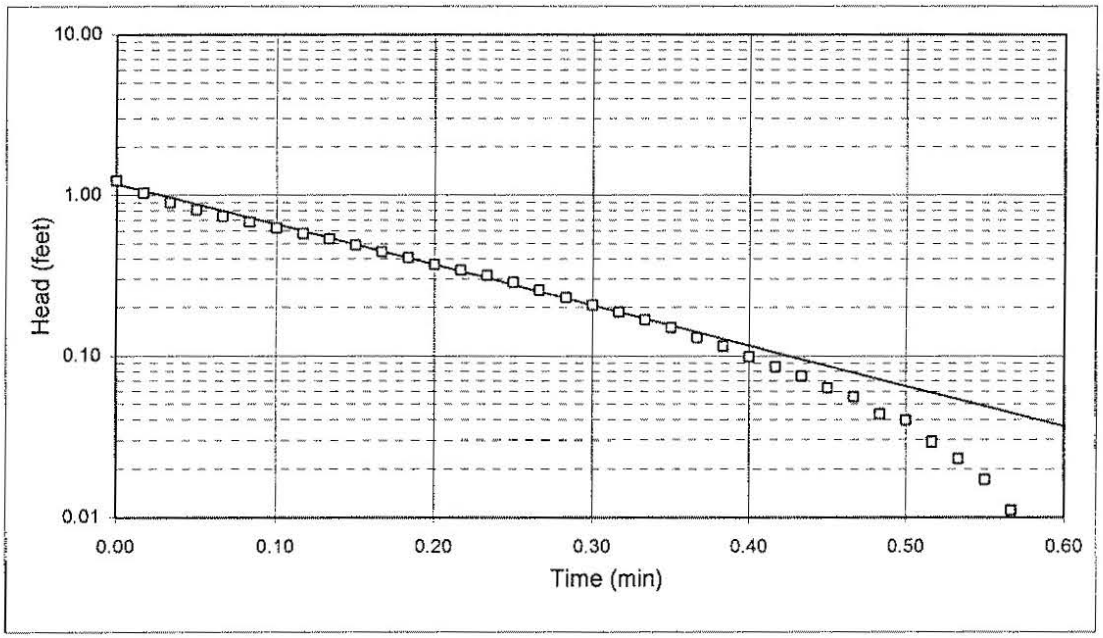
BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-303-AS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.24			
r_w =	0.43			
L_e =	7.92	K=	1.48E-02	cm/sec
$\ln(R_e/r_w)$	1.34	K=	4.20E+01	ft/day
y_0 =	1.17			
y_t =	0.04			
t =	0.60			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/31/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

FALLING HEAD TEST PZ-304-AS

WELL NO. PZ-304-AS

DATE	10/24/95	
INITAL HEAD ON TRANSDUCER	7.28	FEET H_2O
INITIAL DEPTH TO WATER	21.35	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	13.8	FEET (btoc)
BOTTOM OF OPEN INTERVAL	30.3	FEET (btoc)
SATURATED THICKNESS	140	FEET
WATER TABLE TO BOTTOM OF SCREEN	8.96	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	8.96	FEET
STATIC IN SCREEN?	Y	
MAX. HEAD CHANGE	0.39	FEET
MAX. HEAD IN SCREEN?	Y	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	298	1438	44	7.6689	0.00	20.96	0.39	1.00
305	298	1438	46	7.5014	0.03	21.13	0.22	0.57
305	298	1438	48	7.4805	0.07	21.15	0.20	0.52
305	298	1438	50	7.4567	0.10	21.17	0.18	0.45
305	298	1438	52	7.4413	0.13	21.19	0.16	0.41
305	298	1438	54	7.5322	0.17	21.10	0.25	0.65
305	298	1438	56	7.4344	0.20	21.20	0.15	0.40
305	298	1438	58	7.4224	0.23	21.21	0.14	0.37
305	298	1439	0	7.4117	0.27	21.22	0.13	0.34
305	298	1439	2	7.409	0.30	21.22	0.13	0.33
305	298	1439	4	7.3946	0.33	21.24	0.11	0.29
305	298	1439	6	7.3879	0.37	21.24	0.11	0.28
305	298	1439	8	7.3814	0.40	21.25	0.10	0.26
305	298	1439	10	7.3773	0.43	21.25	0.10	0.25
305	298	1439	12	7.3724	0.47	21.26	0.09	0.24
305	298	1439	14	7.3658	0.50	21.26	0.09	0.22
305	298	1439	16	7.3609	0.53	21.27	0.08	0.21
305	298	1439	18	7.3603	0.57	21.27	0.08	0.21
305	298	1439	20	7.3566	0.60	21.27	0.08	0.20
305	298	1439	22	7.3524	0.63	21.28	0.07	0.19
305	298	1439	24	7.3498	0.67	21.28	0.07	0.18
305	298	1439	26	7.3429	0.70	21.29	0.06	0.16
305	298	1439	28	7.3438	0.73	21.29	0.06	0.16
305	298	1439	30	7.3411	0.77	21.29	0.06	0.16
305	298	1439	32	7.3355	0.80	21.29	0.06	0.14
305	298	1439	34	7.3354	0.83	21.29	0.06	0.14
305	298	1439	36	7.3322	0.87	21.30	0.05	0.13
305	298	1439	38	7.3297	0.90	21.30	0.05	0.13
305	298	1439	40	7.3275	0.93	21.30	0.05	0.12
305	298	1439	42	7.326	0.97	21.30	0.05	0.12

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	298	1439	44	7.3246	1.00	21.31	0.04	0.11
305	298	1439	46	7.3223	1.03	21.31	0.04	0.11
305	298	1439	55	7.3194	1.18	21.31	0.04	0.10
305	298	1439	56	7.3154	1.20	21.31	0.04	0.09
305	298	1439	57	7.3155	1.22	21.31	0.04	0.09
305	298	1439	58	7.3138	1.23	21.32	0.03	0.09
305	298	1439	59	7.3133	1.25	21.32	0.03	0.09
305	298	1440	0	7.3121	1.27	21.32	0.03	0.08
305	298	1440	1	7.3119	1.28	21.32	0.03	0.08
305	298	1440	2	7.3102	1.30	21.32	0.03	0.08
305	298	1440	3	7.3103	1.32	21.32	0.03	0.08
305	298	1440	4	7.3099	1.33	21.32	0.03	0.08
305	298	1440	5	7.3085	1.35	21.32	0.03	0.07
305	298	1440	6	7.3081	1.37	21.32	0.03	0.07
305	298	1440	7	7.3072	1.38	21.32	0.03	0.07
305	298	1440	8	7.3086	1.40	21.32	0.03	0.07
305	298	1440	9	7.3053	1.42	21.32	0.03	0.07
305	298	1440	10	7.3056	1.43	21.32	0.03	0.07
305	298	1440	11	7.3048	1.45	21.33	0.02	0.06
305	298	1440	12	7.3038	1.47	21.33	0.02	0.06
305	298	1440	13	7.3028	1.48	21.33	0.02	0.06
305	298	1440	14	7.3035	1.50	21.33	0.02	0.06
305	298	1440	15	7.3017	1.52	21.33	0.02	0.06
305	298	1440	16	7.3012	1.53	21.33	0.02	0.05
305	298	1440	17	7.3019	1.55	21.33	0.02	0.06
305	298	1440	18	7.3004	1.57	21.33	0.02	0.05
305	298	1440	19	7.2996	1.58	21.33	0.02	0.05
305	298	1440	20	7.2972	1.60	21.33	0.02	0.04
305	298	1440	21	7.2977	1.62	21.33	0.02	0.05
305	298	1440	22	7.2968	1.63	21.33	0.02	0.04
305	298	1440	23	7.2963	1.65	21.33	0.02	0.04
305	298	1440	24	7.2967	1.67	21.33	0.02	0.04
305	298	1440	25	7.2954	1.68	21.33	0.02	0.04
305	298	1440	26	7.2946	1.70	21.34	0.01	0.04
305	298	1440	27	7.2944	1.72	21.34	0.01	0.04
305	298	1440	28	7.2944	1.73	21.34	0.01	0.04
305	298	1440	29	7.2925	1.75	21.34	0.01	0.03
305	298	1440	30	7.2921	1.77	21.34	0.01	0.03
305	298	1440	31	7.2906	1.78	21.34	0.01	0.03
305	298	1440	32	7.2898	1.80	21.34	0.01	0.03
305	298	1440	33	7.2899	1.82	21.34	0.01	0.03
305	298	1440	34	7.2888	1.83	21.34	0.01	0.02
305	298	1440	35	7.2893	1.85	21.34	0.01	0.02
305	298	1440	36	7.2889	1.87	21.34	0.01	0.02
305	298	1440	37	7.289	1.88	21.34	0.01	0.02
305	298	1440	38	7.2872	1.90	21.34	0.01	0.02

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-304-AS

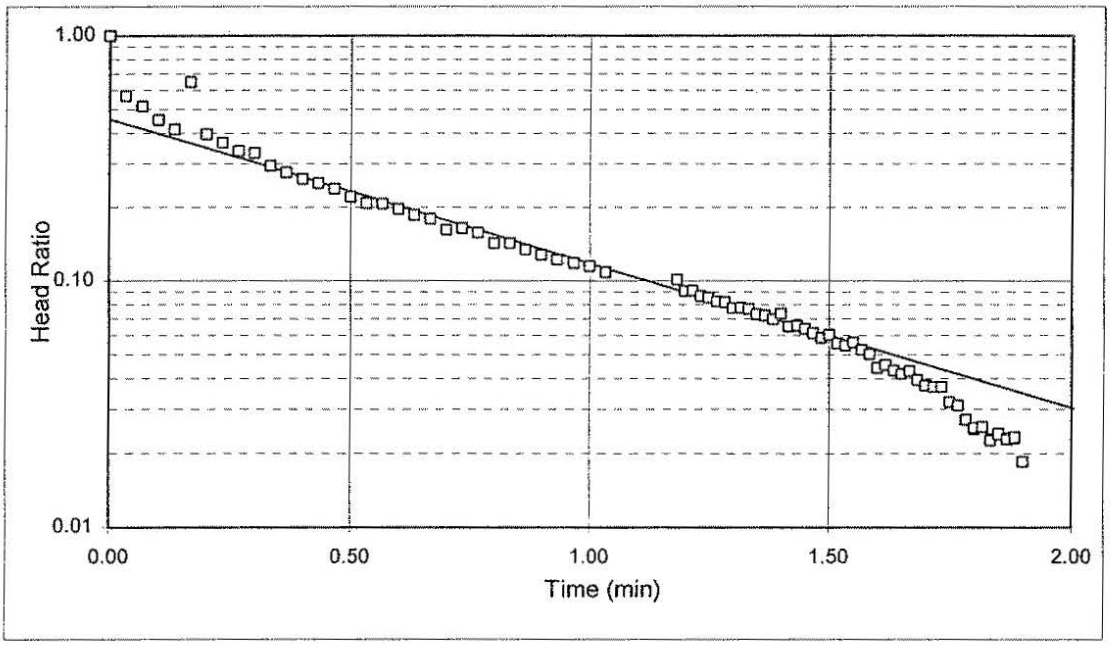
$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.34
L_e =	8.96
t_1 (min) =	0
t_2 (min) =	2.01
h_1/h_0 =	0.46
h_2/h_0 =	0.03

RESULTS

K=	8.69E-04	cm/sec
K=	2.46E+00	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/24/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

RISING HEAD TEST PZ-304-AS

WELL NO. PZ-304-AS

DATE	10/24/95	
INITAL HEAD ON TRANSDUCER	7.28	FEET H_2O
INITIAL DEPTH TO WATER	21.35	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	13.8	FEET (btoc)
BOTTOM OF OPEN INTERVAL	30.3	FEET (btoc)
SATURATED THICKNESS	140	FEET
WATER TABLE TO BOTTOM OF SCREEN	8.96	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	8.96	FEET
STATIC IN SCREEN?	Y	
MAX. HEAD CHANGE	2.48	FEET
MAX. HEAD IN SCREEN?	Y	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	298	1442	36	4.797	0.00	23.83	2.48	1.00
305	298	1442	38	5.555	0.03	23.08	1.73	0.69
305	298	1442	40	6.0565	0.07	22.57	1.22	0.49
305	298	1442	42	6.3892	0.10	22.24	0.89	0.36
305	298	1442	44	6.6299	0.13	22.00	0.65	0.26
305	298	1442	46	6.8063	0.17	21.82	0.47	0.19
305	298	1442	48	6.9305	0.20	21.70	0.35	0.14
305	298	1442	50	7.0198	0.23	21.61	0.26	0.10
305	298	1442	52	7.0945	0.27	21.54	0.19	0.07
305	298	1442	54	7.1446	0.30	21.49	0.14	0.05
305	298	1442	56	7.1798	0.33	21.45	0.10	0.04
305	298	1442	58	7.204	0.37	21.43	0.08	0.03
305	298	1443	0	7.2242	0.40	21.41	0.06	0.02
305	298	1443	2	7.2386	0.43	21.39	0.04	0.02
305	298	1443	4	7.2479	0.47	21.38	0.03	0.01
305	298	1443	6	7.261	0.50	21.37	0.02	0.01
305	298	1443	8	7.2662	0.53	21.36	0.01	0.01

HVORSLEV SLUG TEST ANALYSIS
RISING HEAD TEST PZ-304-AS

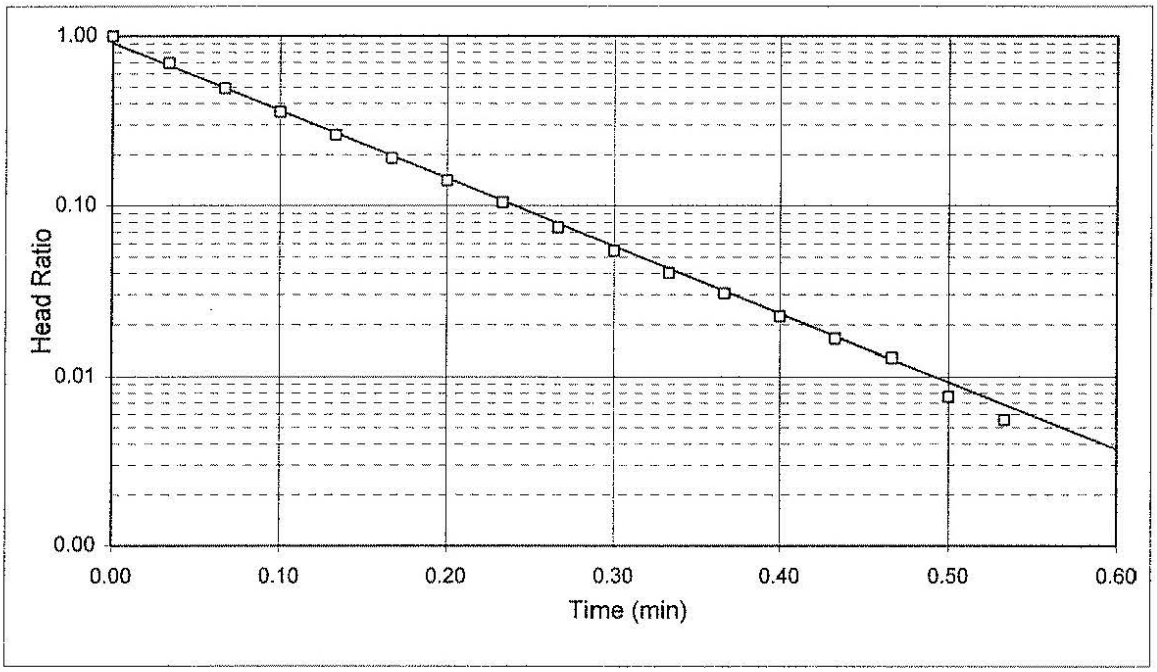
$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.34
L_e =	8.96
t_1 (min) =	0
t_2 (min) =	0.60
h_1/h_0 =	0.91
h_2/h_0 =	0.00

RESULTS

K=	5.89E-03	cm/sec
K=	1.67E+01	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/24/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

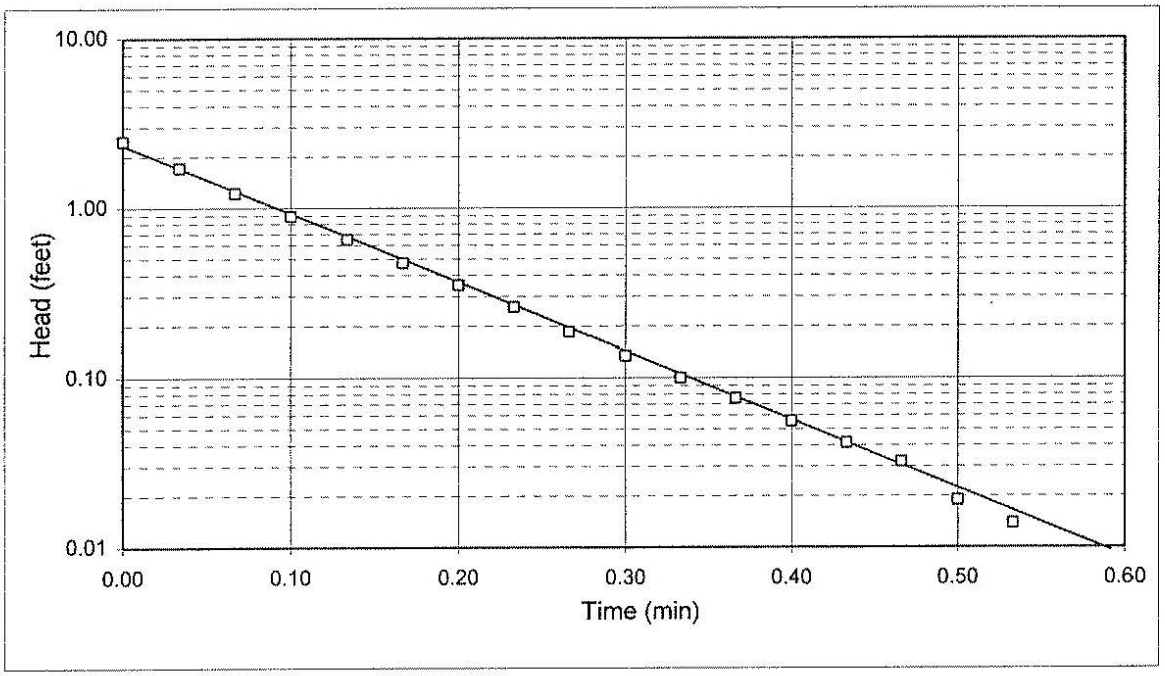
BOUWER AND RICE SLUG TEST ANALYSIS
RISING HEAD TEST PZ-304-AS

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.20			
r_w =	0.34			
L_e =	8.96	K=	1.84E-02	cm/sec
$\ln(R_e/r_w)$	1.73	K=	5.22E+01	ft/day
y_0 =	2.34			
y_t =	0.01			
t =	0.59			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/24/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

FALLING HEAD TEST PZ-304-AI

WELL NO. PZ-304-AI

DATE	10/24/95	
INITAL HEAD ON TRANSDUCER	9.9	FEET H_2O
INITIAL DEPTH TO WATER	21.72	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	38.3	FEET (btoc)
BOTTOM OF OPEN INTERVAL	52.4	FEET (btoc)
SATURATED THICKNESS	140	FEET
WATER TABLE TO BOTTOM OF SCREEN	30.7	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	14.1	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	2.48	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	298	1414	6	12.383	0.00	19.24	2.48	1.00
305	298	1414	8	9.2916	0.03	21.11	0.61	0.25
305	298	1414	10	9.8479	0.07	21.67	0.05	0.02
305	298	1414	12	9.9482	0.10	21.67	0.05	0.02
305	298	1414	14	9.9399	0.13	21.68	0.04	0.02
305	298	1414	16	9.9217	0.17	21.70	0.02	0.01
305	298	1414	18	9.9179	0.20	21.70	0.02	0.01

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-304-AI

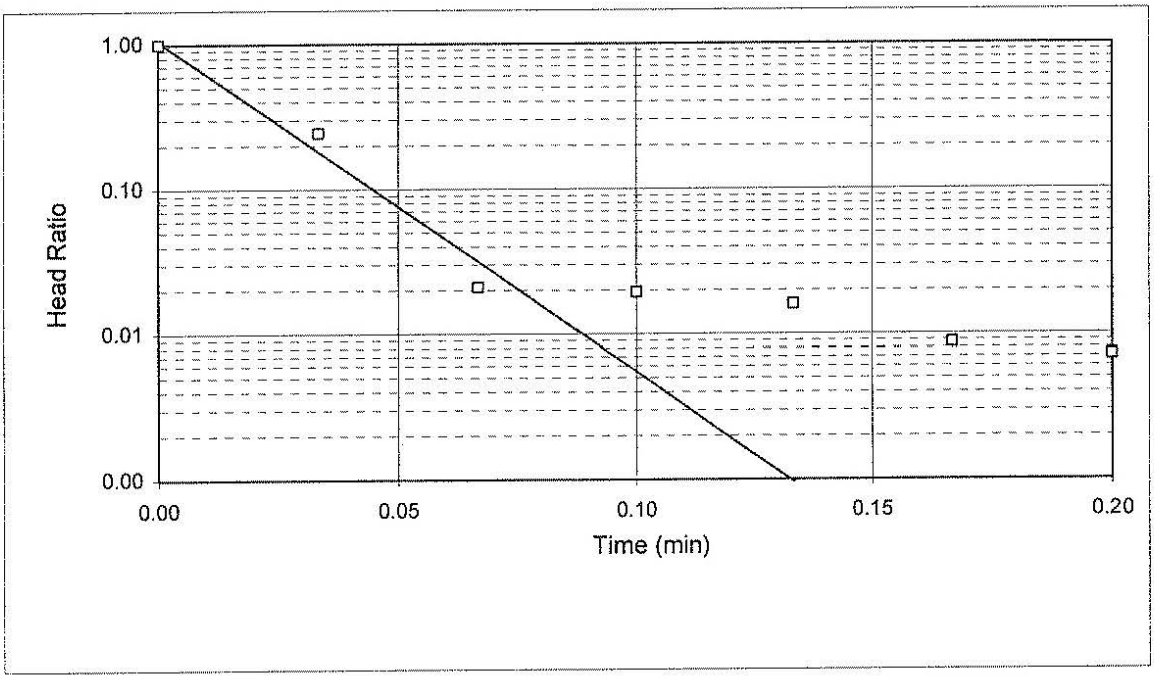
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.34
L_e =	14.1
t_1 (min) =	0
t_2 (min) =	0.13
h_1/h_0 =	1.05
h_2/h_0 =	0.00

RESULTS

K=	2.44E-02	cm/sec
K=	6.91E+01	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/24/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-304-AI

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

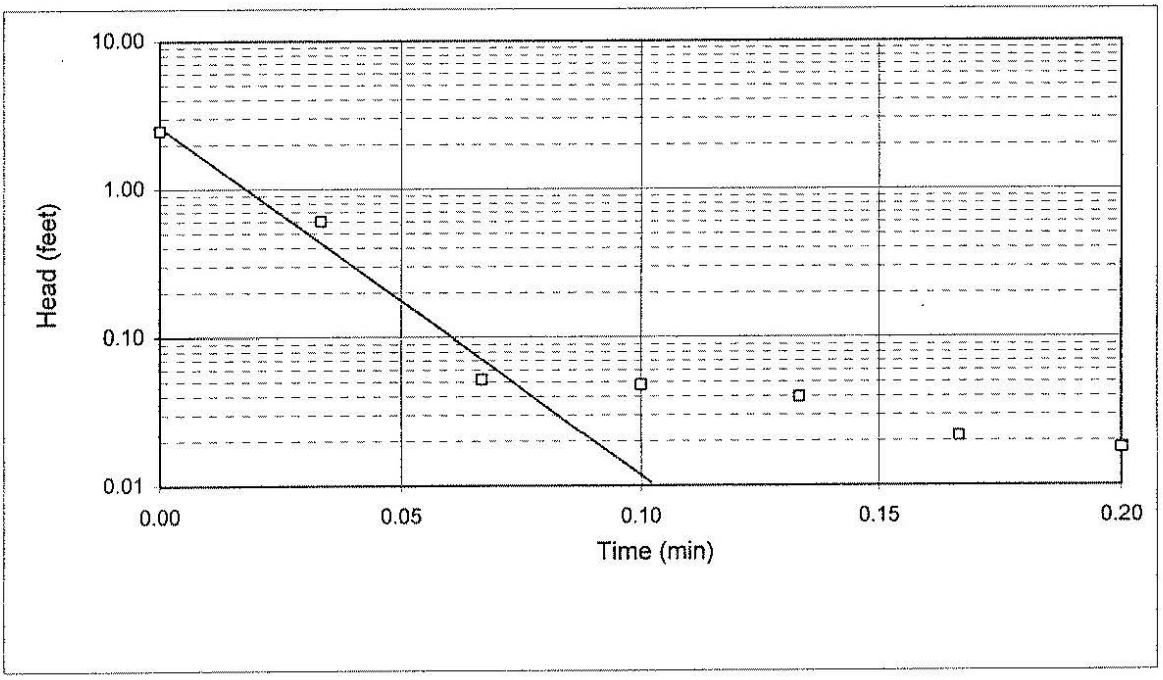
where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS	
r_c =	0.08
r_w =	0.34
L_e =	14.1
$\ln(R_e/r_w)$	2.53
y_0 =	2.63
y_t =	0.01
t =	0.10

RESULTS

K=	1.71E-02	cm/sec
K=	4.86E+01	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/24/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-305-AI

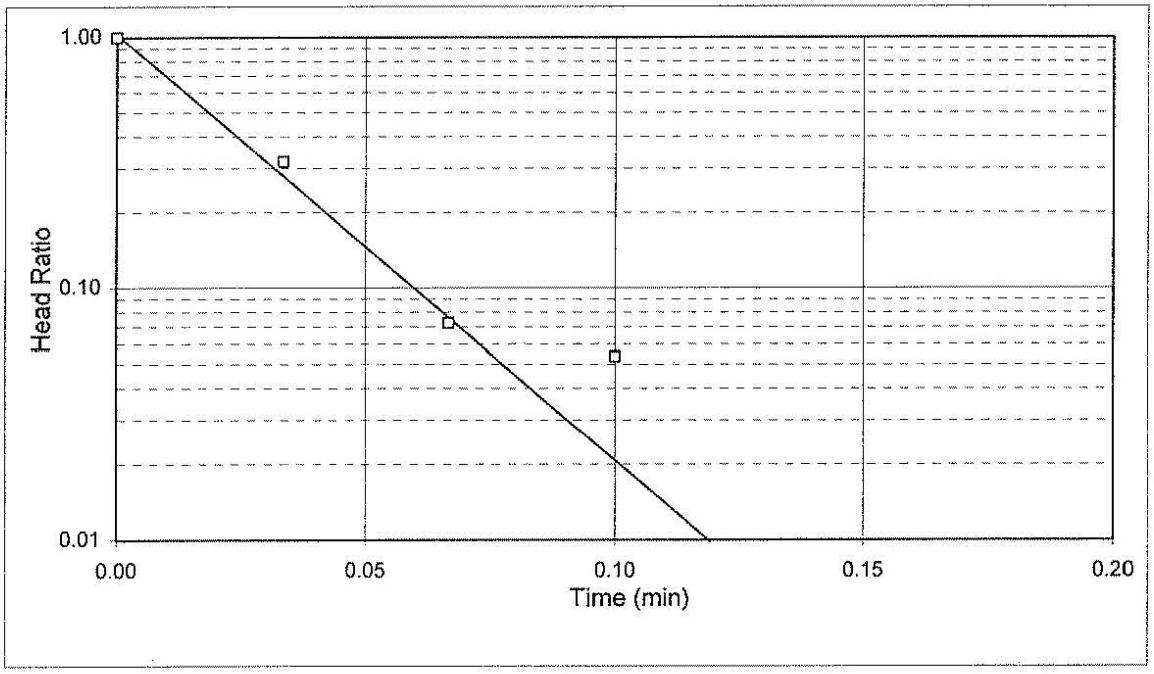
$$K = \frac{r_c^2}{2L_e} \ln\frac{L_e}{R_e}\left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)}\right] 30.48$$

where: r_c = casing radius (feet);
R_e = filter pack radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS	
r_c =	0.08
R_e =	0.34
L_e =	14.1
t_1 (min) =	0
t_2 (min) =	0.12
h_1/h_0 =	1.02
h_2/h_0 =	0.01

RESULTS

K=	1.81E-02	cm/sec
K=	5.13E+01	ft/day



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/31/95

Analysis By: CVK
Checked By: FRB
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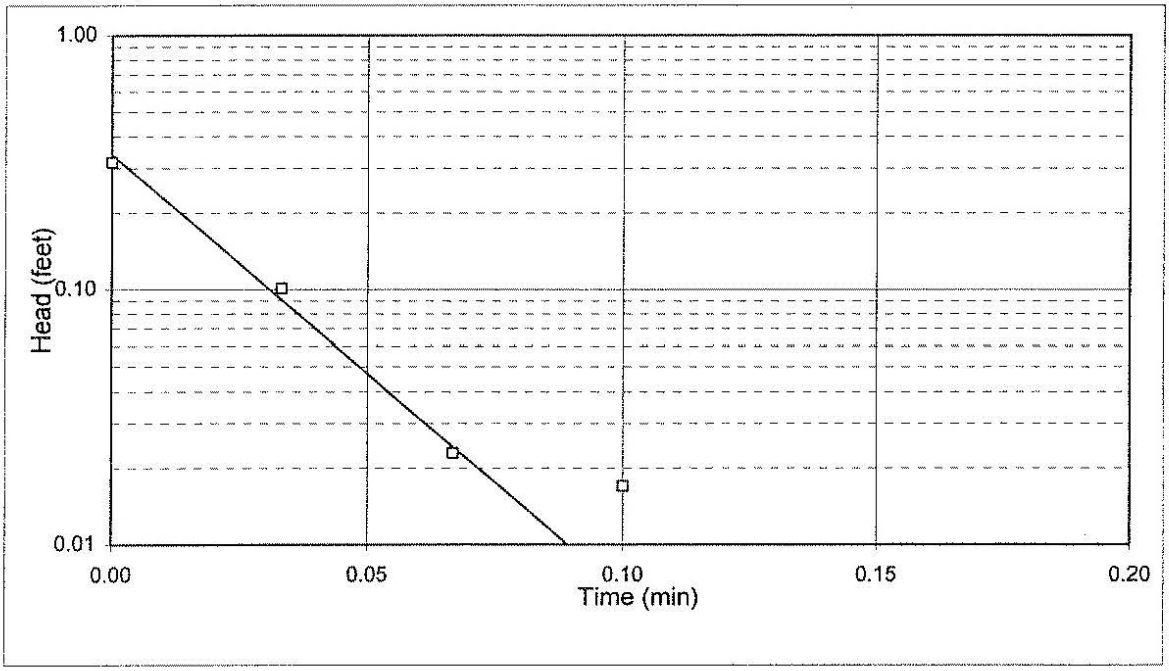
BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-305-AI

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
r_w =	0.34			
L_e =	14.1	K=	1.38E-02	cm/sec
$\ln(R_e/r_w)$	2.80	K=	3.92E+01	ft/day
y_0 =	0.34			
y_t =	0.01			
t =	0.09			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/31/95

Analysis By: CVK
Checked By: FRB
Analysis Date: 1/22/96

FALLING HEAD TEST PZ-305-AI

WELL NO. PZ-305-AI

DATE	10/31/95	
INITAL HEAD ON TRANSDUCER	10.74	FEET H_2O
INITIAL DEPTH TO WATER	27.18	FEET (btoc)
CASING DIAMETER	2	INCHES
SAND DIAMETER	8.25	INCHES
TOP OF OPEN INTERVAL	50.9	FEET (btoc)
BOTTOM OF OPEN INTERVAL	65.0	FEET (btoc)
SATURATED THICKNESS	500	FEET
WATER TABLE TO BOTTOM OF SCREEN	37.8	FEET
EQUIVALENT DIAMETER	4.82	INCHES
OPEN INTERVAL LENGTH	14.1	FEET
STATIC IN SCREEN?	N	
MAX. HEAD CHANGE	2.52	FEET
MAX. HEAD IN SCREEN?	N	

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	305	957	30	13.26	0.00	24.66	2.52	1.00
305	305	957	32	10.474	0.03	26.91	0.27	0.11
305	305	957	34	10.707	0.07	27.15	0.03	0.01
305	305	957	36	10.817	0.10	27.10	0.08	0.03
305	305	957	38	10.765	0.13	27.16	0.02	0.01
305	305	957	40	10.744	0.17	27.18	0.00	0.00
305	305	957	42	10.75	0.20	27.17	0.01	0.00
305	305	957	44	10.752	0.23	27.17	0.01	0.00
305	305	957	46	10.749	0.27	27.17	0.01	0.00
305	305	957	48	10.748	0.30	27.17	0.01	0.00
305	305	957	50	10.748	0.33	27.17	0.01	0.00
305	305	957	52	10.748	0.37	27.17	0.01	0.00
305	305	957	54	10.748	0.40	27.17	0.01	0.00
305	305	957	56	10.748	0.43	27.17	0.01	0.00
305	305	957	58	10.747	0.47	27.17	0.01	0.00
305	305	958	34	11.057	1.07	26.86	0.32	0.13
305	305	958	36	10.639	1.10	27.08	0.10	0.04
305	305	958	38	10.717	1.13	27.16	0.02	0.01
305	305	958	40	10.757	1.17	27.16	0.02	0.01
305	305	958	42	10.739	1.20	27.18	0.00	0.00
305	305	958	44	10.739	1.23	27.18	0.00	0.00
305	305	959	51	10.926	2.35	26.99	0.19	0.07
305	305	959	52	10.425	2.37	26.87	0.31	0.12
305	305	959	53	10.604	2.38	27.04	0.14	0.05
305	305	959	54	10.741	2.40	27.18	0.00	0.00
305	305	959	55	10.79	2.42	27.13	0.05	0.02
305	305	959	56	10.804	2.43	27.12	0.06	0.03
305	305	959	57	10.781	2.45	27.14	0.04	0.02
305	305	959	58	10.753	2.47	27.17	0.01	0.01
305	305	959	59	10.741	2.48	27.18	0.00	0.00

DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	305	1000	0	10.741	2.50	27.18	0.00	0.00
305	305	1001	21	9.8456	3.85	28.07	0.89	0.35
305	305	1001	22	11.004	3.87	27.44	0.26	0.10
305	305	1001	23	11.242	3.88	27.68	0.50	0.20
305	305	1001	24	10.981	3.90	27.42	0.24	0.10
305	305	1001	25	10.723	3.92	27.20	0.02	0.01
305	305	1001	26	10.636	3.93	27.28	0.10	0.04
305	305	1001	27	10.669	3.95	27.25	0.07	0.03
305	305	1001	28	10.726	3.97	27.19	0.01	0.01
305	305	1001	29	10.754	3.98	27.19	0.01	0.01
305	305	1001	30	10.756	4.00	27.20	0.02	0.01
305	305	1001	31	10.746	4.02	27.19	0.01	0.00
305	305	1001	32	10.738	4.03	27.18	0.00	0.00
305	305	1001	33	10.739	4.05	27.18	0.00	0.00
305	305	1001	34	10.739	4.07	27.18	0.00	0.00
305	305	1002	41	11.331	5.18	26.59	0.59	0.23
305	305	1002	42	10.251	5.20	26.69	0.49	0.19
305	305	1002	43	10.521	5.22	26.96	0.22	0.09
305	305	1002	44	10.672	5.23	27.11	0.07	0.03
305	305	1002	45	10.779	5.25	27.14	0.04	0.02
305	305	1002	46	10.812	5.27	27.11	0.07	0.03
305	305	1002	47	10.803	5.28	27.12	0.06	0.03
305	305	1002	48	10.77	5.30	27.15	0.03	0.01
305	305	1002	49	10.749	5.32	27.17	0.01	0.00
305	305	1002	50	10.745	5.33	27.18	0.00	0.00
305	305	1002	51	10.745	5.35	27.18	0.00	0.00
305	305	1003	25	4.5032	5.92	33.42	6.24	2.47
305	305	1003	26	10.801	5.93	27.24	0.06	0.02
305	305	1003	27	11.451	5.95	27.89	0.71	0.28
305	305	1003	28	11.212	5.97	27.65	0.47	0.19
305	305	1003	29	10.806	5.98	27.25	0.07	0.03
305	305	1003	30	10.616	6.00	27.30	0.12	0.05
305	305	1003	31	10.624	6.02	27.30	0.12	0.05
305	305	1003	32	10.703	6.03	27.22	0.04	0.01
305	305	1003	33	10.753	6.05	27.19	0.01	0.01
305	305	1003	34	10.762	6.07	27.20	0.02	0.01
305	305	1003	35	10.751	6.08	27.19	0.01	0.00
305	305	1003	36	10.74	6.10	27.18	0.00	0.00
305	305	1003	37	10.736	6.12	27.18	0.00	0.00
305	305	1003	38	10.74	6.13	27.18	0.00	0.00
305	305	1003	39	10.742	6.15	27.18	0.00	0.00
305	305	1003	40	10.743	6.17	27.18	0.00	0.00
305	305	1003	41	10.745	6.18	27.19	0.00	0.00
305	305	1003	42	10.745	6.20	27.19	0.00	0.00
305	305	1003	43	10.741	6.22	27.18	0.00	0.00
305	305	1003	44	10.742	6.23	27.18	0.00	0.00
305	305	1003	45	10.744	6.25	27.18	0.00	0.00
305	305	1003	46	10.742	6.27	27.18	0.00	0.00

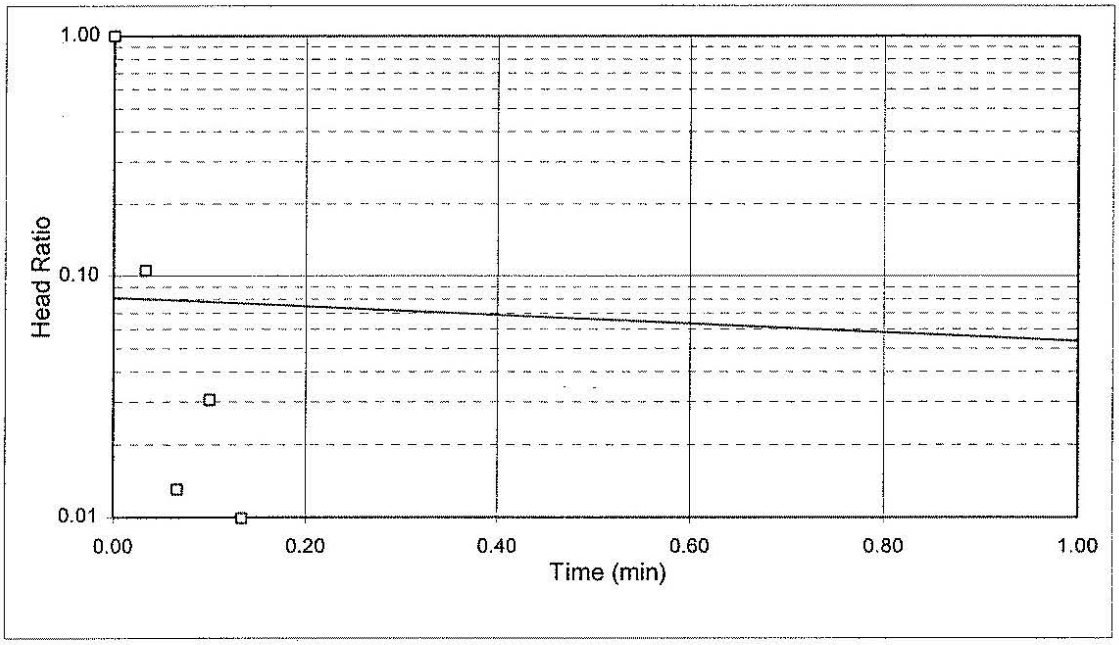
DATALOGGER TIME				TRANSDUCER TR1	ELAPSED TIME	DEPTH TO WATER	HEAD	HEAD RATIO
YEAR	DAY	HR-MIN	SEC	(FEET H_2O)	(MIN)	(FEET)	(FEET)	
305	305	1003	47	10.744	6.28	27.18	0.00	0.00
305	305	1003	48	10.745	6.30	27.19	0.00	0.00
305	305	1003	49	10.744	6.32	27.18	0.00	0.00
305	305	1003	50	10.743	6.33	27.18	0.00	0.00
305	305	1003	51	10.745	6.35	27.19	0.00	0.00
305	305	1003	52	10.745	6.37	27.19	0.00	0.00
305	305	1003	53	10.745	6.38	27.19	0.00	0.00
305	305	1003	54	10.744	6.40	27.18	0.00	0.00
305	305	1003	55	10.745	6.42	27.19	0.00	0.00
305	305	1003	56	10.744	6.43	27.18	0.00	0.00
305	305	1003	57	10.743	6.45	27.18	0.00	0.00
305	305	1003	58	10.744	6.47	27.18	0.00	0.00
305	305	1003	59	10.744	6.48	27.18	0.00	0.00
305	305	1004	0	10.745	6.50	27.19	0.00	0.00
305	305	1004	1	10.745	6.52	27.19	0.00	0.00
305	305	1004	2	10.745	6.53	27.19	0.00	0.00
305	305	1004	3	10.745	6.55	27.19	0.00	0.00
305	305	1004	4	10.743	6.57	27.18	0.00	0.00
305	305	1004	5	10.744	6.58	27.18	0.00	0.00
305	305	1004	6	10.745	6.60	27.19	0.00	0.00
305	305	1004	7	10.746	6.62	27.19	0.01	0.00
305	305	1004	8	10.745	6.63	27.19	0.00	0.00

HVORSLEV SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-305-AI

$$K = \frac{r_c^2}{2L_e} \ln \frac{L_e}{R_e} \left[\frac{\ln\left(\frac{h_1}{h_2}\right)}{(t2 - t1)} \right] 30.48$$

where: r_c = casing radius (feet);
R_e = equivalent radius (feet);
L_e = length of screened interval (feet);
t = time (seconds); and,
h_t = head at time t (feet).

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
R_e =	0.34			
L_e =	14.1	K=	1.93E-04	cm/sec
t_1 (min) =	0	K=	5.46E-01	ft/day
t_2 (min) =	1.00			
h_1/h_0 =	0.08			
h_2/h_0 =	0.05			



Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/31/95

Analysis By: CVK
Checked By:
Analysis Date: 1/22/96

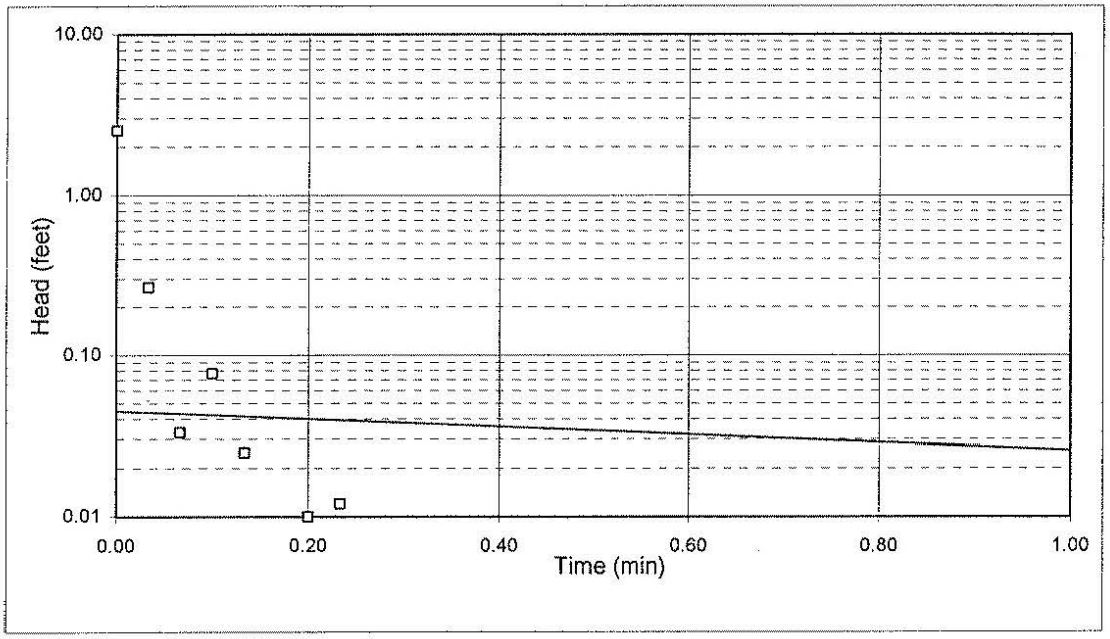
BOUWER AND RICE SLUG TEST ANALYSIS
FALLING HEAD TEST PZ-305-AI

$$K = \frac{r_c^2 \ln\left(\frac{R_e}{r_w}\right)}{2L_e} \frac{1}{t} \ln\frac{y_0}{y_t}$$

where:

r_c = casing radius (feet);
R_e = effective radius (feet);
L_e = length of screened interval (feet);
r_w = radial distance to undisturbed aquifer (feet)
y_0 = initial drawdown (feet)
y_t = drawdown (feet) at time t (minutes)

INPUT PARAMETERS		RESULTS		
r_c =	0.08			
r_w =	0.34			
L_e =	14.1	K=	1.72E-04	cm/sec
$\ln(R_e/r_w)$	2.49	K=	4.89E-01	ft/day
y_0 =	0.04			
y_t =	0.03			
t =	1.00			

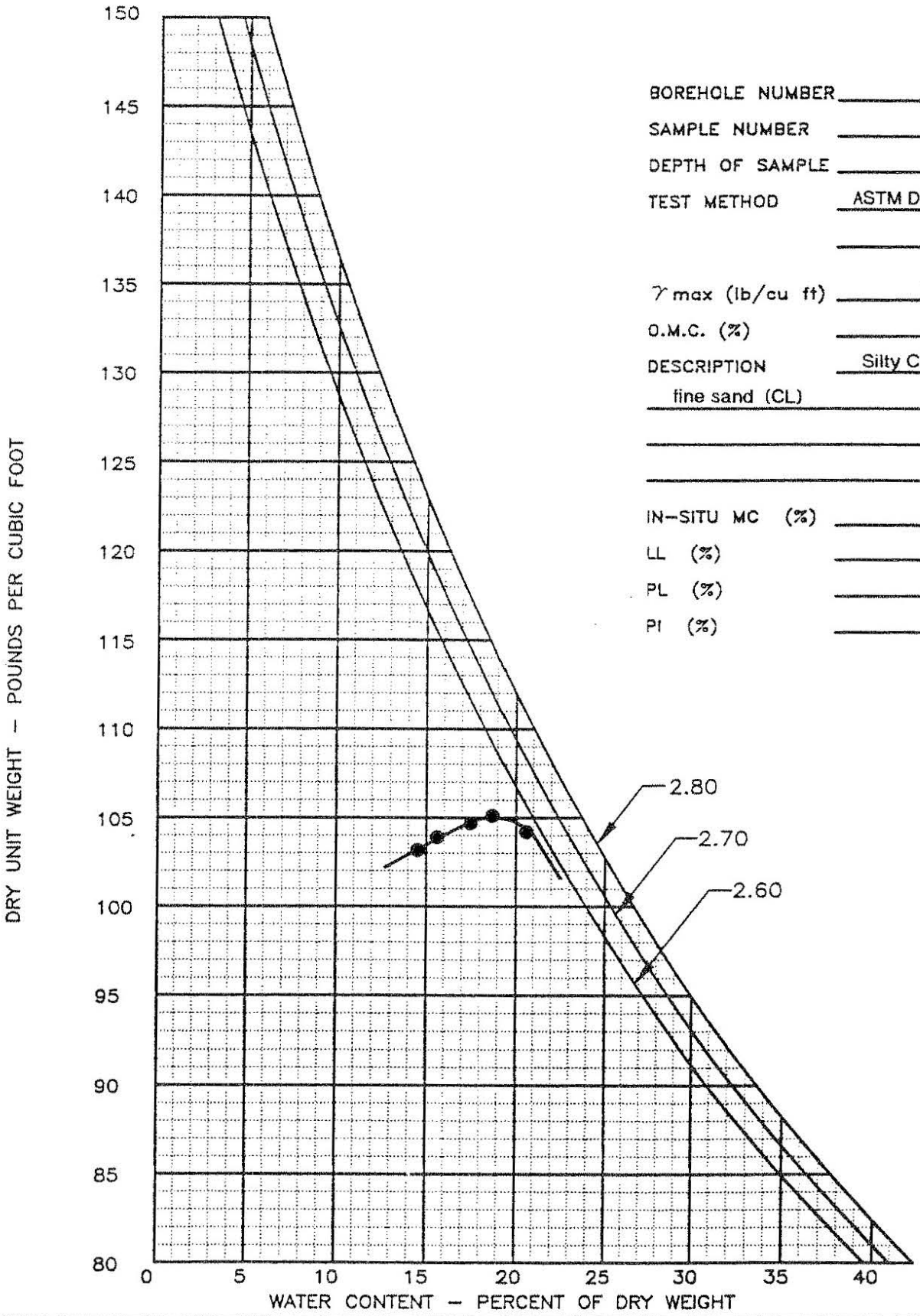


Project Name: LAIDLAW / OU-2 RIFS / MO
Project No.: 943-2848
Test Date: 10/31/95

Analysis By: CVK
Checked By:
Analysis Date: 1/22/96

APPENDIX D

GEOTECHNICAL TEST DATA



BOREHOLE NUMBER

SAMPLE NUMBER PS-1

DEPTH OF SAMPLE

TEST METHOD ASTM D698 METHOD A

γ max (lb/cu ft) 105.0

O.M.C. (%) 19.0

DESCRIPTION Silty CLAY with trace fine sand (CL)

IN-SITU MC (%) 23.0

LL (%) 47

PL (%) 17

PI (%) 30

Golder Associates Denver, Colorado

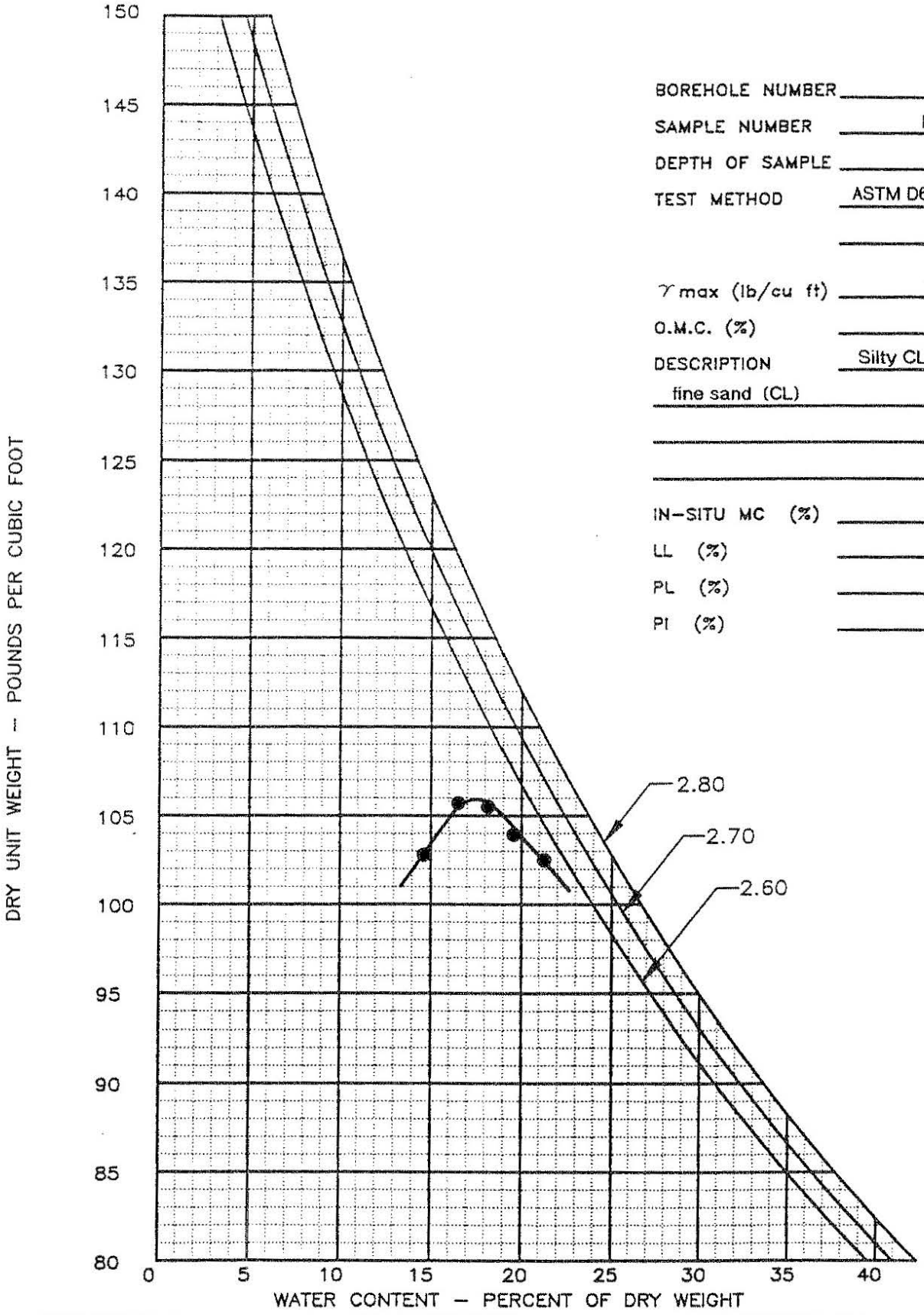
TITLE

PROCTOR CURVE SAMPLE #PS-1

CLIENT/PROJECT

LAIDLAW/OU2 RIFS/MO

DRAWN	ASF	DATE	JULY 1995	JOB NO.	943-2848.202
CHECKED	KMR	SCALE	AS SHOWN	DWG NO./REV. NO.	
REVIEWED		FILE NO.	WATER.DWG	FIGURE NO.	



BOREHOLE NUMBER

SAMPLE NUMBER PS-2

DEPTH OF SAMPLE

TEST METHOD ASTM D698 METHOD A

γ max (lb/cu ft) 106.0

O.M.C. (%) 17.5

DESCRIPTION Silty CLAY with trace fine sand (CL)

IN-SITU MC (%) 25.9

LL (%) 39

PL (%) 22

PI (%) 17

Golder Associates Denver, Colorado

TITLE

PROCTOR CURVE SAMPLE #PS-2

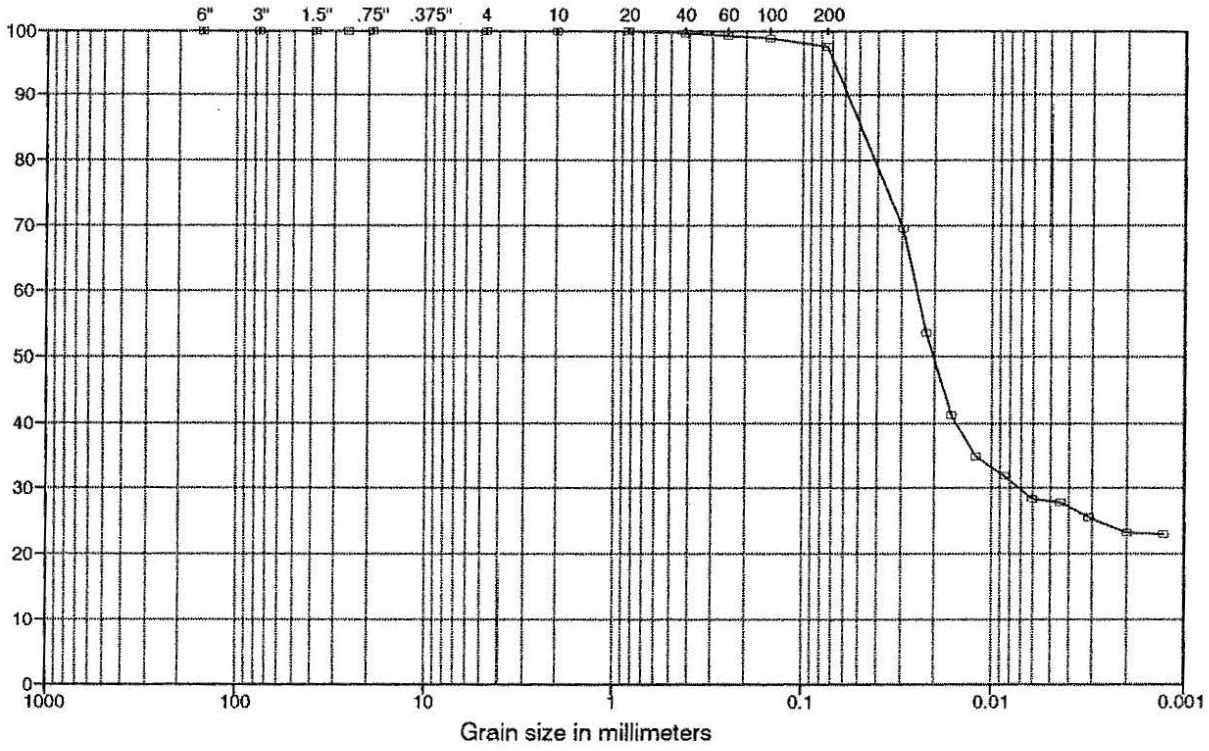
CLIENT/PROJECT

LAIDLAW/OU2 RIFS/MO

DRAWN	ASF	DATE	JULY 1995	JOB NO.	943-2848.202
CHECKED	KMR	SCALE	AS SHOWN	DWG NO./REV. NO.	
REVIEWED		FILE NO.	WATER.DWG	FIGURE NO.	

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



% PASSING

USCS

COBBLES	GRAVEL		SAND			FINES (Silt and Clay)
	Coarse	Fine	Cor	Med	Fine	

SAMPLE ID	W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE SAMPLE NO. PS-2 DEPTH	25.9	39	22	17	2.81	Silty CLAY with trace fine sand

Sample Type: Date Tested: 6/28/95 USCS: CL

TECH: BRB
DATE: 07/11/95
CHECKED: ASF
REVIEWED:

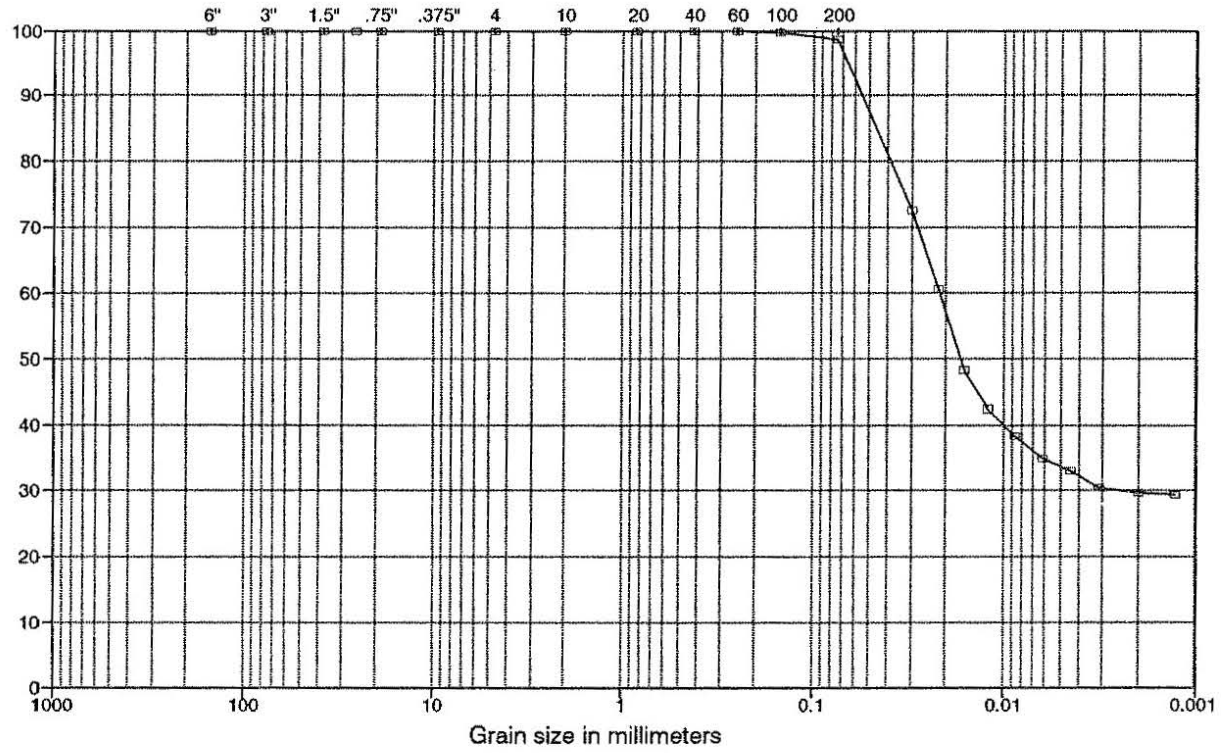
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2848PS2

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	COBBLES	Coarse	Fine	Cor	Med	Fine	FINES (Silt and Clay)
		GRAVEL		SAND			

SAMPLE ID	W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE SAMPLE NO. PS-1 DEPTH	23.0	47	17	30	2.74	Silty CLAY with trace fine sand

Sample Type: Date Tested: 6/28/95 USCS: CL

TECH: BRB
DATE: 07/11/95
CHECKED: ASF
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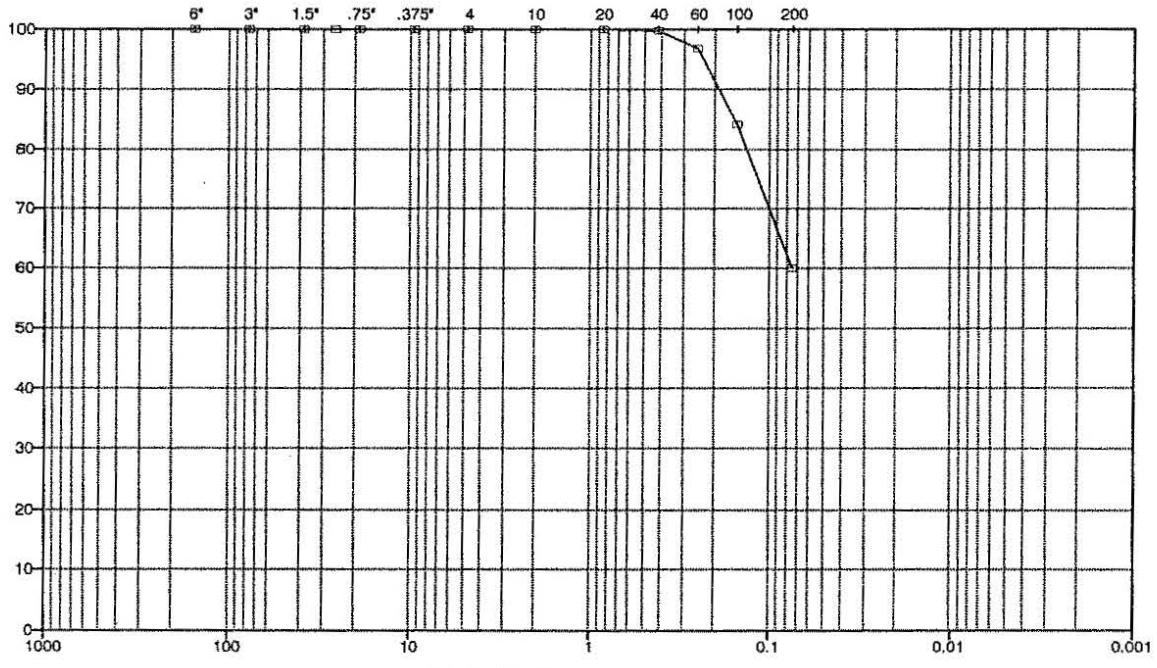
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2848PS1

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS

	Coarse	Fine	C	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt or Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE	PZ-208-SS	--	--	--	--	--	FINES and fine SAND
SAMPLE NO.							
DEPTH (FT.)	10-12'						

Sample Type: Date Tested: 6/29/95 USCS: --

TECH: HM
DATE: 07/11/95
CHECKED: ASF
REVIEWED:

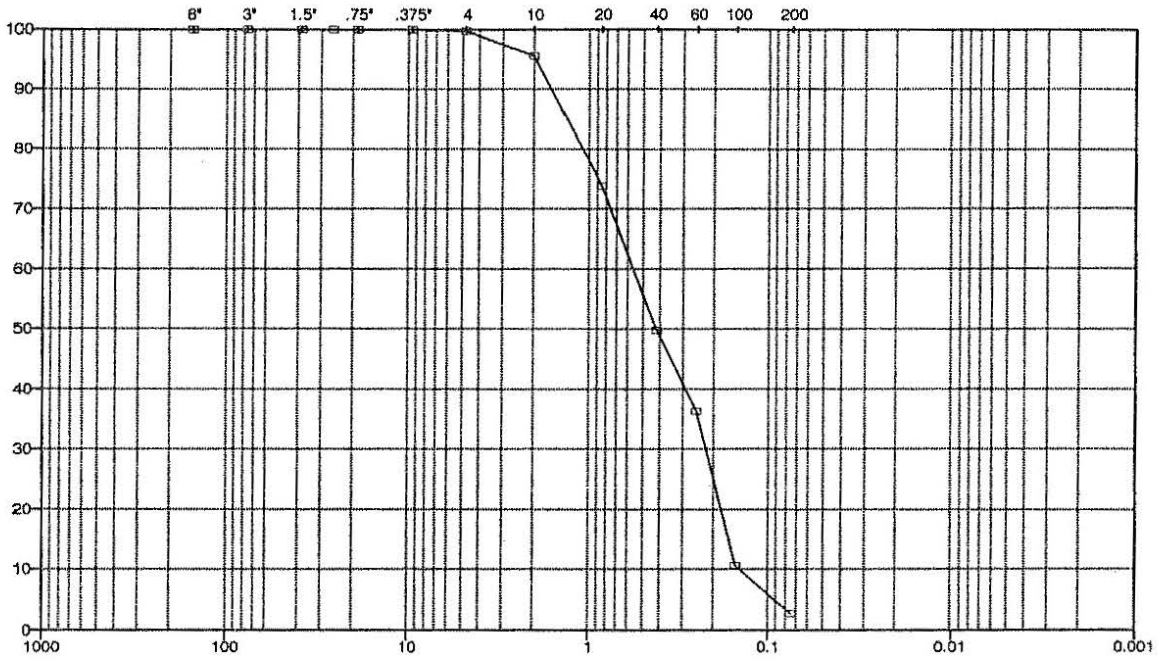
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2848204

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS

	Coarse	Fine	C	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt or Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		17.0%	--	--	--	--	Coarse to fine SAND with trace fines
SAMPLE NO.	PZ-207AS						
DEPTH (FT.)	36.0-38.0						
Sample Type:		Date Tested: 4/28/95					USCS: SP

TECH: KRF
DATE: 07/11/95
CHECKED: ASF
REVIEWED:

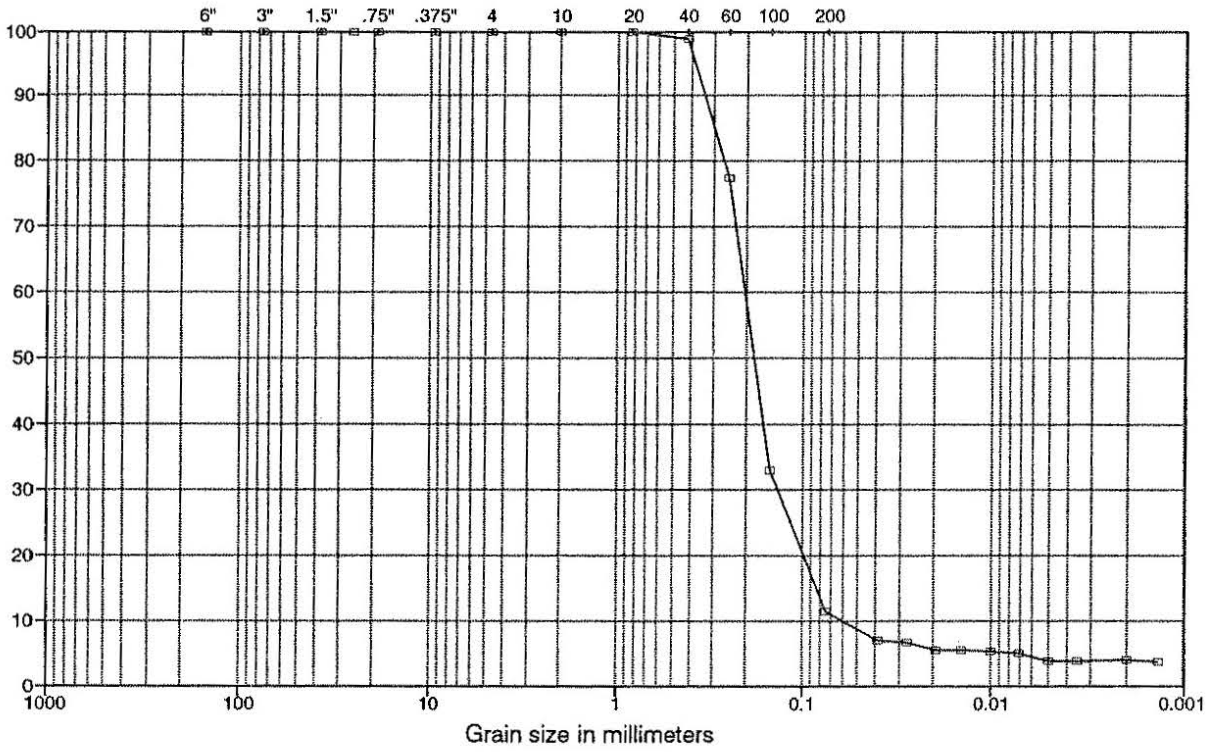
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2848207

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	COBBLES	Coarse GRAVEL	Fine GRAVEL	Cor SAND	Med SAND	Fine SAND	FINES (Silt and Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE			--	NP	NP	2.62	Medium to fine SAND with little silt
SAMPLE NO.	PZ-206-SS						
DEPTH	8-10,32-34						

Sample Type: Date Tested: 4/6/95 USCS: SP-SM

TECH: GI
DATE: 07/11/95
CHECKED: ASF
REVIEWED:

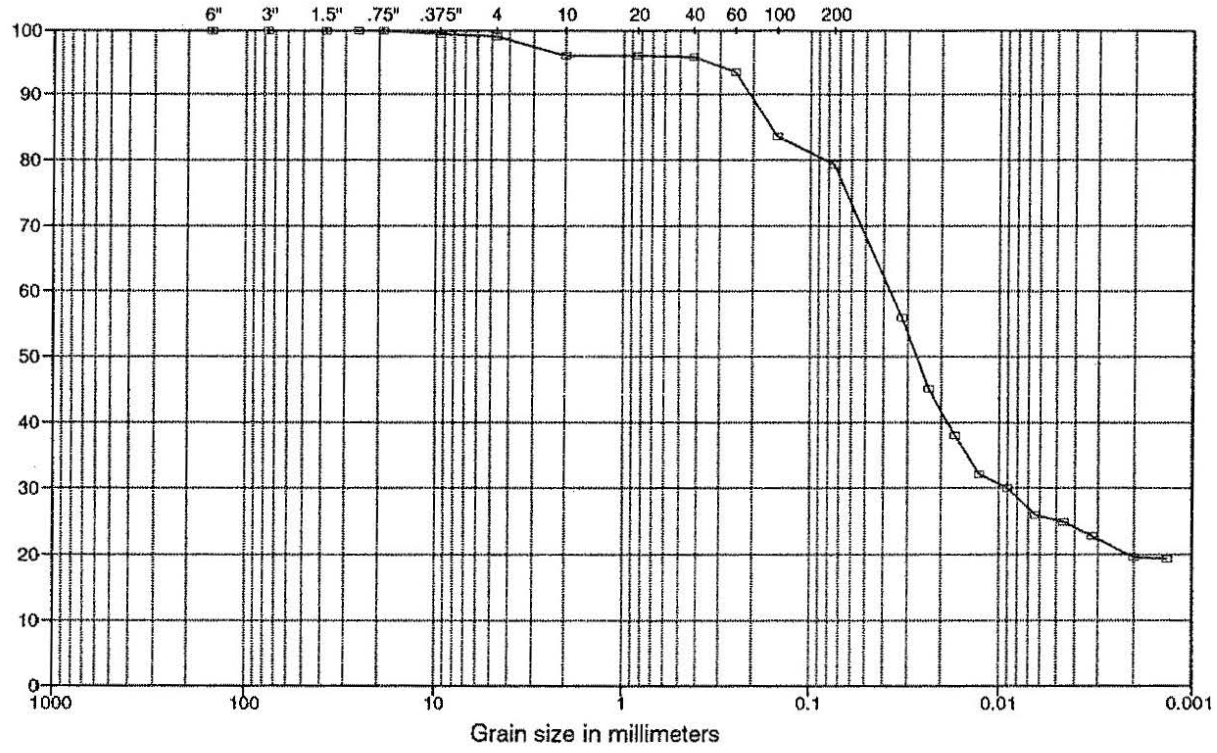
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2844206

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	COBBLES	GRAVEL		SAND			FINES (Silt and Clay)
		Coarse	Fine	Cor	Med	Fine	

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE	PZ-205-AS	--	--	--	--	2.68	SILT with some coarse to fine sand, trace fine gravel
SAMPLE NO.							
DEPTH	31-33'						

Sample Type: Date Tested: 6/28/95 USCS: ML

TECH: BRB
DATE: 07/11/95
CHECKED: ASF
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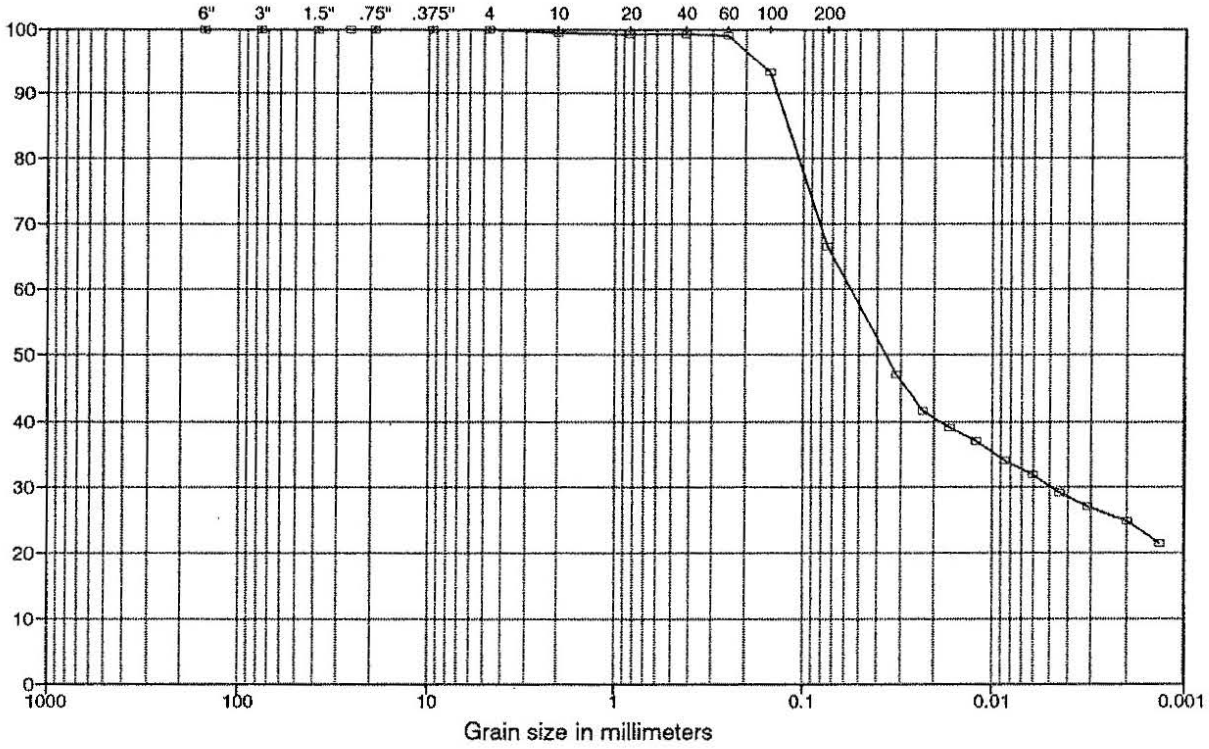
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2444205B

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS

COBBLES	Coarse	Fine	Cor	Med	Fine	FINES (Silt and Clay)
	GRAVEL		SAND			

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE	PZ-205-AS	--	--	--	--	2.81	FINES and coarse to fine SAND
SAMPLE NO.							
DEPTH	41-43'						

Sample Type: Date Tested: 6/27/95 USCS: --

TECH: GI
DATE: 07/11/95
CHECKED: ASF
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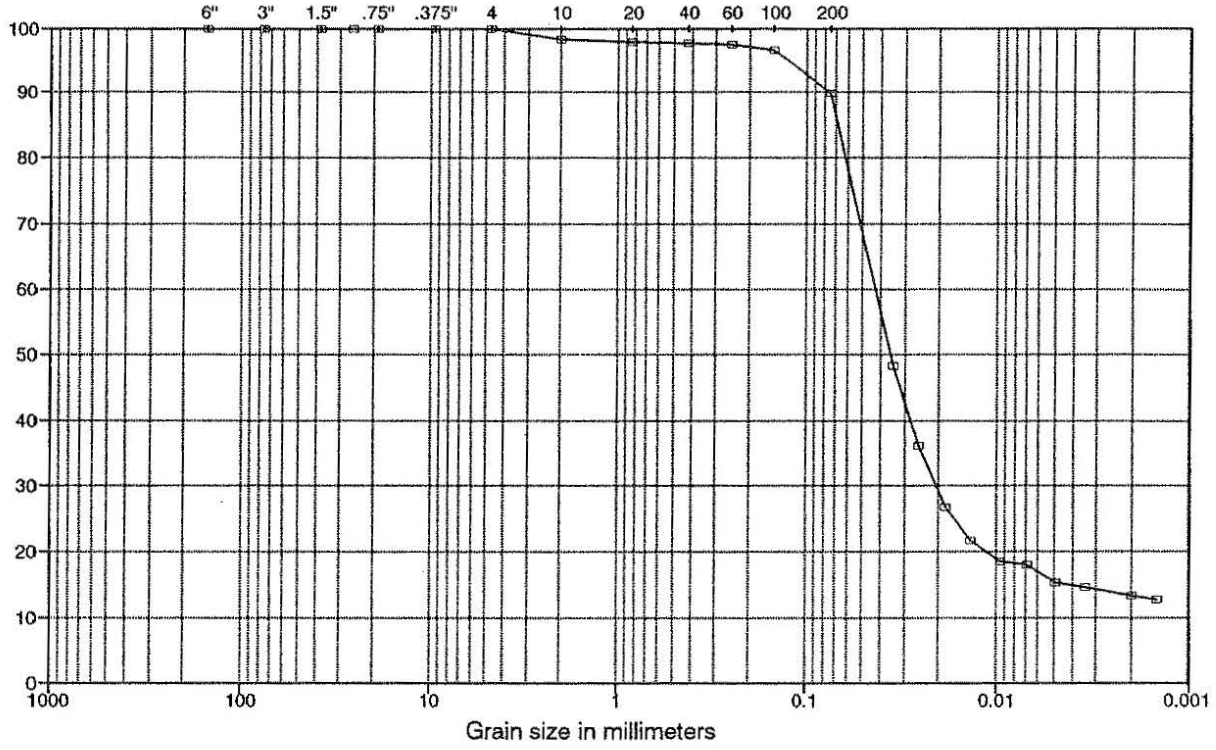
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2848205A

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	Coarse	Fine	Cor	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt and Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE			--	--	--	2.64	FINES with little coarse to fine sand
SAMPLE NO.	PZ-205-SS						
DEPTH	28-30						

Sample Type: Date Tested: 4/9/95 USCS: --

TECH: GI
DATE: 07/11/95
CHECKED: ASF
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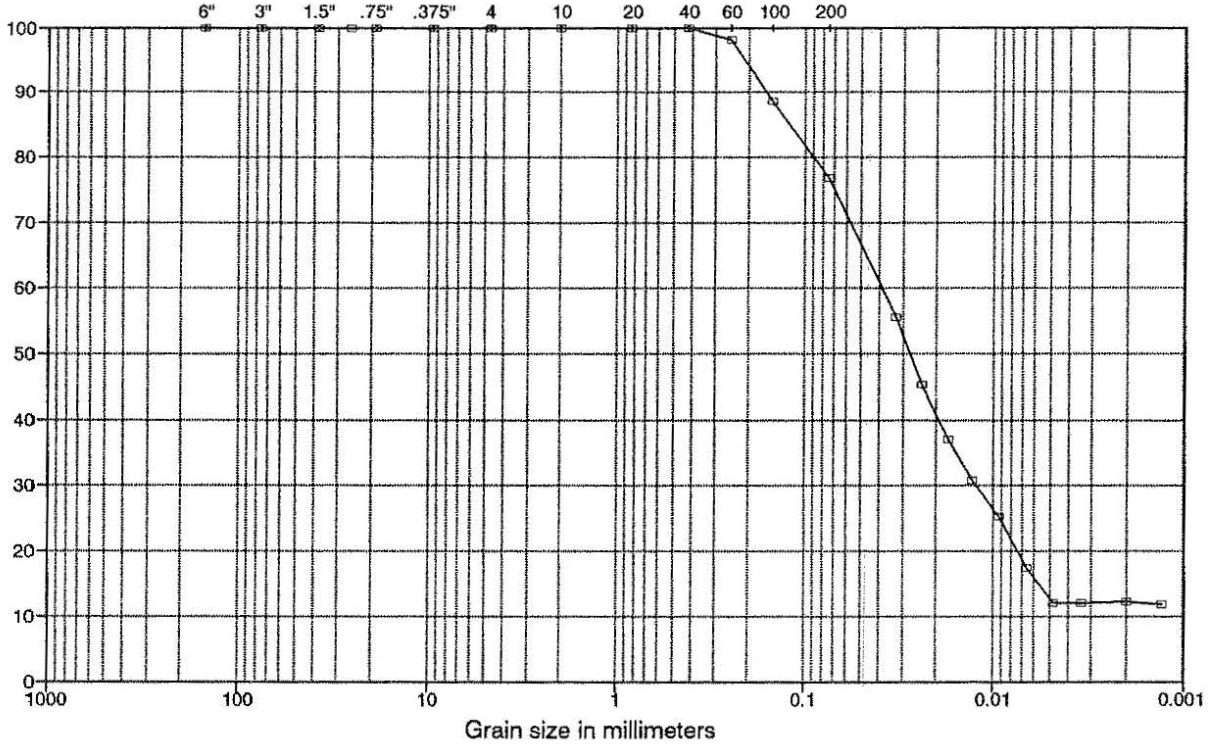
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2848205

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	Coarse	Fine	Cor	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt and Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE			--	NP	NP	2.68	SILT with some fine sand
SAMPLE NO.	PZ-204-SS						
DEPTH	8-10,10-12						

Sample Type: Date Tested: 4/6/95 USCS: ML

TECH: GI
DATE: 07/11/95
CHECKED: ASF
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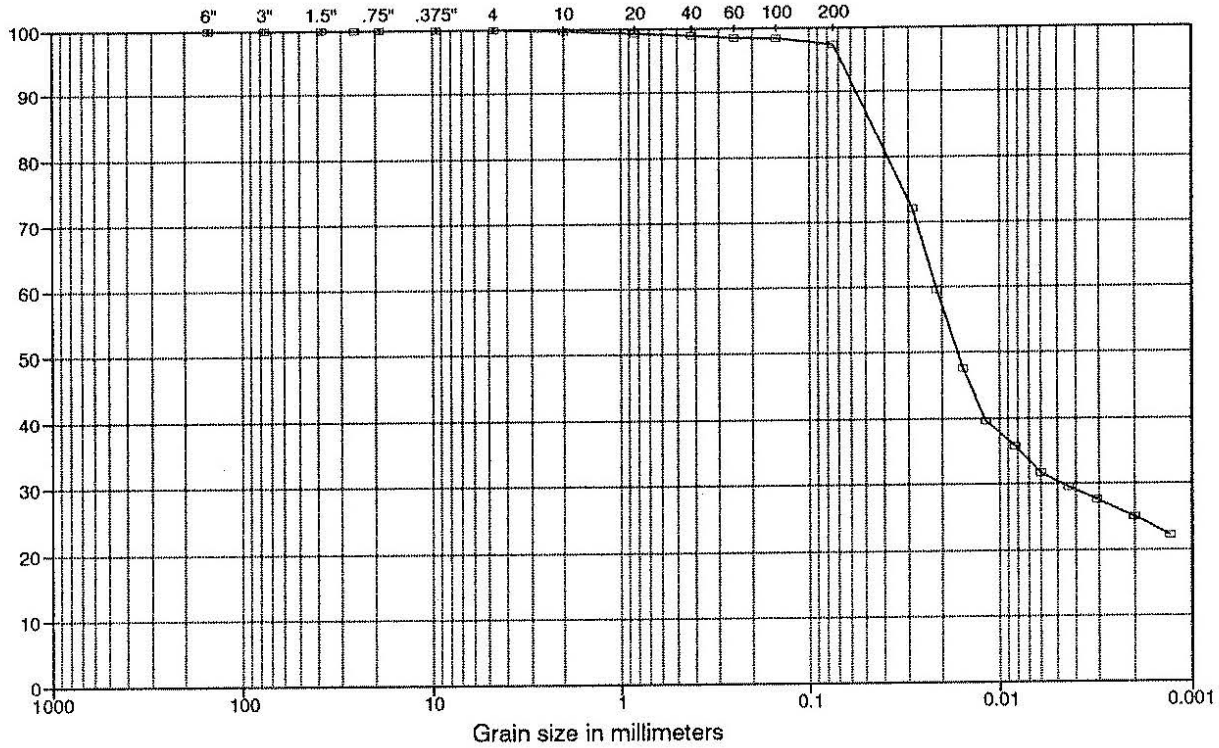
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2845204

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	COBBLES	Coarse	Fine	Cor	Med	Fine	FINES (Silt and Clay)
		GRAVEL		SAND			

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE	PZ-203-SS	--	--	--	--	2.85	FINES with trace medium to fine sand
SAMPLE NO.							
DEPTH	8-10'						

Sample Type: Date Tested: 6/27/95 USCS: --

TECH: GI
DATE: 07/11/95
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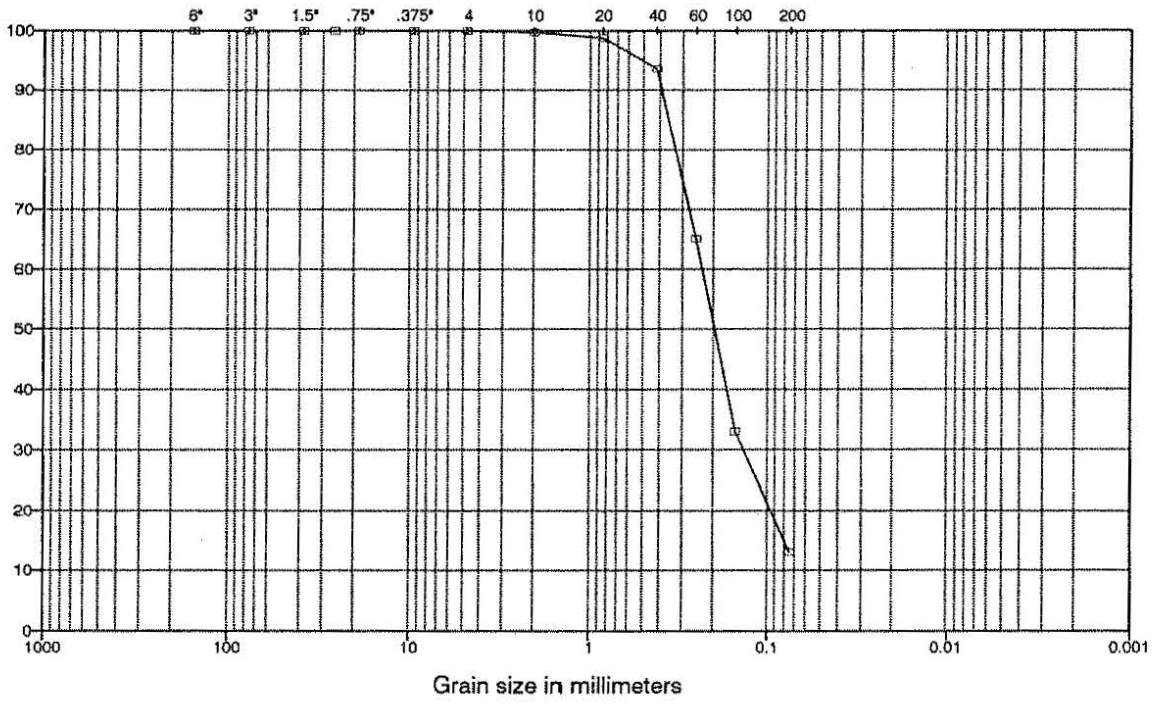
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943-2848.202

FILENAME: 2848203A

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS

	Coarse	Fine	C	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt or Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE	PZ-203-SS	--	--	--	--	--	Medium to fine SAND with some fines
SAMPLE NO.							
DEPTH (FT.)	38-40'						

Sample Type: Date Tested: 6/26/95 USCS: --

TECH: HM
DATE: 07/11/95
CHECKED: ASF
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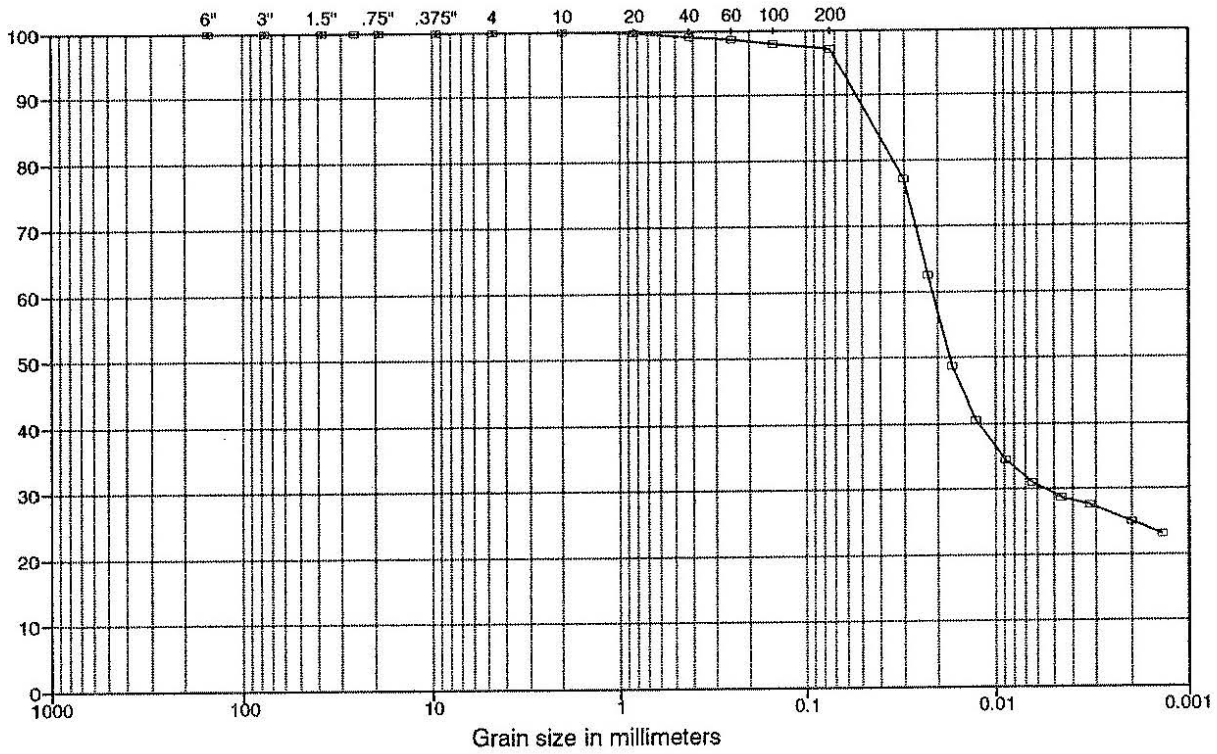
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2648203

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	COBBLES	GRAVEL		SAND			FINES (Silt and Clay)
		Coarse	Fine	Cor	Med	Fine	

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		26.7	45	24	21	2.74	Silty CLAY with trace medium to fine sand
SAMPLE NO.	PZ-202-SS						
DEPTH	6-8,8-10						

Sample Type: Date Tested: 4/9/95 USCS: CL

TECH: GI
DATE: 07/11/95
CHECKED: ASF
REVIEWED:

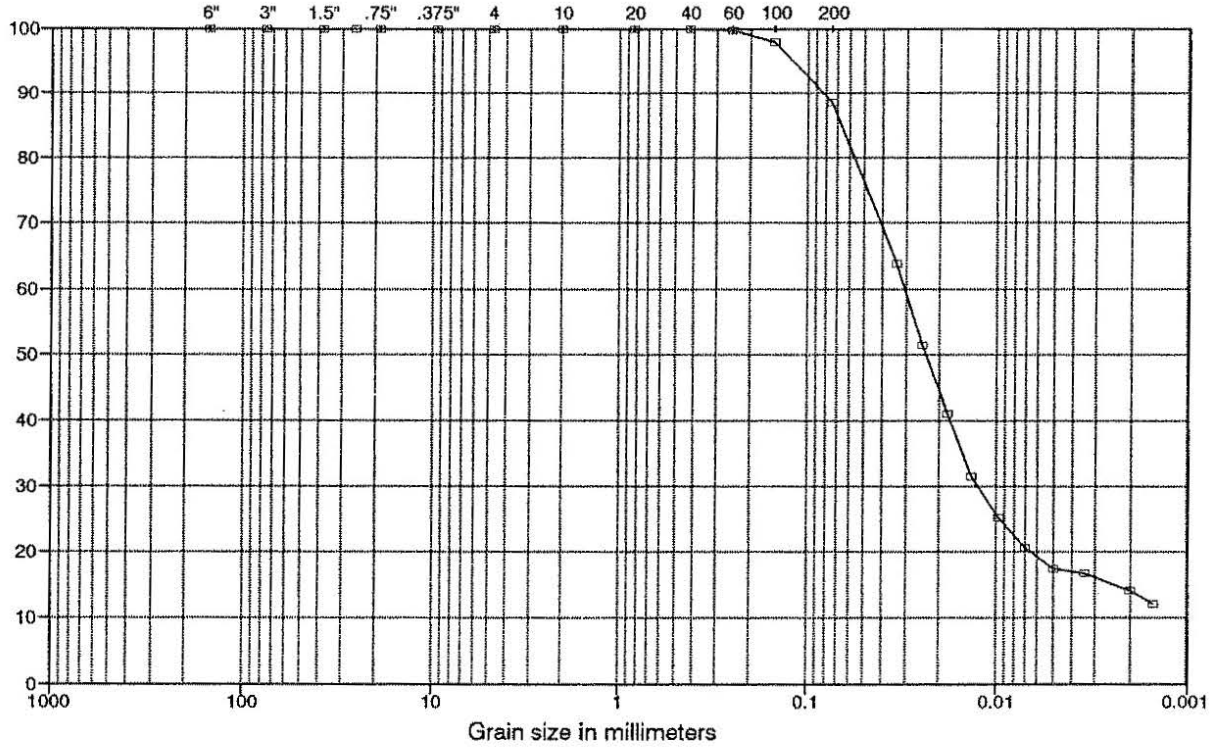
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943-2848.202

FILENAME: 2848202

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS

COBBLES	Coarse	Fine	Cor	Med	Fine	FINES (Silt and Clay)
	GRAVEL		SAND			

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		34.5	--	NP	NP	2.62	SILT with little fine sand
SAMPLE NO.	PZ-201-SS						
DEPTH	24-26,26-28						
Sample Type:		Date Tested: 4/9/95					USCS: ML

TECH: GI
DATE: 07/11/95
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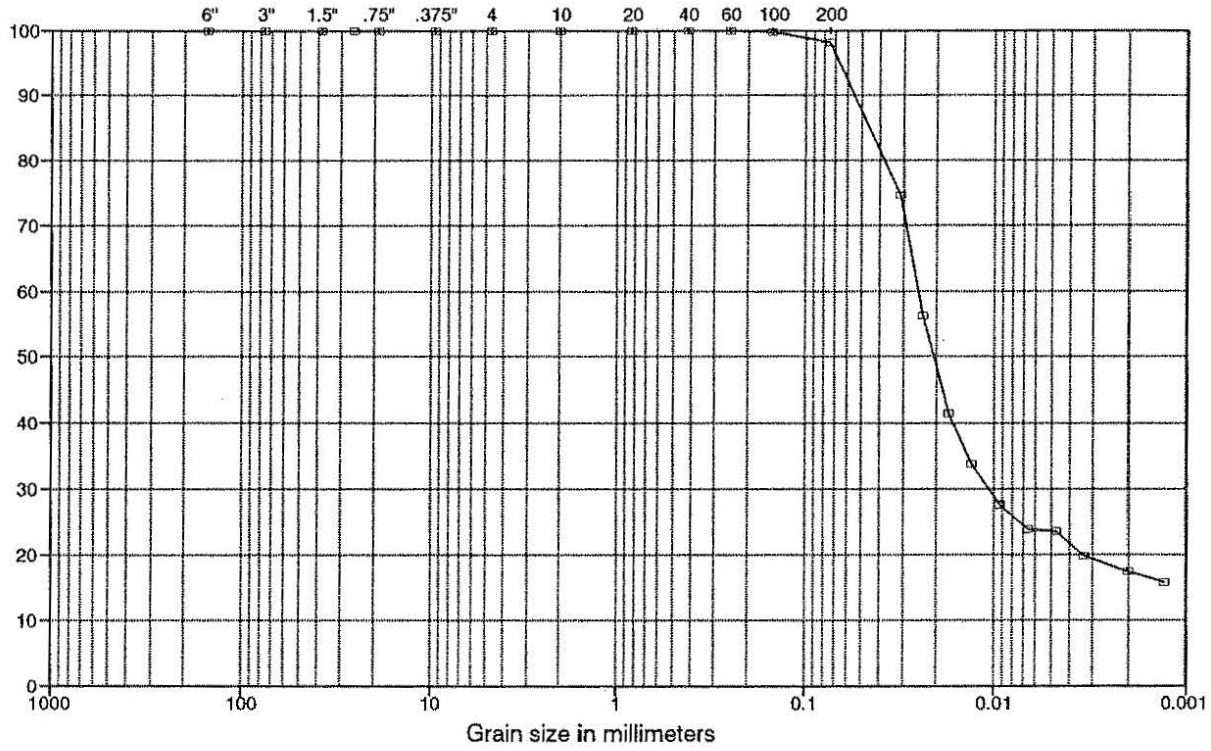
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2848201

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	COBBLES	Coarse	Fine	Cor	Med	Fine	FINES (Silt and Clay)
		GRAVEL		SAND			

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		27.5	36	24	12	2.64	Clayey SILT with trace fine sand
SAMPLE NO.	PZ-200-SS						
DEPTH	6-8,8-10						
Sample Type:		Date Tested: 04/06/95					USCS: CL-ML

TECH: GI
DATE: 07/11/95
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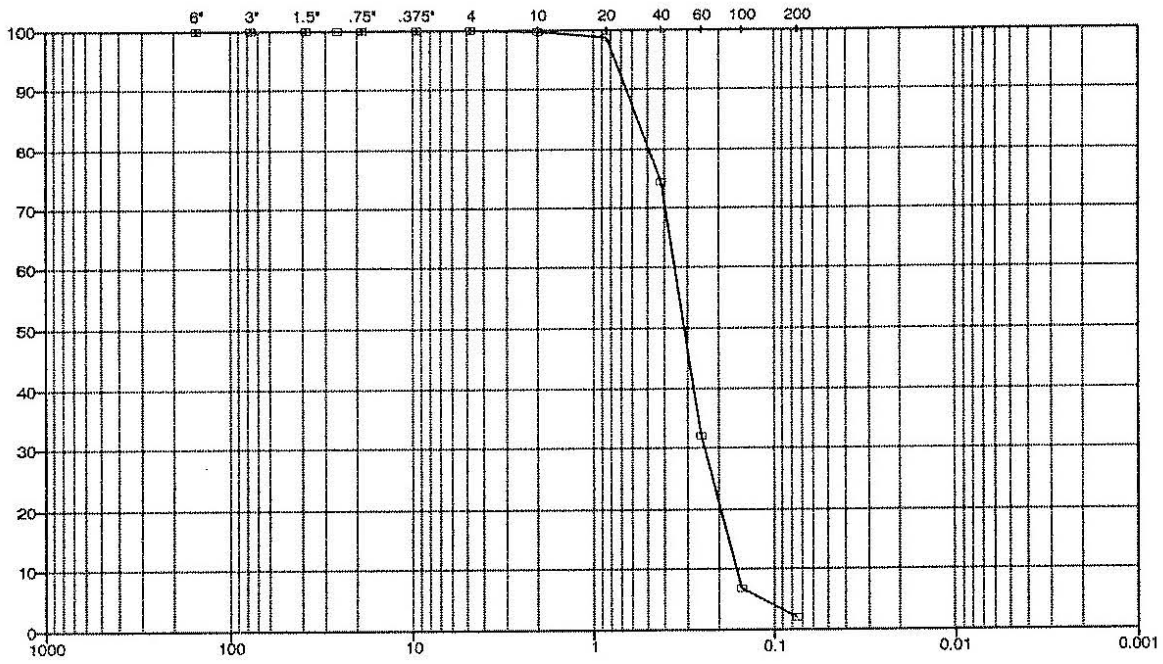
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2848200

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS

COBBLES	Coarse	Fine	C	Med	Fine	FINES (Silt or Clay)
	GRAVEL		SAND			

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE	PZ-116-SS	--	--	--	--	--	Medium to fine SAND with trace fines
SAMPLE NO.							
DEPTH (FT.)	29-31'						
Sample Type:		Date Tested: 6/26/95					USCS: SP

TECH: HM
DATE: 07/11/95
CHECKED: ASF
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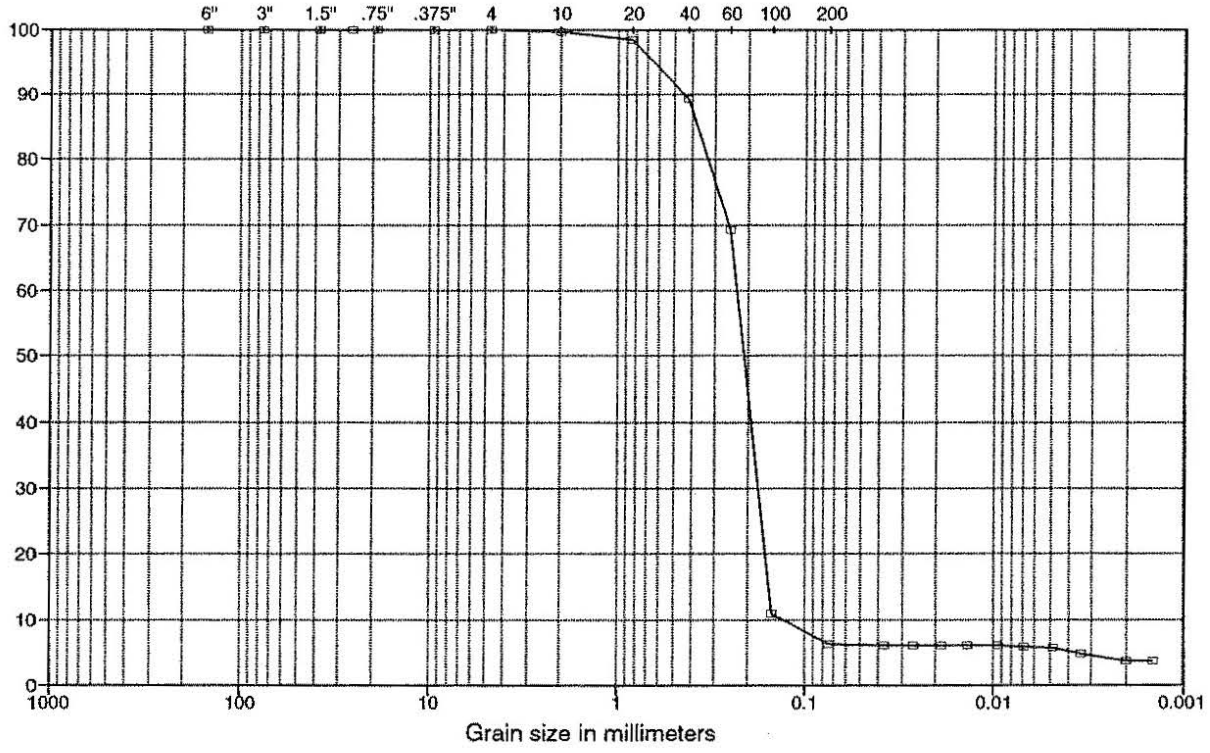
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2848116

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	Coarse	Fine	Cor	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt and Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE	PZ-115-SS	--	--	--	--	2.72	Medium to fine SAND with little fines
SAMPLE NO.							
DEPTH	30-32'						

Sample Type: Date Tested: 6/27/95 USCS: --

TECH: GI
DATE: 07/11/95
CHECKED: ASF
REVIEWED:

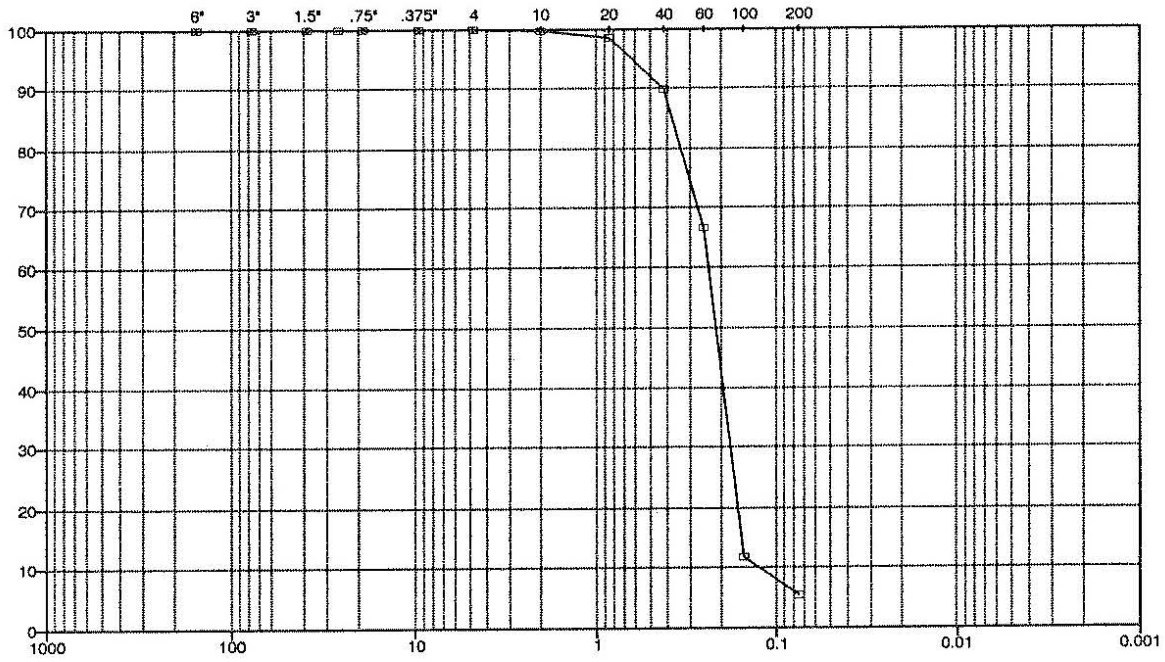
LAIDLAW/OU2 RIFS/MO
943-2848.202

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GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS

	Coarse	Fine	C	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt or Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		17.0%				--	
SAMPLE NO.	PZ-115-SS						
DEPTH (FT.)	30-32'						
Sample Type:		Date Tested:	6/26/95				USCS:

TECH: HM
DATE: 07/11/95
CHECKED: ASF
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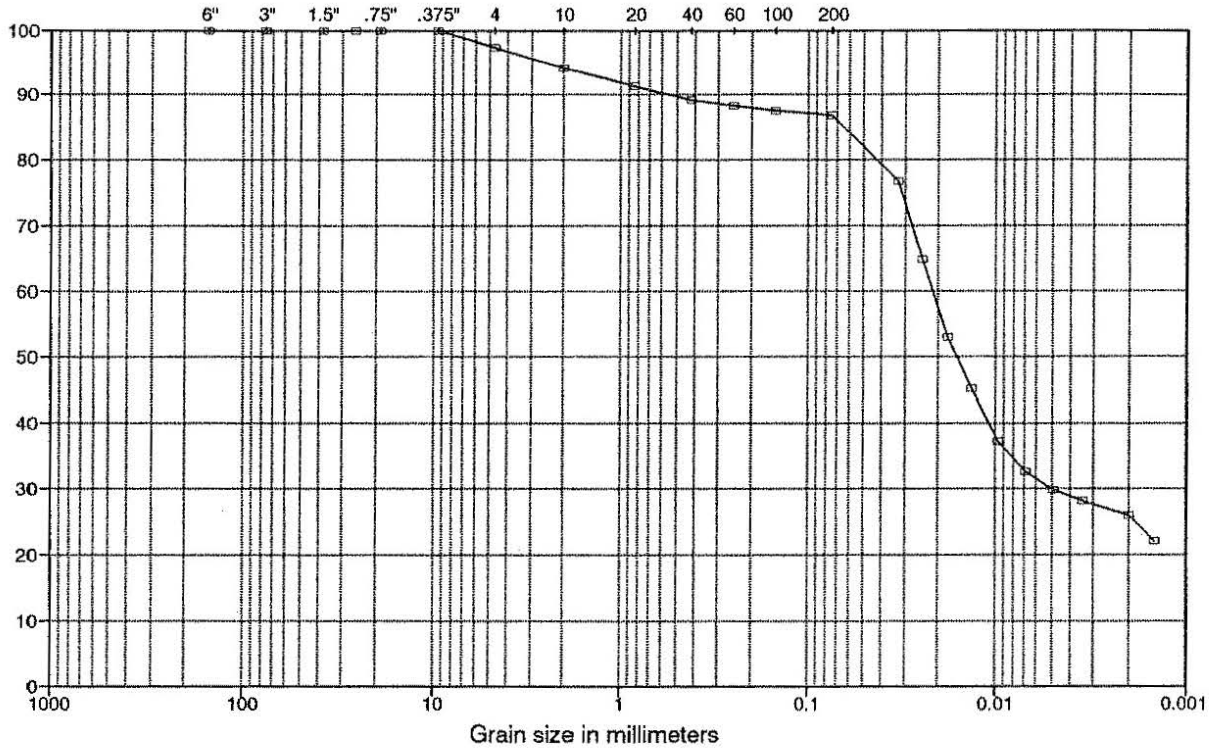
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2848115

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS

COBBLES	Coarse	Fine	Cor	Med	Fine	FINES (Silt and Clay)
	GRAVEL		SAND			

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		33.2	40	24	16	2.51	Silty CLAY with little coarse to fine
SAMPLE NO.	PZ-114-AS						sand, trace fine gravel
DEPTH	12.0-14.0						

Sample Type: Date Tested: 4/29/95 USCS: CL

TECH: GI
DATE: 07/11/95
CHECKED: ASF
REVIEWED:

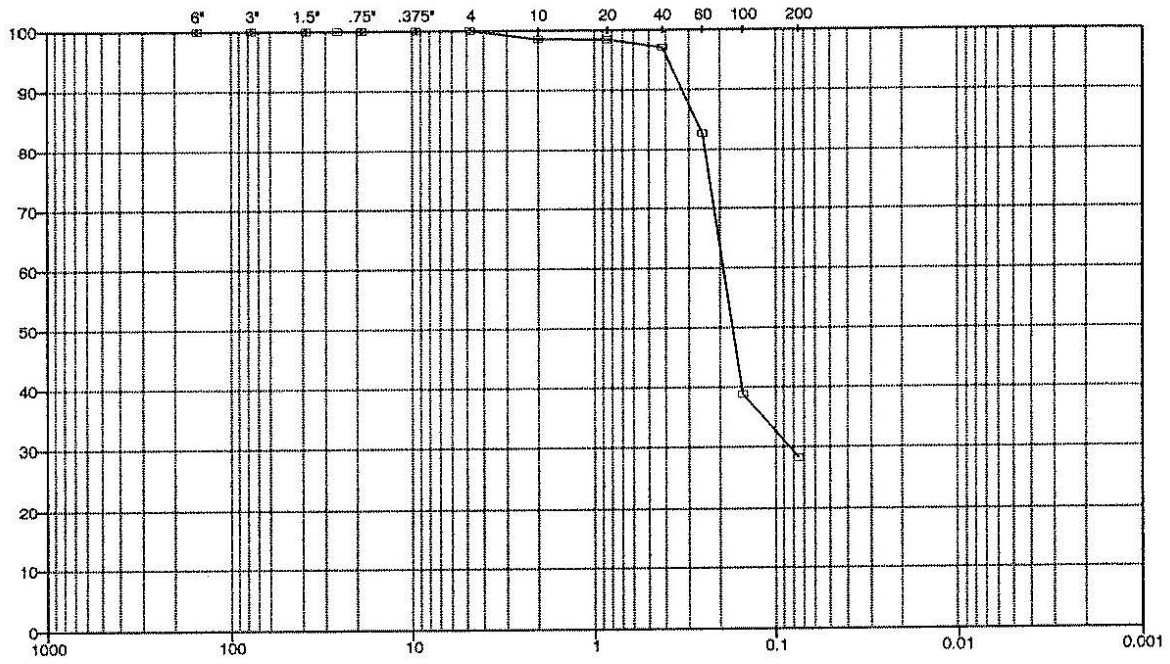
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2848114A

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS

	Coarse	Fine	C	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt or Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		20.3%	--	--	--	--	Coarse to fine SAND with some fines
SAMPLE NO.	PZ-114AS						
DEPTH (FT.)	24.0-26.0						

Sample Type: Date Tested: 4/28/95 USCS: --

TECH: KRF
DATE: 07/11/95
CHECKED: ASF
REVIEWED:

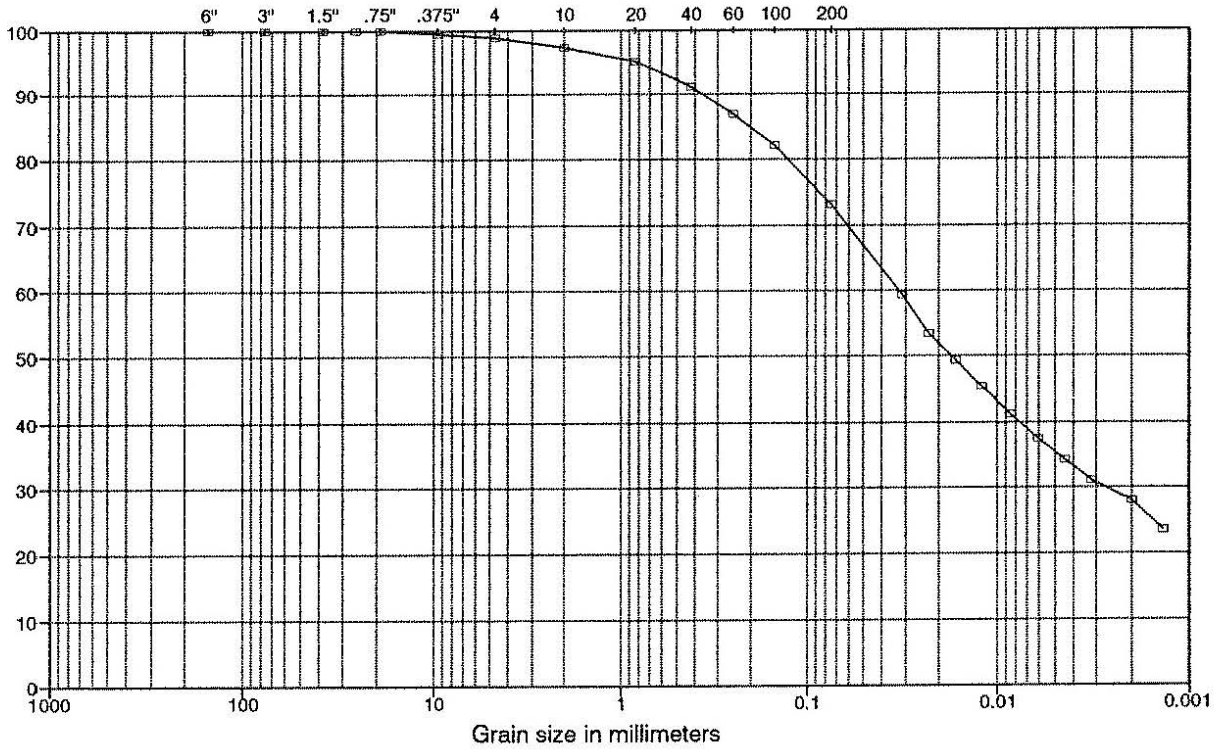
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2848114

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	Coarse	Fine	Cor	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt and Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE	PZ-113-AS	--	--	--	--	2.69	FINES with some coarse to fine sand
SAMPLE NO.							
DEPTH	8-10'						

Sample Type: Date Tested: 6/27/95 USCS: --

TECH: GI
DATE: 07/11/95
CHECKED: ASF
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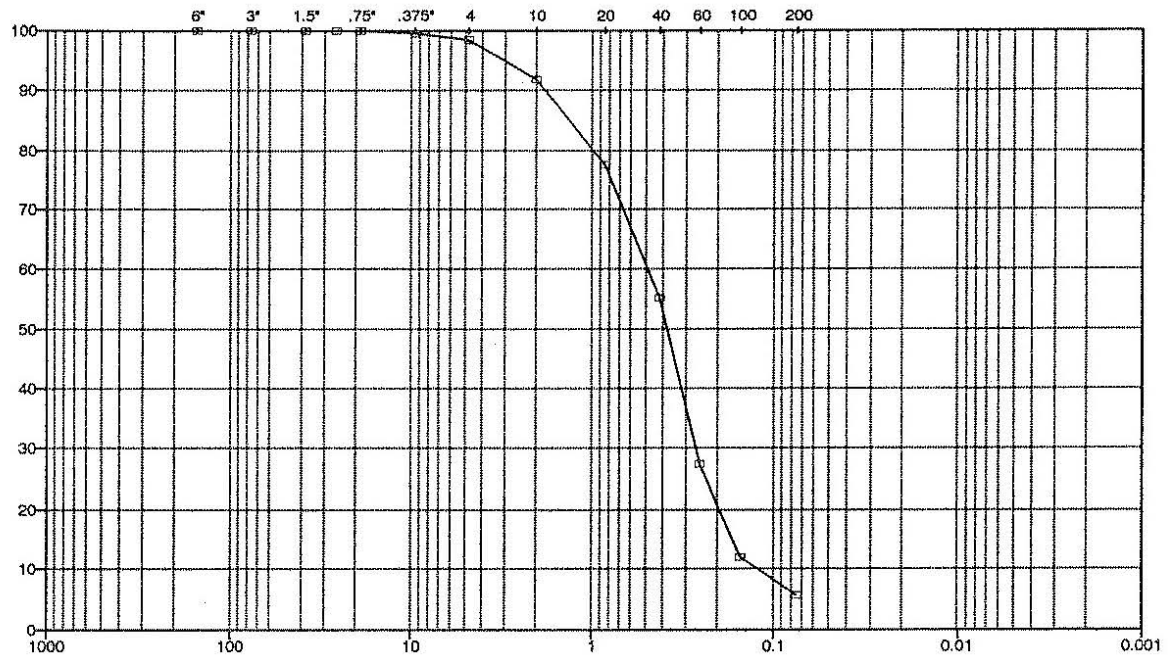
LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2848113D

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS						
	Coarse	Fine	C	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt or Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE	PZ-113-AS	--	--	--	--	--	Coarse to fine SAND with little fines,
SAMPLE NO.							trace fine gravel
DEPTH (FT.)	94-96'						
Sample Type:		Date Tested: 6/26/95					USCS: --

TECH: HM
DATE: 07/11/95
CHECKED: ASF
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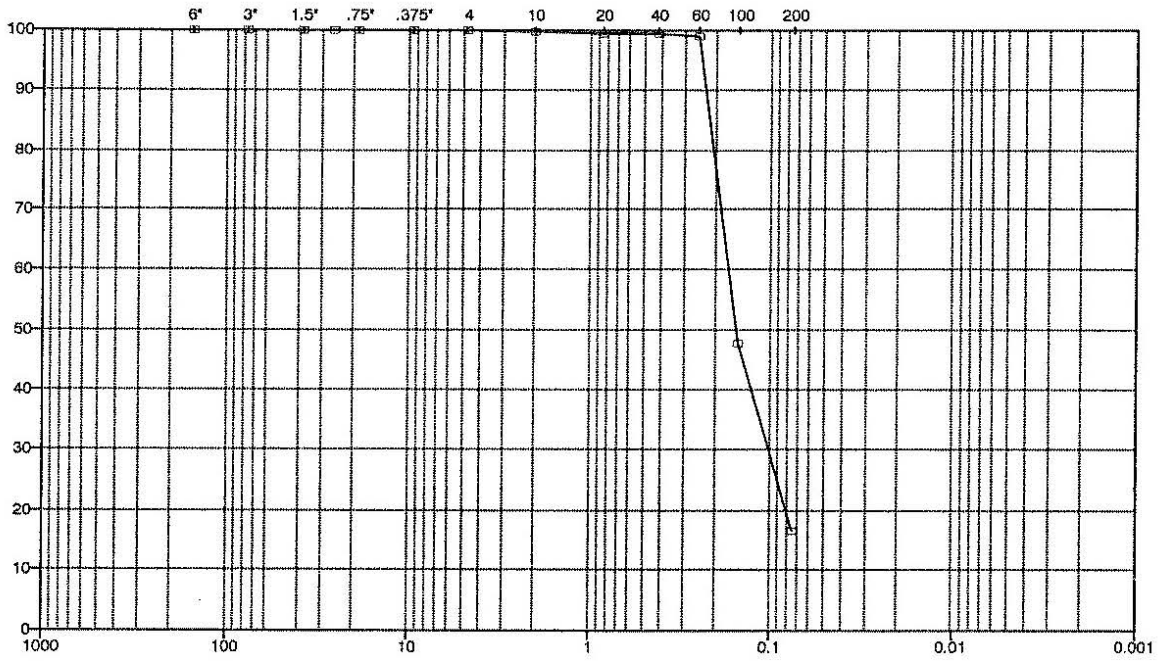
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FILENAME: 2848113C

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS

	Coarse	Fine	C	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt or Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE	PZ-113-AS	--	--	--	--	--	Fine SAND with some fines
SAMPLE NO.							
DEPTH (FT.)	28-30'						

Sample Type: Date Tested: 6/26/95 USCS: --

TECH: HM
DATE: 07/11/95
CHECKED: ASF
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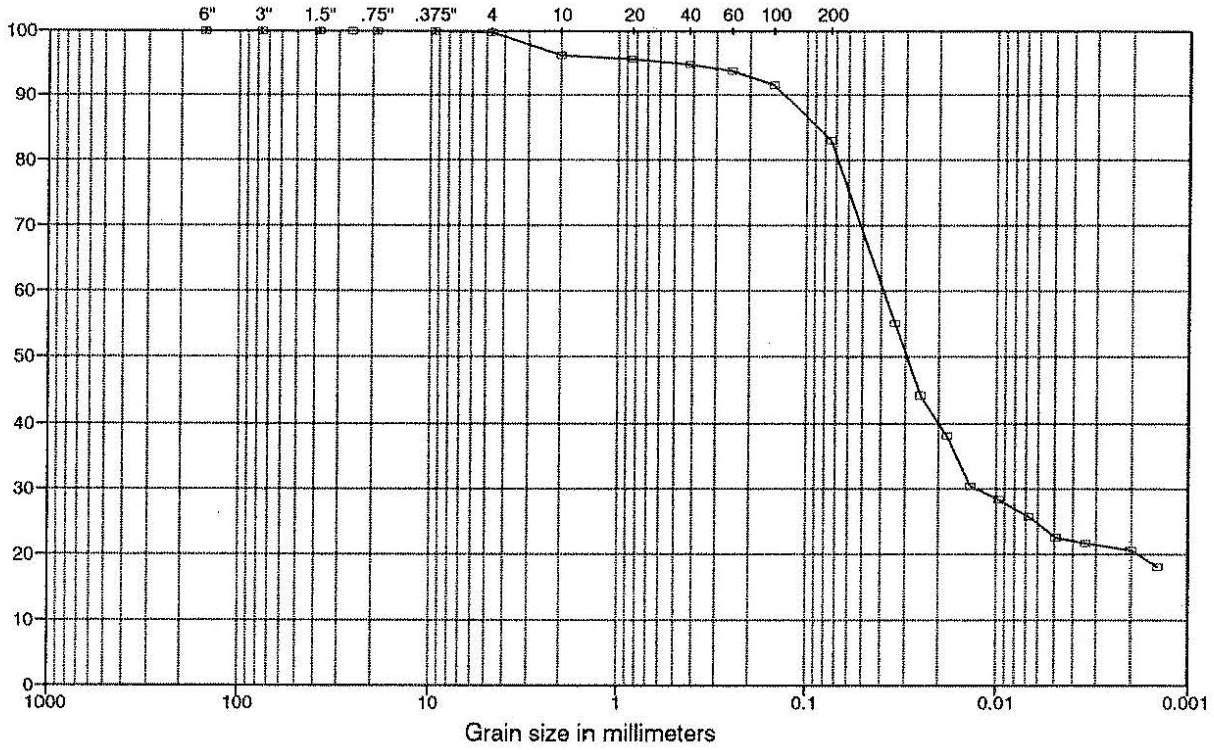
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943-2848.202

FILENAME: 2845113B

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS

COBBLES	GRAVEL		SAND			FINES (Silt and Clay)
	Coarse	Fine	Cor	Med	Fine	

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		20.1	32	23	9	2.62	Silty CLAY with some coarse to fine sand
SAMPLE NO.	PZ-113-AS						
DEPTH	10.0-12.0						

Sample Type: Date Tested: 4/29/95 USCS: CL

TECH: GI
DATE: 07/11/95
CHECKED: ASF
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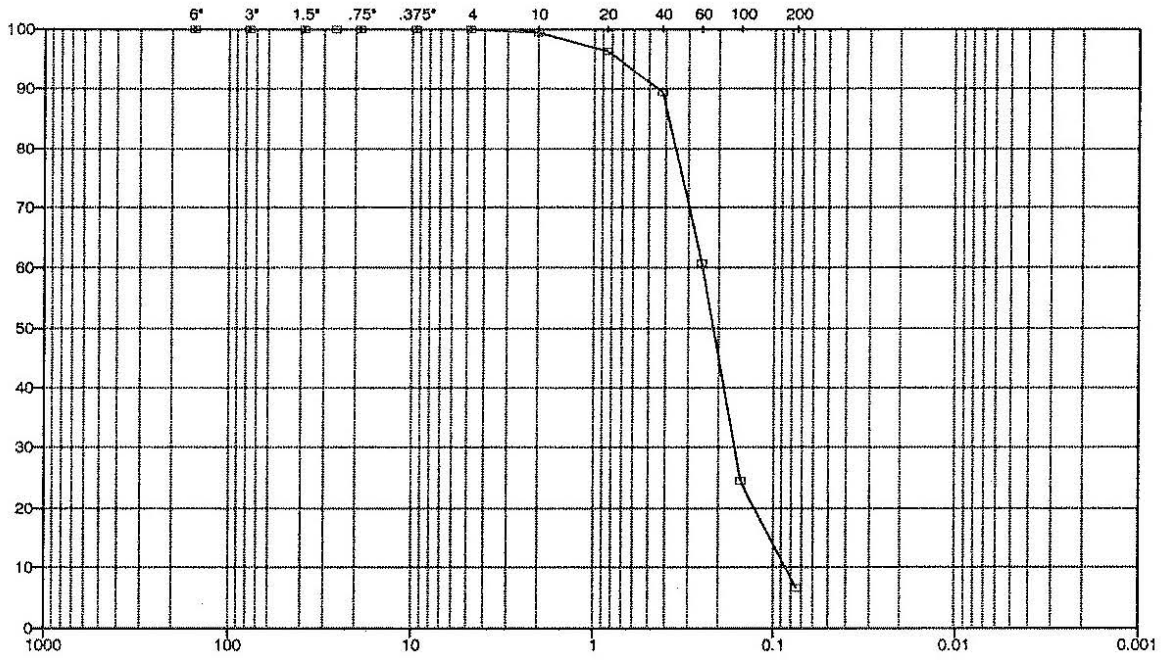
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943-2848.202

FILENAME: 2848113A

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS

COBBLES	Coarse	Fine	C	Med	Fine	FINES (Silt or Clay)
	GRAVEL		SAND			

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		18.0%	--	--	--	--	Coarse to fine SAND with little fines
SAMPLE NO.	PZ-113AS						
DEPTH (FT.)	34.0-36.0						
Sample Type:		Date Tested: 4/28/95					USCS: SP-SM

TECH: KRF
DATE: 07/11/95
CHECKED: ASF
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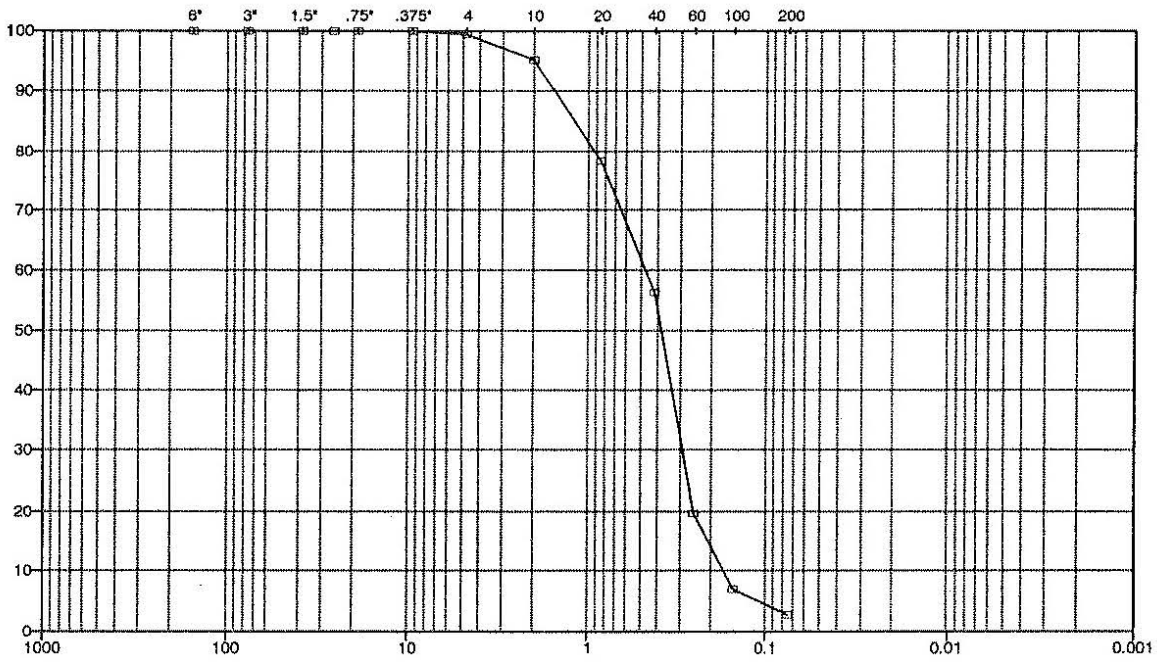
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943-2848.202

FILENAME: 2848113

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS

	Coarse	Fine	C	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt or Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		14.0%	--	--	--	--	Coarse to fine SAND with trace fines,
SAMPLE NO.	PZ-112AS						trace fine gravel
DEPTH (FT.)	34.0-36.0						
Sample Type:		Date Tested: 4/28/95					USCS: SP

TECH: KRF
DATE: 07/11/95
CHECKED: ASF
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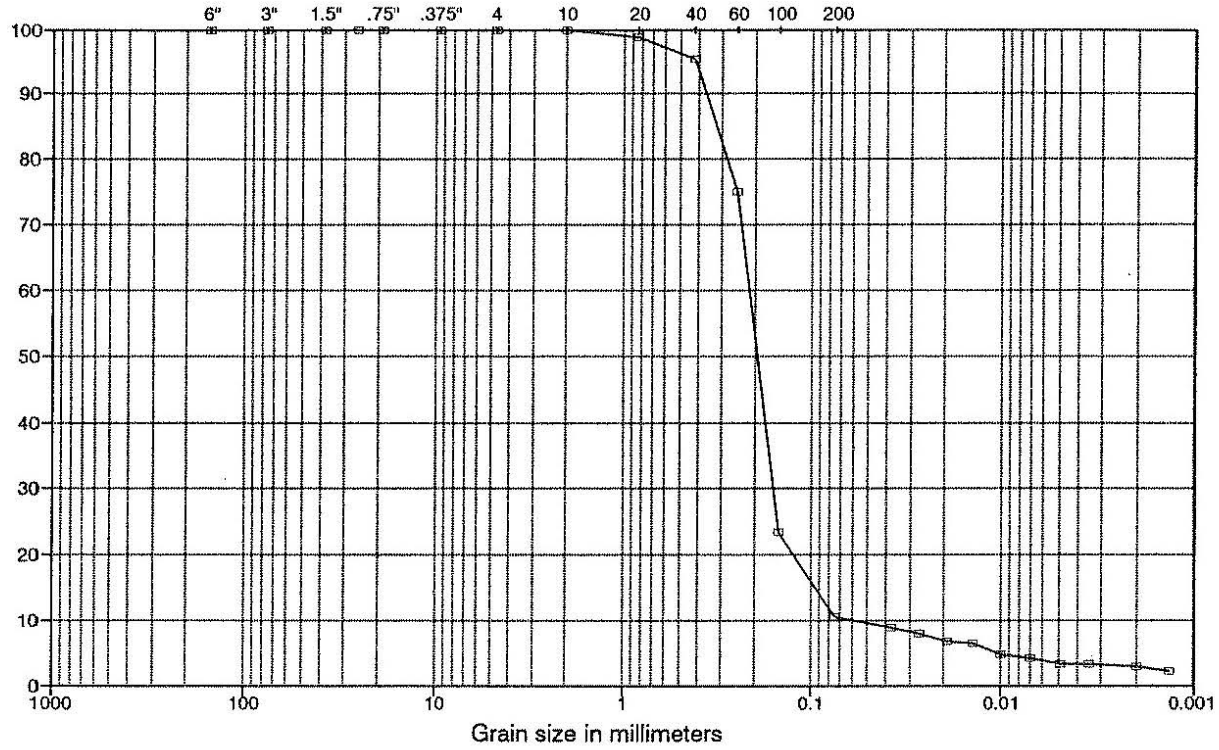
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FILENAME: 2848112

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	Coarse	Fine	Cor	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt and Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE			--	--	--	2.67	Medium to fine SAND with little fines
SAMPLE NO.	PZ-110-SS						
DEPTH	52-54						

Sample Type: Date Tested: 4/6/95 USCS: --

TECH: GI
DATE: 07/11/95
CHECKED: ASF
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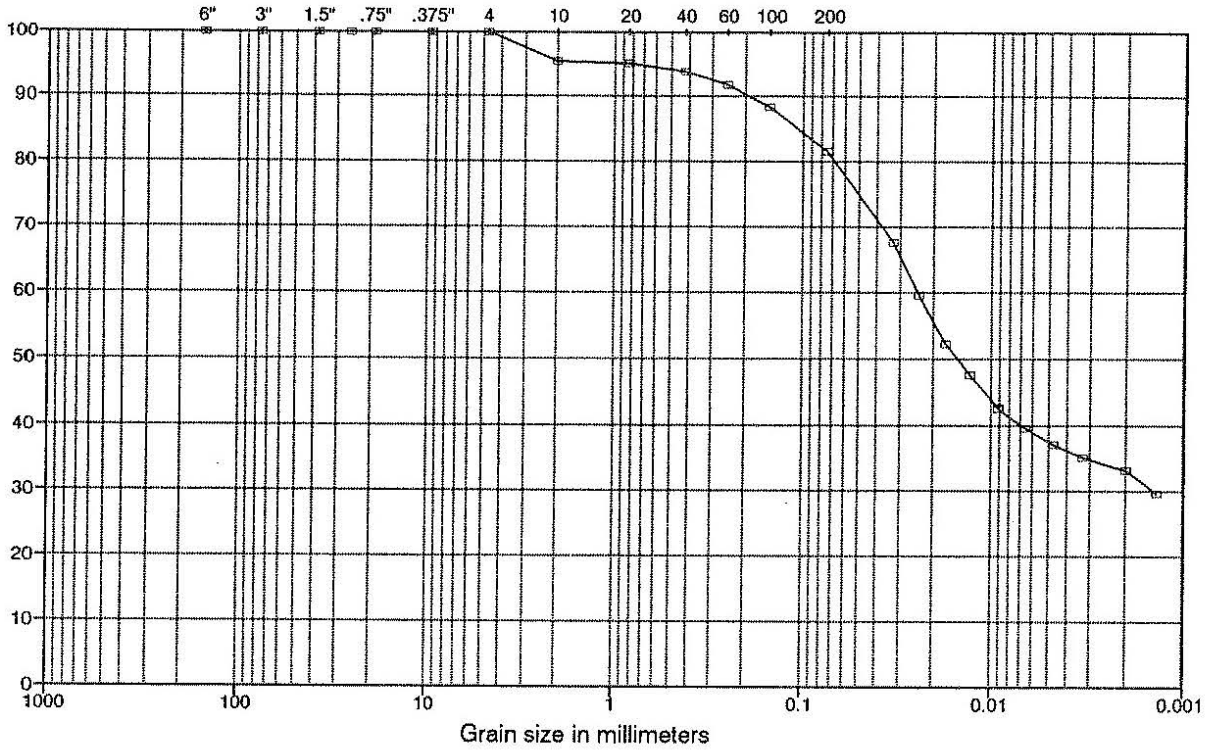
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FILENAME: 2846110

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	COBBLES	GRAVEL		SAND			FINES (Silt and Clay)
		Coarse	Fine	Cor	Med	Fine	

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		28.1	44	19	25	2.61	Silty CLAY with some coarse to fine sand
SAMPLE NO.	PZ-109-SS						
DEPTH	10.0-12.0						

Sample Type: Date Tested: 4/29/95 USCS: CL

TECH: GI
DATE: 07/11/95
CHECKED: ASF
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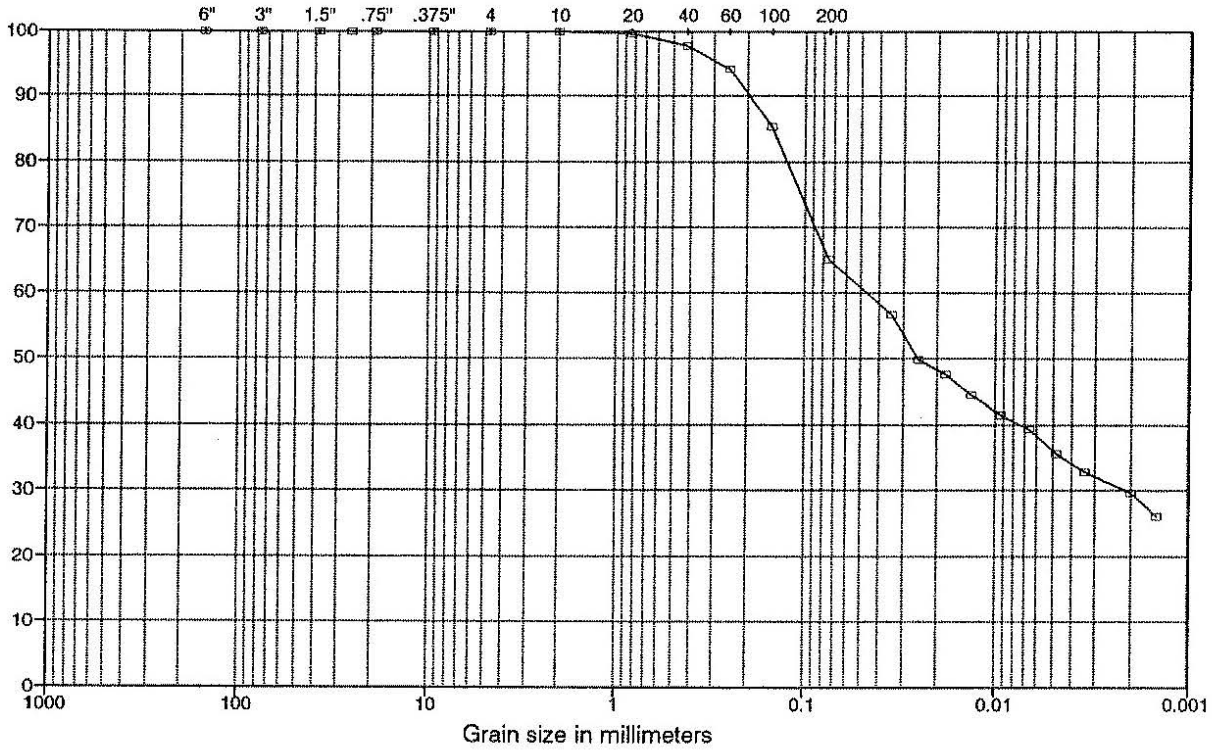
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943-2848.202

FILENAME: 2848109

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	COBBLES	GRAVEL		SAND			FINES (Silt and Clay)
		Coarse	Fine	Cor	Med	Fine	

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE			--	--	--	2.56	FINES and medium to fine SAND
SAMPLE NO.	PZ-108-SS						
DEPTH	16-18						

Sample Type: Date Tested: 4/9/95 USCS: --

TECH: GI
DATE: 07/11/95
CHECKED: ASF
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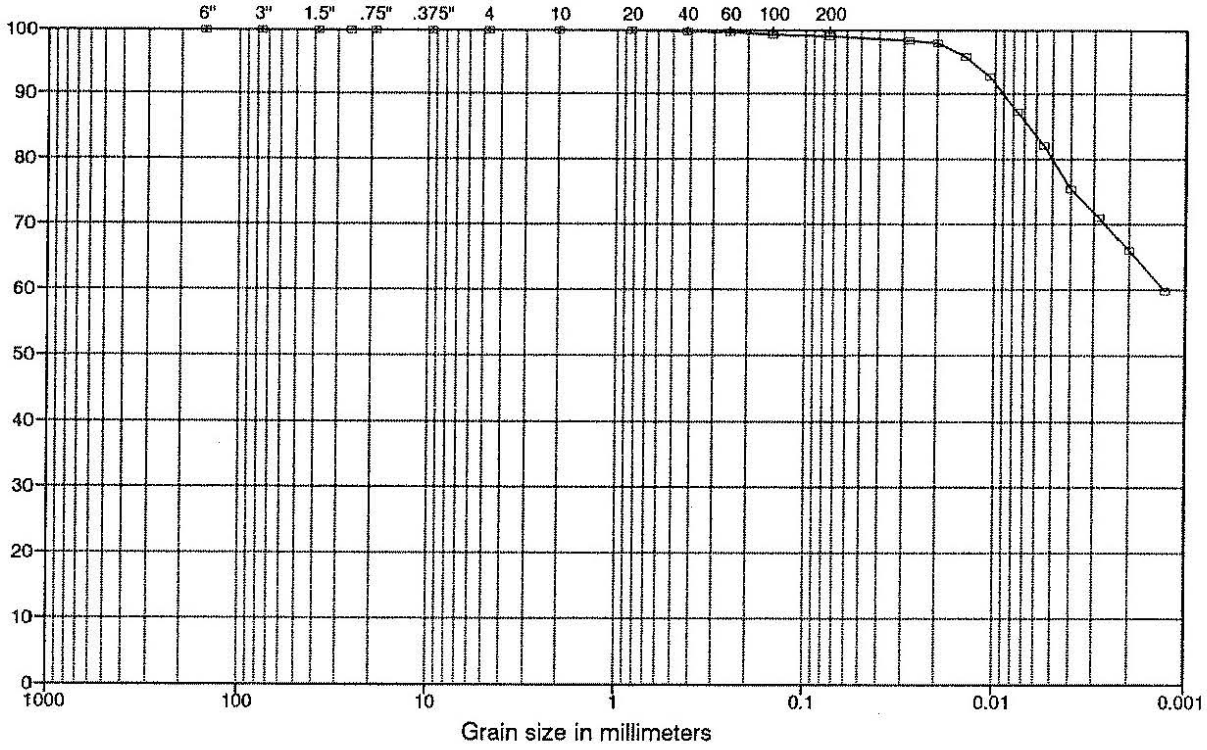
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943-2848.202

FILENAME: 2848108

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	Coarse	Fine	Cor	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt and Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE			--	--	--	2.69	FINES with trace fine sand
SAMPLE NO.	PZ-107-SS						
DEPTH	22-24						

Sample Type: Date Tested: 4/9/95 USCS: --

TECH: GI
DATE: 07/11/95
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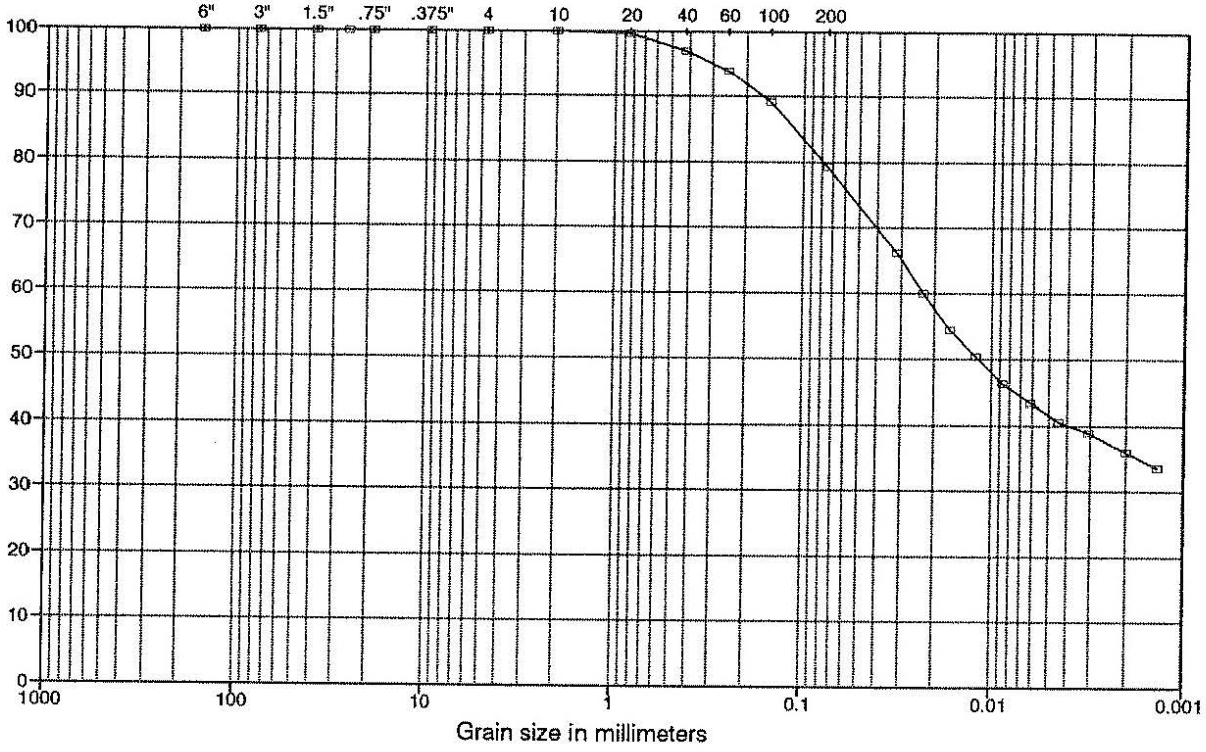
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FILENAME: 2848107

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	COBBLES	Coarse	Fine	Cor	Med	Fine	FINES (Silt and Clay)
		GRAVEL		SAND			

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		22.2	47	20	27	2.77	Silty CLAY with some medium to fine sand
SAMPLE NO.	PZ-106-KS						
DEPTH	6-8,8-10						

Sample Type: Date Tested: 4/9/95 USCS: CL

TECH: GI
DATE: 07/11/95
CHECKED: ASF
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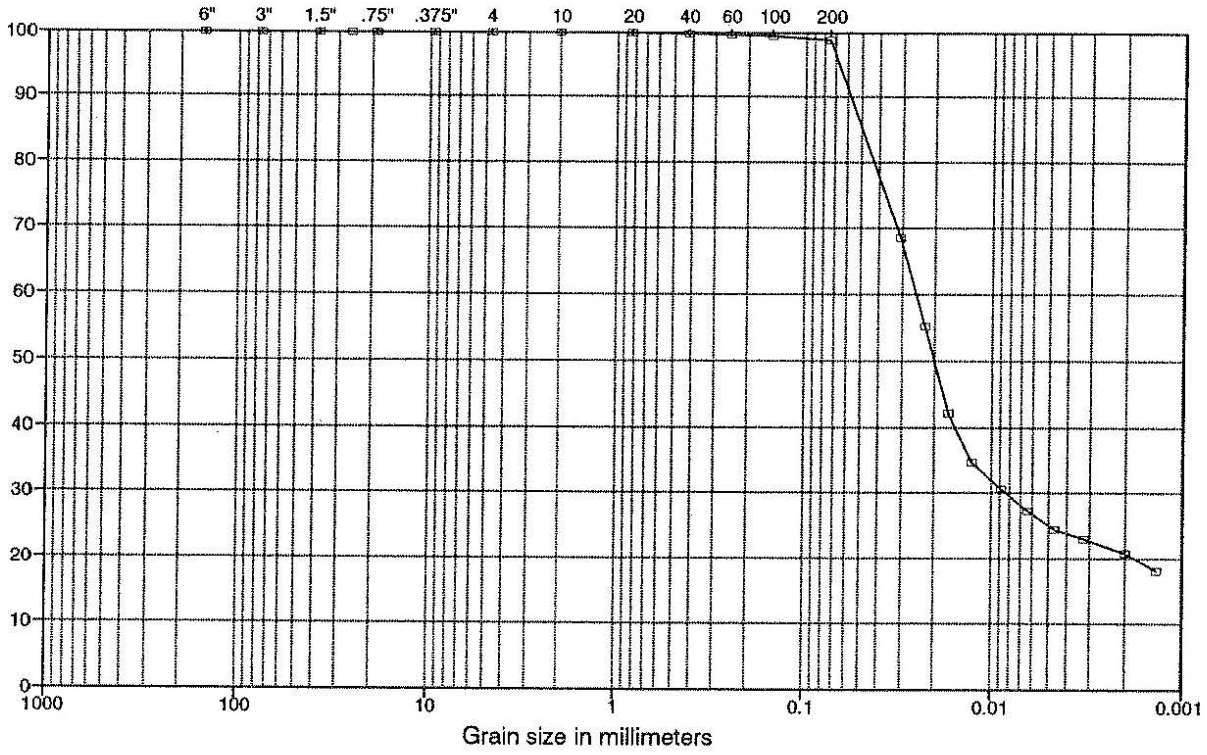
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943-2848.202

FILENAME: 2848106

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	COBBLES	Coarse	Fine	Cor	Med	Fine	FINES (Silt and Clay)
		GRAVEL		SAND			

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE	PZ-105-SS	--	--	--	--	2.71	FINES with trace fine sand
SAMPLE NO.							
DEPTH	10-12'						

Sample Type: Date Tested: 6/27/95 USCS: --

TECH: GI
DATE: 07/11/95
CHECKED: ASF
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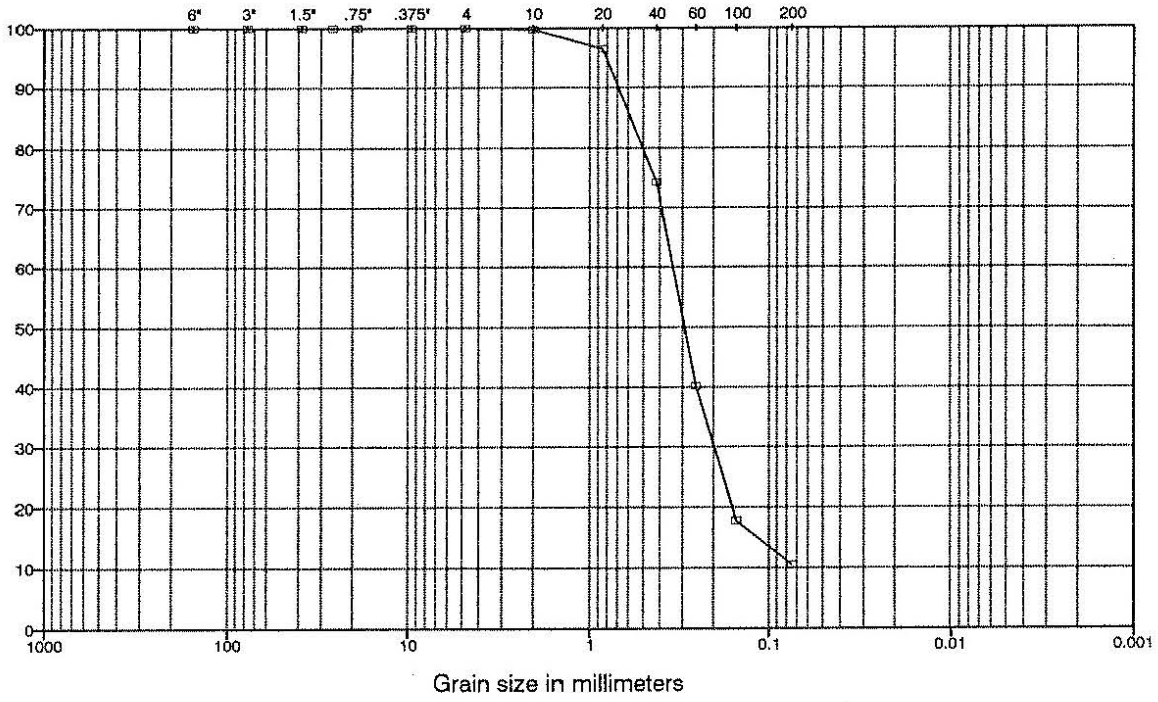
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FILENAME: 2848105A

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS

COBBLES	Coarse	Fine	C	Med	Fine	FINES (Silt or Clay)
	GRAVEL		SAND			

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE	PZ-105-SS	--	--	--	--	--	Medium to fine SAND with little fines
SAMPLE NO.							
DEPTH (FT.)	30-32'						

Sample Type: Date Tested: 6/26/95 USCS: --

TECH: HM
DATE: 07/11/95
CHECKED: ASF
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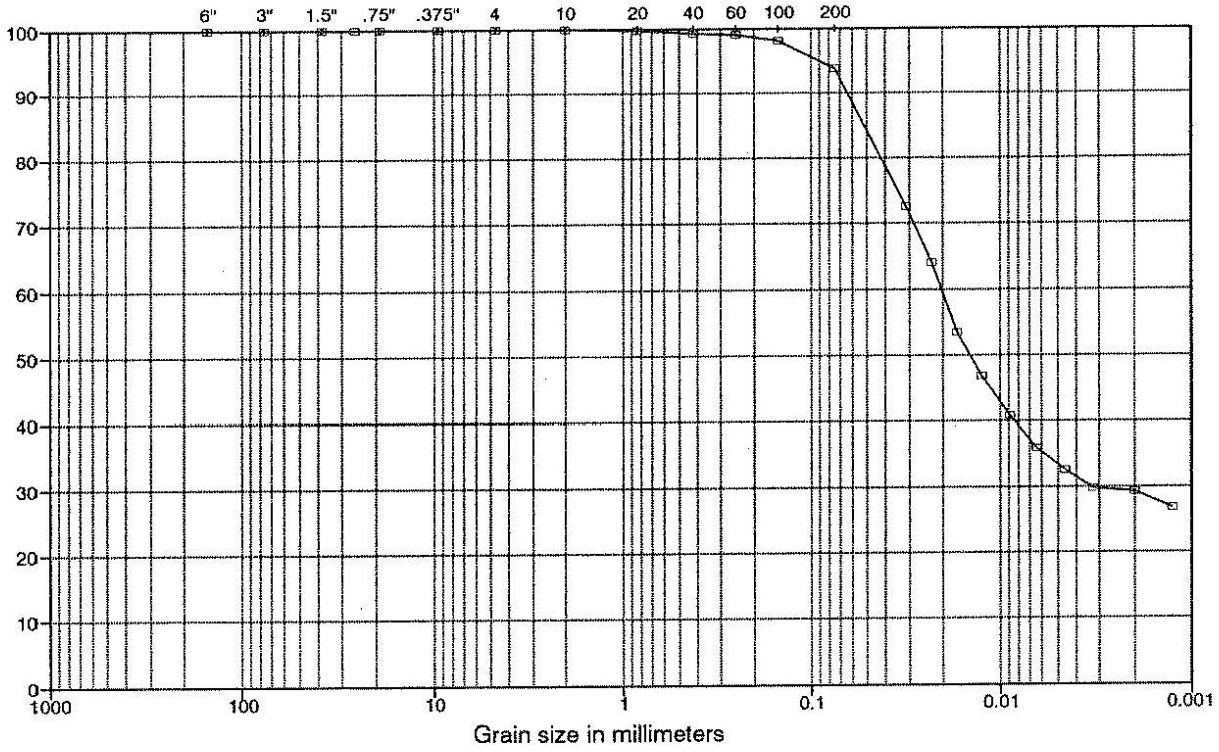
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943-2848.202

FILENAME: 2848105

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	Coarse	Fine	Cor	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt and Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		23.6	46	25	21	2.66	Silty CLAY with little medium to fine sand
SAMPLE NO.	PZ-104-KS						
DEPTH	4-6,6-8						

Sample Type: Date Tested: 4/6/95 USCS: CL

TECH: GI
DATE: 07/11/95
CHECKED: ASF
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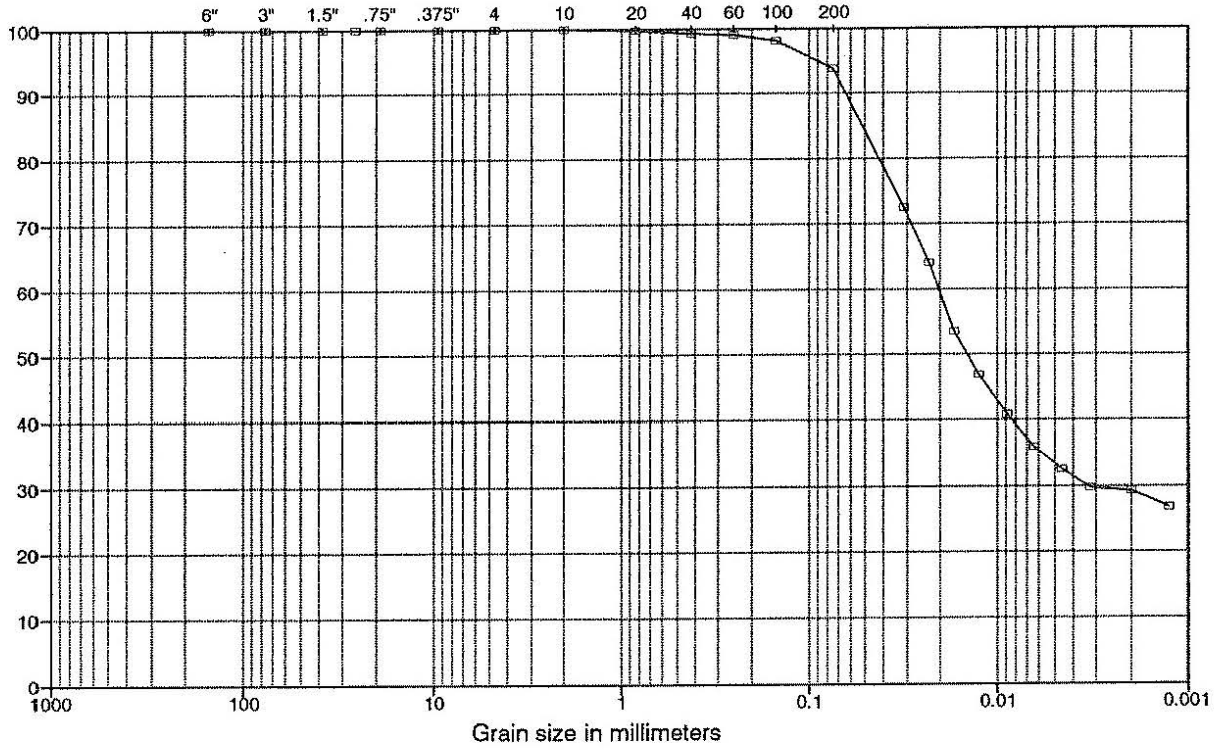
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943-2848.202

FILENAME: 2848104

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	COBBLES	GRAVEL		SAND			FINES (Silt and Clay)
		Coarse	Fine	Cor	Med	Fine	

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		23.6	46	25	21	2.66	Silty CLAY with little medium to fine sand
SAMPLE NO.	PZ-104-KS						
DEPTH	4-6,6-8						

Sample Type: Date Tested: 4/6/95 USCS: CL

TECH: GI
DATE: 07/11/95
CHECKED: ASF
REVIEWED:

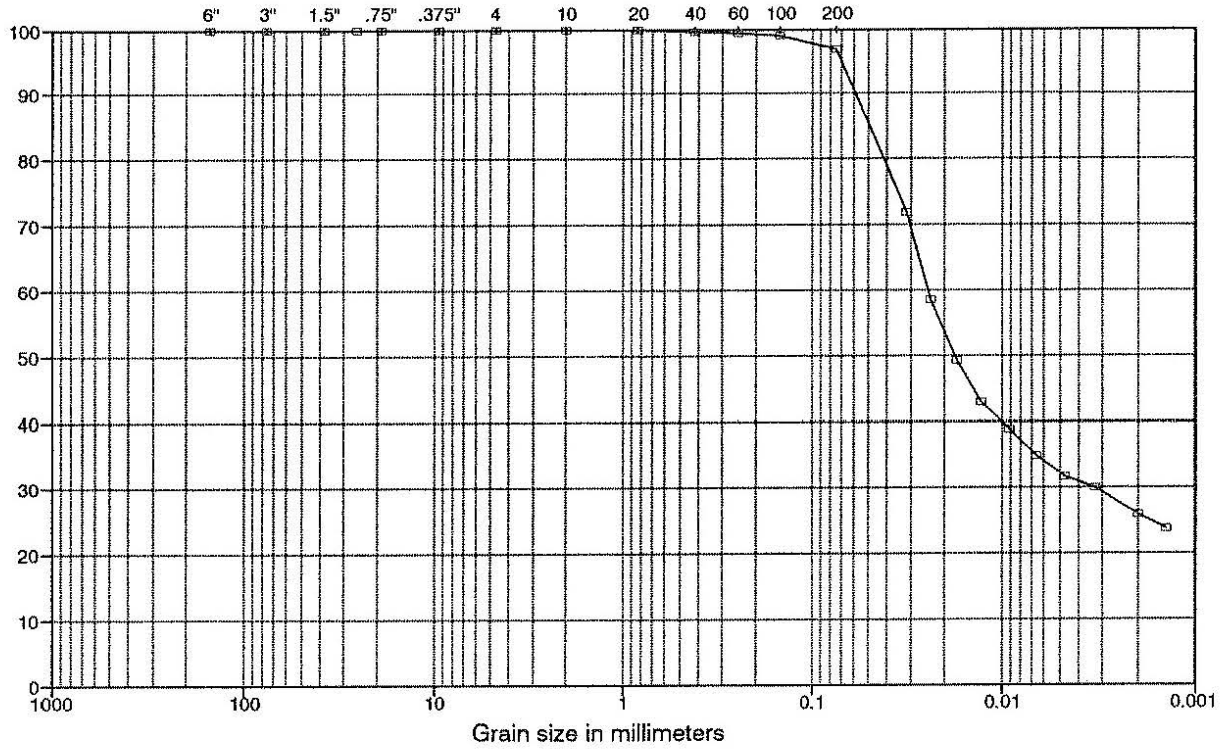
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943-2848.202

FILENAME: Z848104

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



% PASSING

USCS

COBBLES	GRAVEL		SAND			FINES (Silt and Clay)
	Coarse	Fine	Cor	Med	Fine	

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		28.3	--	NP	NP	2.67	SILT with trace medium to fine sand
SAMPLE NO.	PZ-103-SS						
DEPTH	12-14,14-16						

Sample Type: Date Tested: 4/9/95 USCS: ML

TECH: GI
DATE: 07/11/95
CHECKED: ASF
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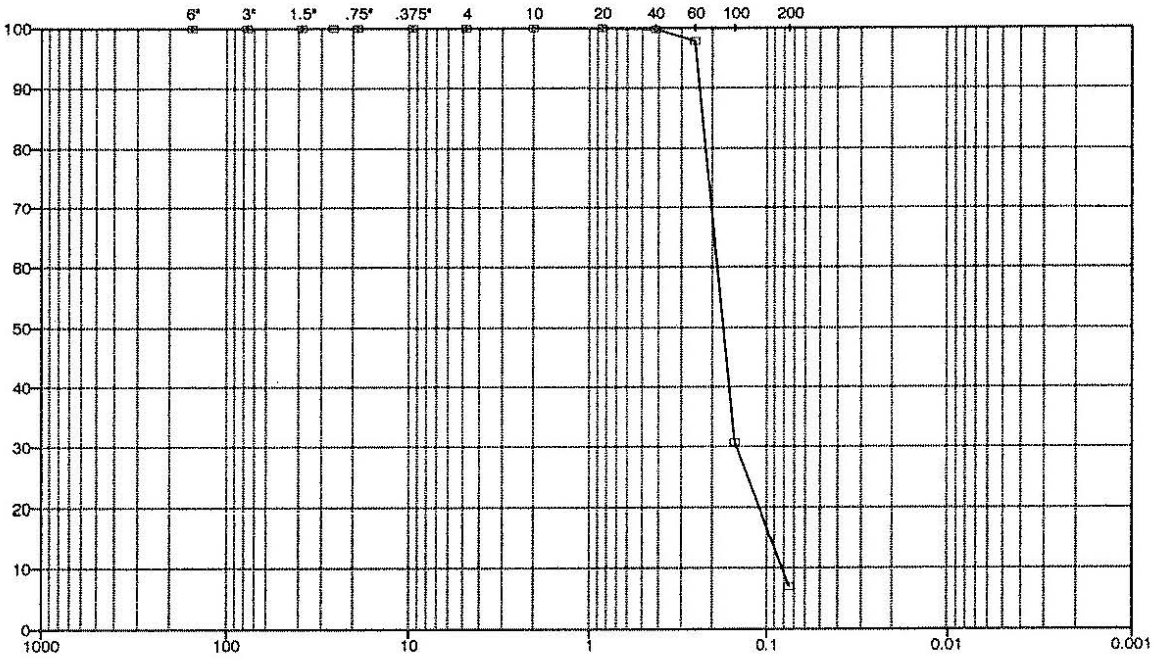
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943-2848.202

FILENAME: 2848103

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS

COBBLES	GRAVEL		SAND			FINES (Silt or Clay)
	Coarse	Fine	C	Med	Fine	

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		17.0%				--	
SAMPLE NO.	PZ-102R-SS						
DEPTH (FT.)	18-20'						

Sample Type: Date Tested: 6/26/95 USCS:

TECH: HM
DATE: 07/11/95
CHECKED: ASF
REVIEWED:

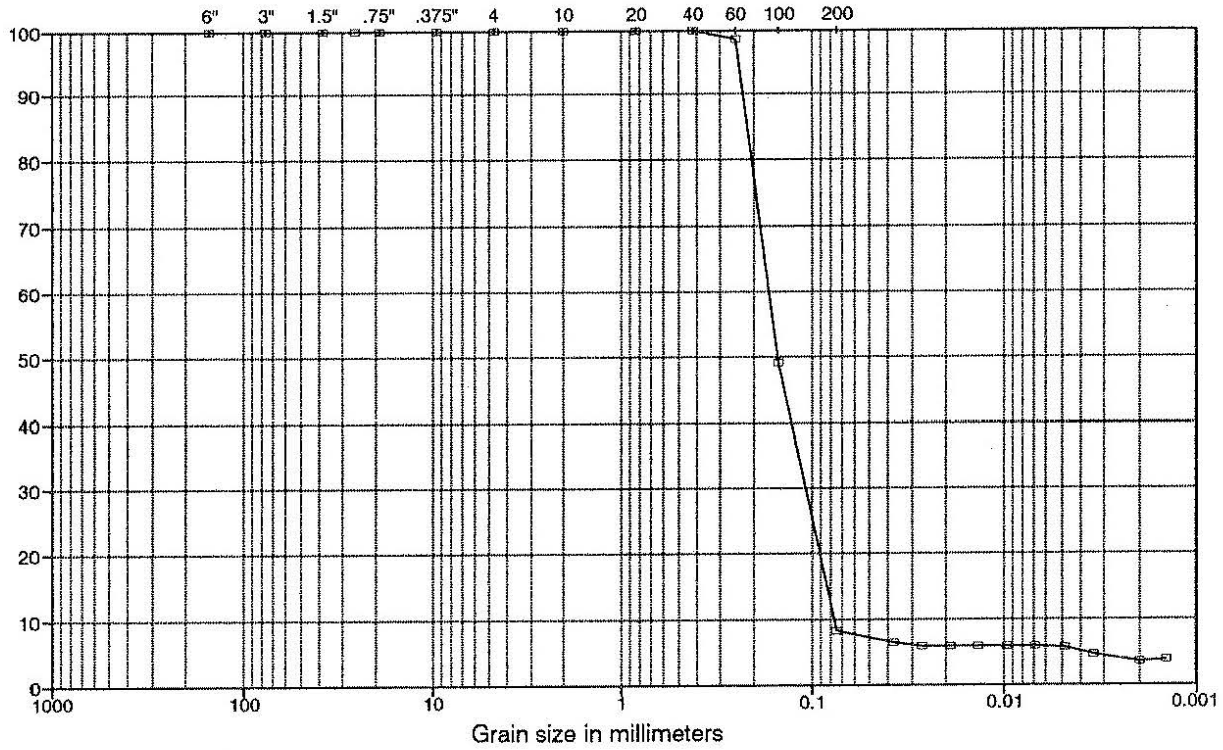
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943-2848.202

FILENAME: 2848102R

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	COBBLES	Coarse	Fine	Cor	Med	Fine	FINES (Silt and Clay)
		GRAVEL		SAND			

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE	PZ-102R-SS	--	--	--	--	2.69	Fine SAND with little fines
SAMPLE NO.							
DEPTH	18-20'						

Sample Type: Date Tested: 6/27/95 USCS: --

TECH: GI
DATE: 07/11/95
CHECKED: ASF
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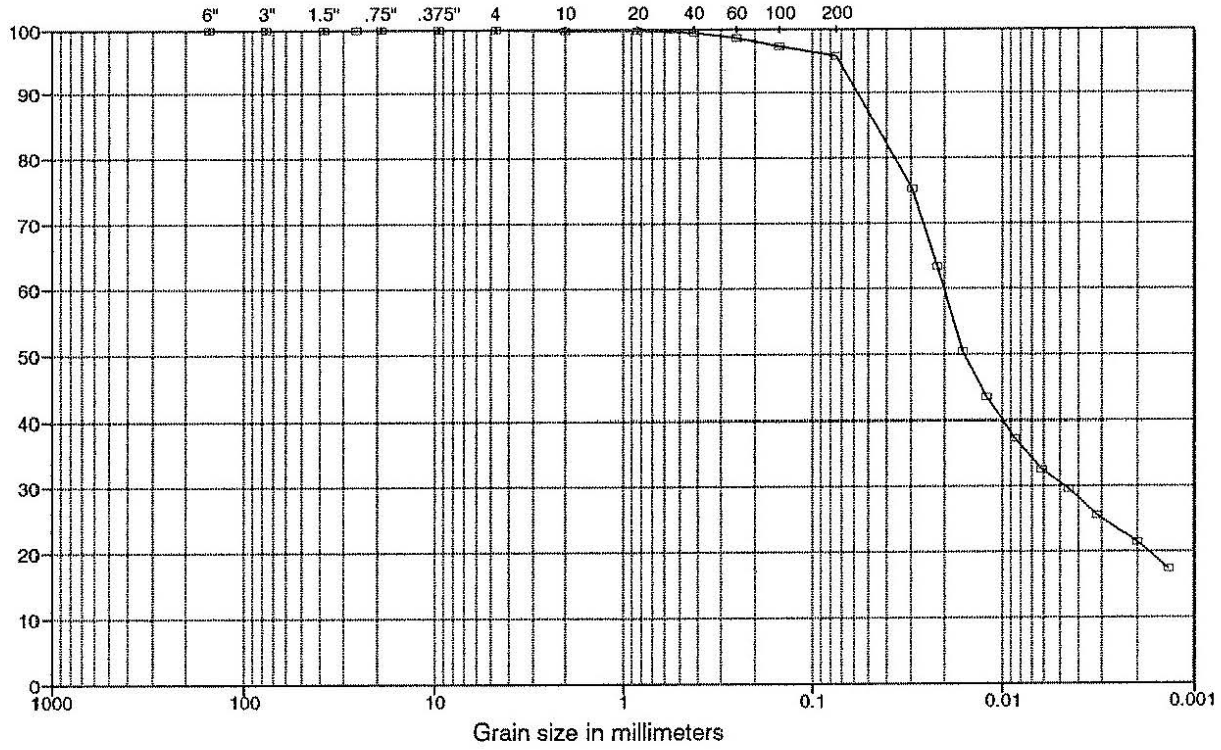
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FILENAME: 2848102B

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	Coarse	Fine	Cor	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt and Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE	PZ-102R-SS	--	--	--	--	2.76	FINES with trace fine sand
SAMPLE NO.							
DEPTH	12-14'						

Sample Type: Date Tested: 6/27/95 USCS: --

TECH: GI
DATE: 07/11/95
CHECKED: ASF
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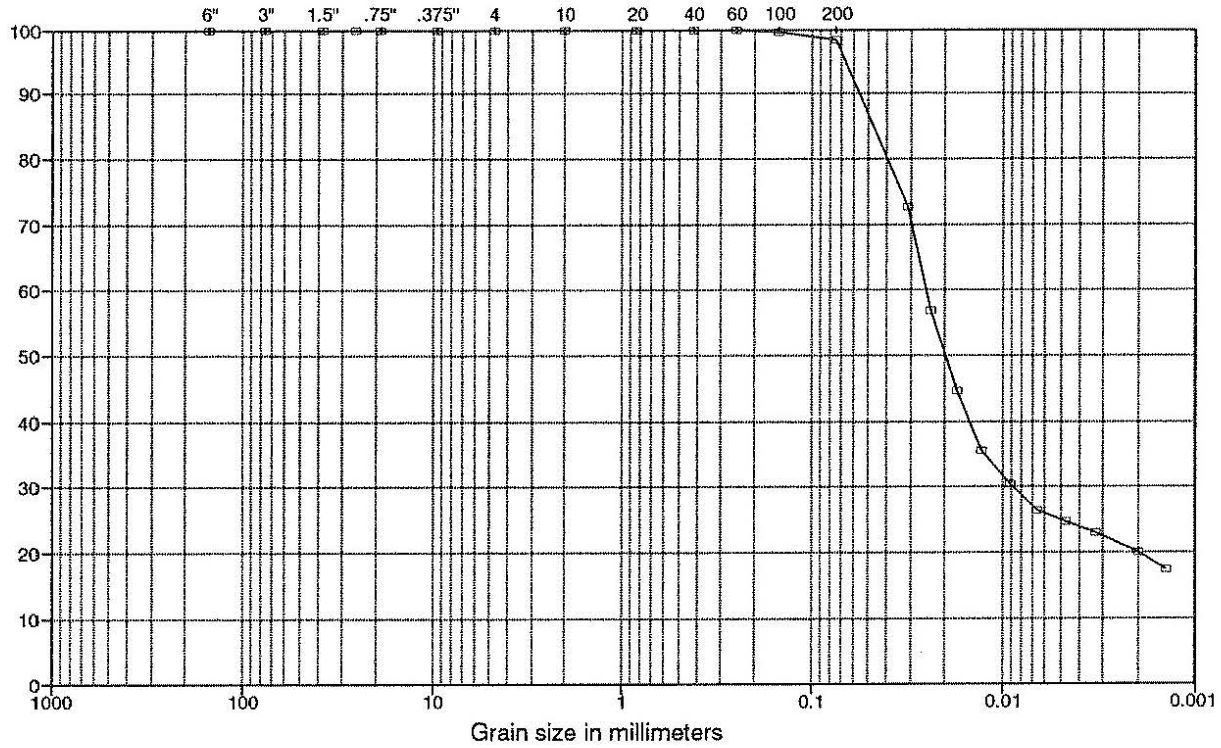
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FILENAME: 2848102A

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	Coarse	Fine	Cor	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt and Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		28.2	39	25	14	2.69	Clayey SILT with trace fine sand
SAMPLE NO.	PZ-102-SS						
DEPTH	4-6,8-10						

Sample Type: Date Tested: 4/9/95 USCS: CL-ML

TECH: GI
DATE: 07/11/95
CHECKED: ASF
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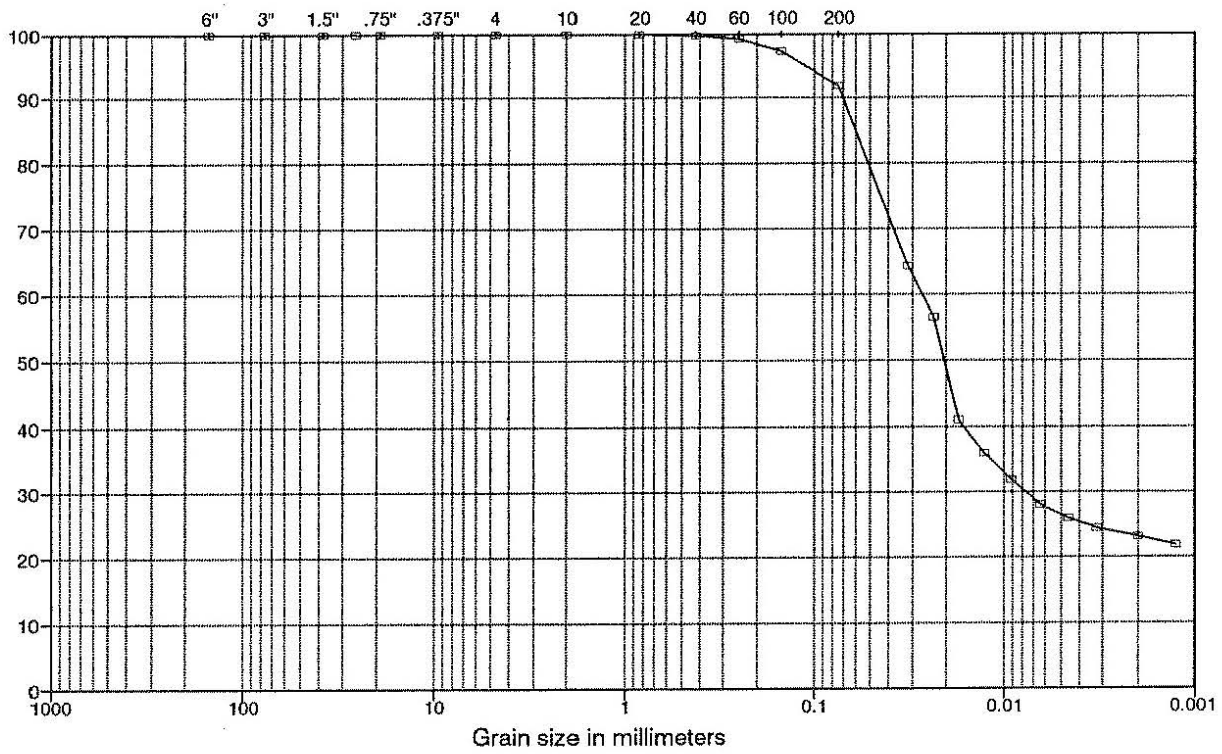
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943-2848.202

FILENAME: 2848102

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	COBBLES	GRAVEL		SAND			FINES (Silt and Clay)
		Coarse	Fine	Cor	Med	Fine	

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE		24.4	38	22	16	2.68	Silty CLAY with little fine sand
SAMPLE NO.	PZ-101-SS						
DEPTH	4-6,6-8						

Sample Type: Date Tested: 4/6/95 USCS: CL

TECH: GI
DATE: 07/11/95
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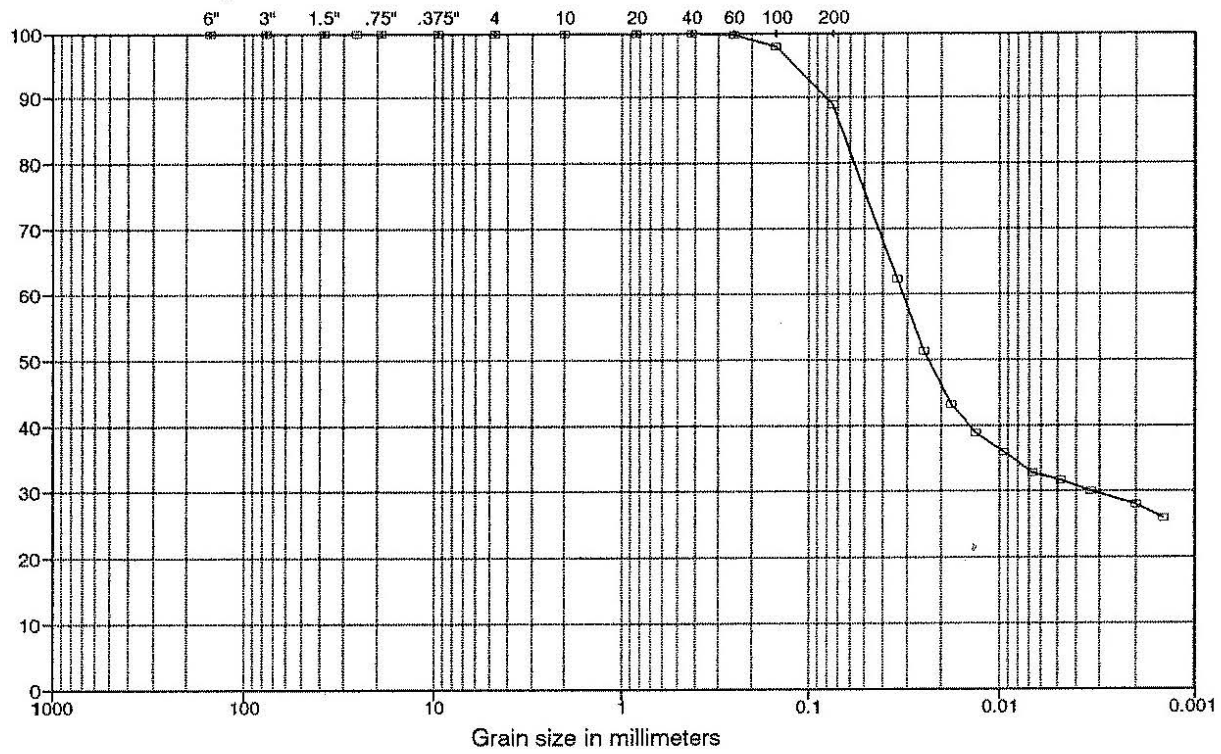
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FILENAME: 2648101

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

PARTICLE SIZE DISTRIBUTION ASTM D421 AND D422

US STANDARD SIEVE OPENING SIZES



USCS	Coarse	Fine	Cor	Med	Fine	
COBBLES	GRAVEL		SAND			FINES (Silt and Clay)

SAMPLE ID		W%	LL	PL	PI	Gs	DESCRIPTION
BOREHOLE			40	24	16	2.62	Silty CLAY with little fine sand
SAMPLE NO.	PZ-100-KS						
DEPTH	4-6,6-8						

Sample Type: Date Tested: 4/9/95 USCS: CL

TECH: GI
DATE: 07/11/95
CHECKED: ASF
REVIEWED:

LAIDLAW/OU2 RIFS/MO
943-2848.202

FILENAME: 2848100

GOLDER ASSOCIATES INC.
LAKEWOOD, COLORADO

APPENDIX L-2

PACKER TESTING SUMMARY

DRAFT

APPENDIX C-1

PACKER TEST DATA

TABLE C-1.1
SUMMARY OF CONSTANT HEAD TEST ANALYSES

COREHOLE NO.	PZ-100-KS	PZ-100-KS	PZ-100-KS	PZ-100-KS	PZ-100-KS	PZ-100-KS	PZ-100-KS	PZ-100-KS	PZ-100-KS
TEST #	1	2	3	4	5	6	7	8	9
TYPE OF PACKER	Single	Single	Single	Double	Double	Double	Double	Double	Double
BOREHOLE DIA. (in)	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0
PRE-TEST W.L. * (feet BGS)	53.5	58.4	81.3	39.8	52.5	82.3	120.7	122.5	99.4
TOP OF TESTED INTERVAL (feet BGS)	377.0	366.0	265.0	37.3	50.0	110.0	195.0	220.0	290.0
BOT OF TESTED INTERVAL (feet BGS)	391.0	391.0	391.0	42.3	55.0	115.0	200.0	225.0	295.0
VERTICAL GAUGE HEIGHT (feet AGS)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0
H(gravity) -feet	57.5	62.4	85.3	43.8	56.5	86.3	124.7	126.5	103.4
H(pressure) -psi	172	143	146	12	20	100.0	12.0	35.0	120.0
Q (gpm)	0.2000	0.1500	3.2000	8.3000	0.0530	0.0180	0.0920	0.0660	3.3000
K (ft/min)	2.7E-06	1.5E-06	8.0E-06	1.5E-03	6.6E-06	7.2E-07	7.7E-06	4.1E-06	1.1E-04
K (cm/sec)	1.4E-06	7.6E-07	4.0E-06	7.5E-04	3.3E-06	3.7E-07	3.9E-06	2.1E-06	5.6E-05

NOTES:

1. The formu $K = [Q/(2\pi LH)]*\ln(L/r)$

Where

K= Hydraulic Conductivity
Q= constant rate of flow into test interval
L= length of the test interval (feet)
H= differential head of water applied in excess of static = H(gravity) + H(pressure)
d= diameter of borehole test interval
*= water levels have been interpolated from measurements taken from completed wells
water levels shown for unsaturated test zones are assumed to be the center of the test interval for calculation purpose

fname: 100KSSUM.XLS

TABLE C-1.2
SUMMARY OF CONSTANT HEAD TEST ANALYSES

COREHOLE NO.	PZ-104-SD	PZ-104-SD	PZ-104-SD	PZ-104-SD	PZ-104-SD	PZ-104-SD
TEST #	1	2	3	4	5	6
TYPE OF PACKER	Single	Single	Double	Double	Double	Double
BOREHOLE DIA. (in)	6.0	6.0	6.0	6.0	6.0	6.0
PRE-TEST W.L. * (feet BGS)	129.6	124.6	129.3	132.9	115.5	52.5
TOP OF TESTED INTERVAL (feet BGS)	162.0	235.0	208.0	188.0	113.0	50.0
BOT OF TESTED INTERVAL (feet BGS)	252.5	252.5	213.0	193.0	118.0	55.0
VERTICAL GAUGE HEIGHT (feet AGS)	4.0	4.0	4.0	4.0	4.0	4.0
H(gravity) -feet	133.6	128.6	133.3	136.9	119.5	56.5
H(pressure) -psi	35	60	100	-	75	40.0
Q (gpm)	1.5000	0.0330	0.4800	-	0.0066	0.0670
K (ft/min)	9.7E-06	6.4E-07	1.7E-05	NA	2.9E-07	5.7E-06
K (cm/sec)	4.9E-06	3.2E-07	8.5E-06	NA	1.5E-07	2.9E-06

NOTES:

1. The formula used for the packer test analysis is:

$$K = [Q/(2PILH)]*\ln(L/r)$$

Where

K = Hydraulic Conductivity
Q = constant rate of flow into test interval
L = length of the test interval (feet)
H = differential head of water applied in excess of static = H(gravity) + H(pressure)
d = diameter of borehole test interval
* = water levels have been interpolated from measurements taken from completed wells
water levels shown for unsaturated test zones are assumed to be the center
of the test interval for calculation purpose
NA = leakage during test

fname: 104SDSUM.XLS

TABLE C-1.3
SUMMARY OF CONSTANT HEAD TEST ANALYSES

COREHOLE NO.	PZ-104-KS	PZ-104-KS	PZ-104-KS	PZ-104-KS	PZ-104-KS	PZ-104-KS	PZ-104-KS	PZ-104-KS
TEST #	1	2	3	4	5	6	7	8
TYPE OF PACKER	Single	Single	Single	Single	Single	Double	Double	Double
BOREHOLE DIA. (in)	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0
PRE-TEST W.L. * (feet BGS)	40.4	48.3	58.9	66.8	72.1	56.5	68.7	98.4
TOP OF TESTED INTERVAL (feet BGS)	390.0	360.0	320.0	290.0	270.0	366.0	343.0	287.0
BOT OF TESTED INTERVAL (feet BGS)	408.0	408.0	408.0	408.0	408.0	371.0	348.0	292.0
VERTICAL GAUGE HEIGHT (feet AGS)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0
H(gravity) -feet	44.4	52.3	62.9	70.8	76.1	60.5	72.7	102.4
H(pressure) -psi	75	85	115	132	85	35.0	48.0	60.0
Q (gpm)	1.1000	1.2000	1.5000	1.7500	1.6000	0.0880	0.0528	0.1010
K (ft/min)	2.6E-05	1.1E-05	6.5E-06	5.2E-06	5.7E-06	7.9E-06	3.7E-06	5.3E-06
K (cm/sec)	1.3E-05	5.7E-06	3.3E-06	2.6E-06	2.9E-06	4.0E-06	1.9E-06	2.7E-06

NOTES:

1. The formula used for the packer test analysis is:

$$K = [Q/(2PILH)]*\ln(L/r)$$

Where

K= Hydraulic Conductivity
Q= constant rate of flow into test interval
L= length of the test interval (feet)
H= differential head of water applied in excess of static = H(gravity) + H(pressure)
d= diameter of borehole test interval
*= water levels have been interpolated from measurements taken from completed wells.

fname: 104KSSUM.XLS

TABLE C-1.4
SUMMARY OF CONSTANT HEAD TEST ANALYSES

COREHOLE NO.	PZ-106-SD	PZ-106-SD	PZ-106-SD	PZ-106-SD	PZ-106-SD
TEST #	1	2	3	4	5
TYPE OF PACKER	Single	Single	Double	Double	Double
BOREHOLE DIA. (in)	6.0	6.0	6.0	6.0	6.0
PRE-TEST W.L. * (feet BGS)	104.6	103.5	103.0	63.5	44.5
TOP OF TESTED INTERVAL (feet BGS)	187.0	140.0	148.0	61.0	42.0
BOT OF TESTED INTERVAL (feet BGS)	201.0	201.0	153.0	66.0	47.0
VERTICAL GAUGE HEIGHT (feet AGS)	4.0	4.0	4.0	4.0	4.0
H(gravity) -feet	108.6	107.5	107.0	67.5	48.5
H(pressure) -psi	69	70	90	30	10
Q (gpm)	0.0154	7.0000	0.2500	0.0440	0.0660
K (ft/min)	3.5E-07	5.0E-05	1.0E-05	4.1E-06	1.2E-05
K (cm/sec)	1.8E-07	2.5E-05	5.1E-06	2.1E-06	6.0E-06

NOTES:

1. The formula used for the packer test analysis is:

$$K = [Q/(2\pi LH)]*\ln(L/r)$$

Where

K= Hydraulic Conductivity
Q= constant rate of flow into test interval
L= length of the test interval (feet)
H= differential head of water applied in excess of static = H(gravity) + H(pressure)
d= diameter of borehole test interval
*= water levels have been interpolated from measurements taken from completed wells. water levels shown for unsaturated test zones are assumed to be the center of the test interval for calculation purpose

fname: 106SDSUM.XLS

TABLE C-1.5
SUMMARY OF CONSTANT HEAD TEST ANALYSES

COREHOLE NO. TEST # TYPE OF PACKER	PZ-106-KS 1 Single	PZ-106-KS 2 Single	PZ-106-KS 3 Single	PZ-106-KS 4 Double	PZ-106-KS 5 Double	PZ-106-KS 6 Double
BOREHOLE DIA. (in)	6.0	6.0	6.0	6.0	6.0	6.0
PRE-TEST W.L. * (feet BGS)	21.5	23.6	34.4	91.6	83.4	23.8
TOP OF TESTED INTERVAL (feet BGS)	364.0	346.0	301.0	215.0	237.0	357.0
BOT OF TESTED INTERVAL (feet BGS)	374.0	374.0	374.0	220.0	242.0	362.0
VERTICAL GAUGE HEIGHT (feet AGS)	4.0	4.0	4.0	4.0	4.0	4.0
H(gravity) -feet	25.5	27.6	38.4	95.6	87.4	27.8
H(pressure) -psi	80	125	41	30	38	88.0
Q (gpm)	0.9000	3.8000	4.6000	0.0066	0.0660	1.0000
K (ft/min)	3.4E-05	4.3E-05	5.7E-05	5.1E-07	4.8E-06	5.5E-05
K (cm/sec)	1.7E-05	2.2E-05	2.9E-05	2.6E-07	2.4E-06	2.8E-05

NOTES:

1. The formula used for the packer test analysis is:

$$K = [Q/(2\pi LH)]*\ln(L/r)$$

Where

K= Hydraulic Conductivity
Q= constant rate of flow into test interval
L= length of the test interval (feet)
H= differential head of water applied in excess of static = H(gravity) + H(pressure)
d= diameter of borehole test interval
*= water levels have been interpolated from measurements taken from completed wells.

fname: 100KSSUM.XLS

TABLE C-1.6
SUMMARY OF CONSTANT HEAD TEST ANALYSES

COREHOLE NO. TEST # TYPE OF PACKER	PZ-111-SD 1 Single	PZ-111-SD 2 Single	PZ-111-SD 3 Single	PZ-111-SD 4 Double	PZ-111-SD 5 Double	PZ-111-SD 6 Double
BOREHOLE DIA. (in)	6.0	6.0	6.0	6.0	6.0	6.0
PRE-TEST W.L. * (feet BGS)	87.5	87.5	87.5	87.5	87.5	87.5
TOP OF TESTED INTERVAL (feet BGS)	175.0	140.0	105.0	195.0	125.0	162.0
BOT OF TESTED INTERVAL (feet BGS)	210.0	210.0	210.0	200.0	130.0	167.0
VERTICAL GAUGE HEIGHT (feet AGS)	3.0	3.0	3.0	3.0	3.0	3.0
H(gravity) -feet	90.5	90.5	90.5	90.5	90.5	90.5
H(pressure) -psi	68	65	43	46	46	102.0
Q (gpm)	0.2000	0.9000	0.6000	0.0018	0.0165	0.0396
K (ft/min)	2.4E-06	6.4E-06	3.9E-06	1.1E-07	1.1E-06	1.5E-06
K (cm/sec)	1.2E-06	3.3E-06	2.0E-06	5.8E-08	5.4E-07	7.9E-07

NOTES:

1. The formula used for the packer test analysis is:

$$K = [Q/(2\pi LH)]*\ln(L/r)$$

Where

K= Hydraulic Conductivity
Q= constant rate of flow into test interval
L= length of the test interval (feet)
H= differential head of water applied in excess of static = H(gravity) + H(pressure)
d= diameter of borehole test interval
*= water levels have been interpolated from measurements taken from completed wells.

fname: 111SDSUM.XLS

TABLE C-1.7
SUMMARY OF CONSTANT HEAD TEST ANALYSES

COREHOLE NO.	PZ-111-KS	PZ-111-KS	PZ-111-KS	PZ-111-KS	PZ-111-KS	PZ-111-KS	PZ-111-KS	PZ-111-KS	PZ-111-KS
TEST #	1	2	3	4	5	6	7	8	9
TYPE OF PACKER	Single	Single	Single	Single	Double	Double	Double	Double	Double
BOREHOLE DIA. (in)	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0	6.0
PRE-TEST W.L. * (feet BGS)	22.8	34.2	40.7	49.3	22.0	27.1	62.7	77.3	79.5
TOP OF TESTED INTERVAL (feet BGS)	343.0	290.0	260.0	220.0	355.0	343.0	260.0	226.0	221.0
BOT OF TESTED INTERVAL (feet BGS)	368.0	368.0	368.0	368.0	360.0	348.0	265.0	231.0	226.0
VERTICAL GAUGE HEIGHT (feet AGS)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0
H(gravity) -feet	26.8	38.2	44.7	53.3	26.0	31.1	66.7	81.3	83.5
H(pressure) -psi	42	60	60	80	54	65.0	66.0	94.0	94.0
Q (gpm)	1.3000	1.9000	1.8500	2.3500	1.0000	0.7000	0.0660	0.0771	0.0440
K (ft/min)	4.1E-05	1.7E-05	1.2E-05	9.1E-06	8.5E-05	4.9E-05	3.8E-06	3.3E-06	1.9E-06
K (cm/sec)	2.1E-05	8.6E-06	6.1E-06	4.6E-06	4.3E-05	2.5E-05	2.0E-06	1.7E-06	9.5E-07

NOTES:

1. The formula used for the packer test analysis is:

$$K = [Q/(2\pi ILH)]*\ln(L/r)$$

Where

K = Hydraulic Conductivity
Q = constant rate of flow into test interval
L = length of the test interval (feet)
H = differential head of water applied in excess of static = H(gravity) + H(pressure)
d = diameter of borehole test interval
* = water levels have been interpolated from measurements taken from completed wells.

fname: 111KSSUM.XLS

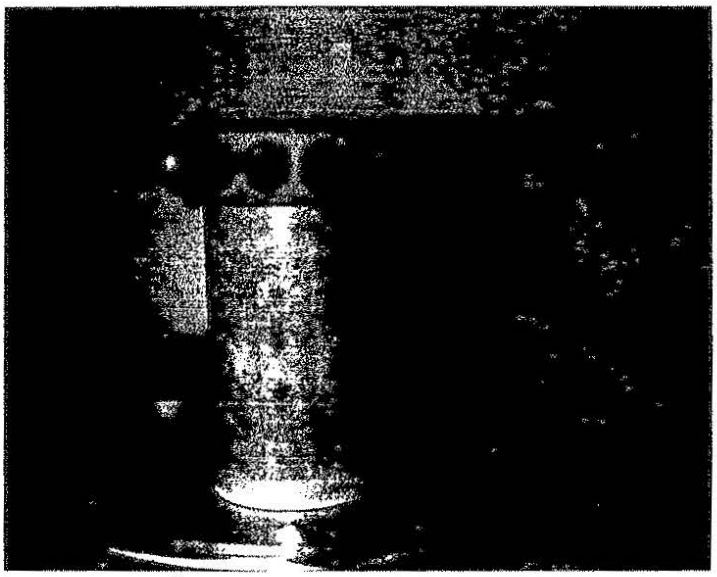
APPENDIX L-3

LABORATORY TESTING SUMMARY

DRAFT

TRIAXIAL, BACK-PRESSURE PERMEABILITY, TX/PBP

ASTM D 5084



Golder Assoc. 3003-31
ST-1 PZ-105-RS Tailings
201.9 - 202.5' 23010 PSF

PERMEABILITY TEST - BACK PRESSURE SATURATED - FLOW PUMP METHOD
ASTM D 5084

CLIENT	Golder Assoc.	JOB NO.	2003-51
BORING NO.	GTS-1	SAMPLED	3-15-95 BT
DEPTH	201.9-202.5'	TEST STARTED	4-22-95 DCW
SAMPLE NO.	PZ-106-KS	TEST FINISHED	5-1-95 CJW/CAL
SOIL DESCR.		CELL NUMBER	1N
TEST TYPE	TX/Pbp	SATURATED TEST	Yes
CONF. PRES. PSF	23040		

MOISTURE/DENSITY DATA		BEFORE TEST	AFTER TEST
Wt. Soil + Moisture	(g)	307.6	311.5
Wt. Wet Soil & Pan	(g)	315.0	319.0
Wt. Dry Soil & Pan	(g)	301.9	301.9
Wt. Lost Moisture	(g)	13.1	17.1
Wt. of Pan Only	(g)	7.4	7.4
Wt. of Dry Soil	(g)	294.5	294.5
Moisture Content %		4.5	5.8
Wet Density PCF		158.6	157.3
Dry Density PCF		151.9	148.6

Init. Diameter	(in)	1.770	(cm)	4.496
Init. Area	(sq in)	2.461	(sq cm)	15.876
Init. Height	(in)	3.002	(cm)	7.625
Vol. Bef. Consol.	(cu ft)	0.00427		
Vol. After Consol.	(cu ft)	0.00437		
Porosity %		13.81		
Constant Head	(PSI)	0.00	(cm)	0.00

FLOW PUMP CALCULATIONS

Pump Setting	1.0
Velocity (cm/s)	7.44E-06
Q (cc/s)	2.38E-07
Height	2.996
Diameter	1.791
Pressure (psi)	13.990
Area after consol. (cm*cm)	16.252
Gradient	129.255
Permeability k (cm/s)	1.1E-10
Back Pressure (psi)	98.0
Cell Pressure (psi)	258.0
Ave. Effective Stress (psi)	153.005

Note: Test Terminated at internal pore pressure development of 13.99 psi (machine capacity). Therefore, actual k value is less than that shown.

Data entry by: NAA Date: 5/2/95
Checked by: MGJ Date: 5-3-95
FileName:B:GOY0GTS1

ADVANCED TERRA TESTING, INC.

TRIAXAL COMPRESSION TEST DATA

CLIENT Golder Assoc. JOB NO. 2003-51

BORING NO.	GTS-1	SAMPLED	3-15-95 BT
DEPTH	201.9-202.5'	TEST STARTED	4-22-95 DCW
SAMPLE NO.	PZ-106-KS	TEST FINISHED	5-1-95 CJW/CAL
SOIL DESCR.		SETUP NO.	1N
TEST TYPE	TX/Pbp	SATURATED TEST	Yes
CONF. PRES. PSF	23040		

SATURATION DATA

Cell Pres. (PSI)	Back Pres. (PSI)	Burette Reading (CC)		Pore Pressure (PSI)		Change	B
		Close	Open	Close	Open		
40.0	38.0	7.2	16.4				
50.0	48.0	17.0	17.7	38.4	45.3	6.9	0.69
60.0	58.0	18.0	18.7	48.4	56.1	7.7	0.77
70.0	68.0	19.0	19.8	59.1	67.2	8.1	0.81
80.0	78.0	19.8	20.4	68.5	76.9	8.4	0.84
90.0	88.0	20.6	21.2	78.2	86.9	8.7	0.87
100.0	98.0	21.1	21.8	88.1	96.8	8.7	0.87
110.0		22.0	22.1	98.3	106.9	8.6	0.86

CONSOLIDATION DATA

Elapsed Time (Min)	SQRT Time (Min)	Burette Reading (CC)	Volume Defl. (cc)
0.00	0.00	23.50	0.00
0.25	0.50	33.40	-9.90
0.5	0.71	33.45	-9.95
1	1.00	33.50	-10.00
2	1.41	33.55	-10.05
4	2.00	33.65	-10.15
9	3.00	33.70	-10.20
16	4.00	33.85	-10.35
30	5.48	34.00	-10.50
60	7.75	34.10	-10.60
120	10.95	34.30	-10.80
240	15.49	34.50	-11.00
360	18.97	34.55	-11.05

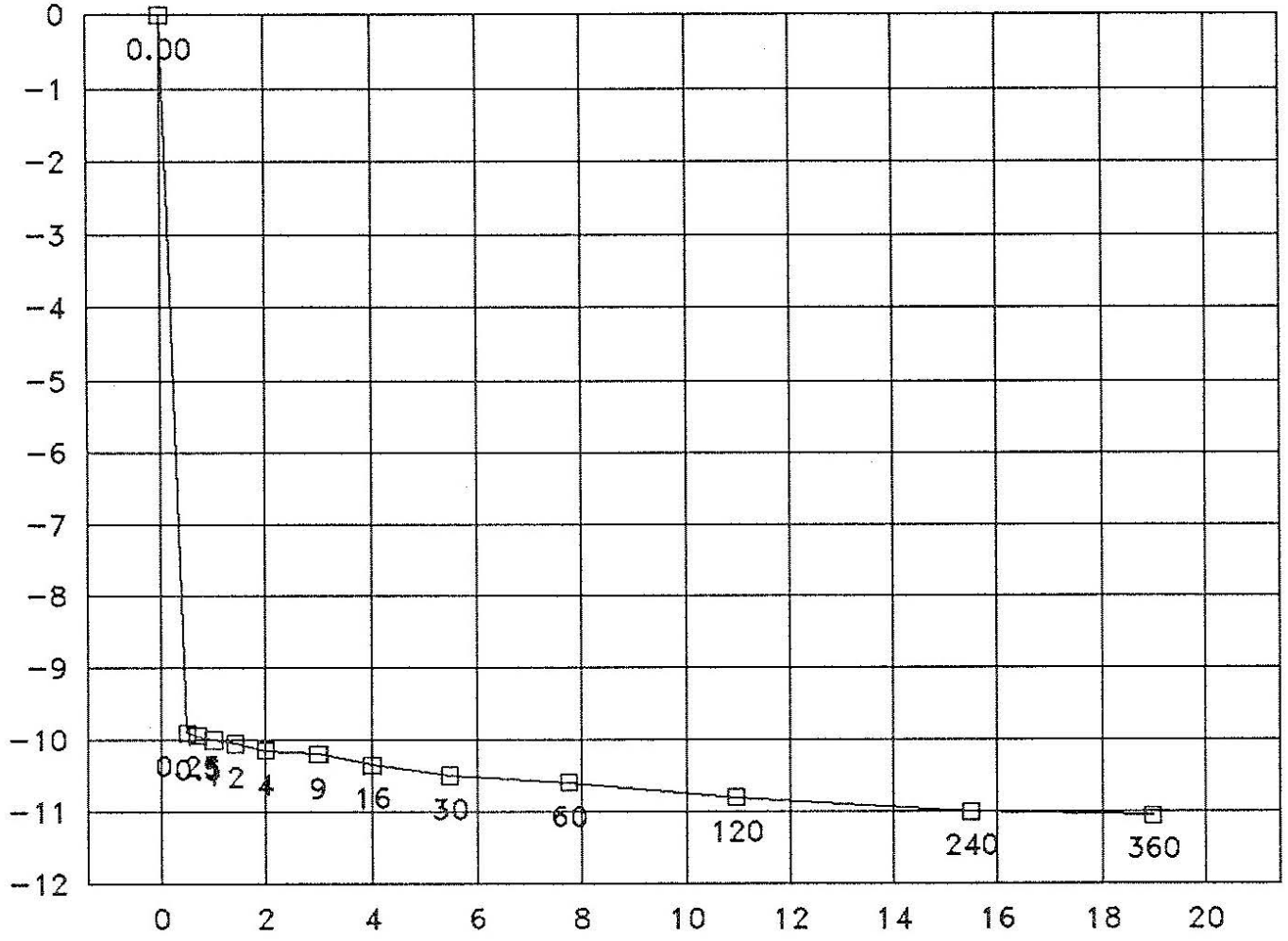
Initial Height	(in)	3.002	Init. Vol.	(CC)	121.07
Height Change	(in)	0.006	Vol. Change	(CC)	27.20
Ht. After Cons.	(in)	2.996	Cell Exp.	(CC)	29.83
Initial Area	(sq in)	2.461	Net Change	(CC)	-2.63
Area After Cons.	(sq in)	2.519	Cons. Vol.	(CC)	123.70

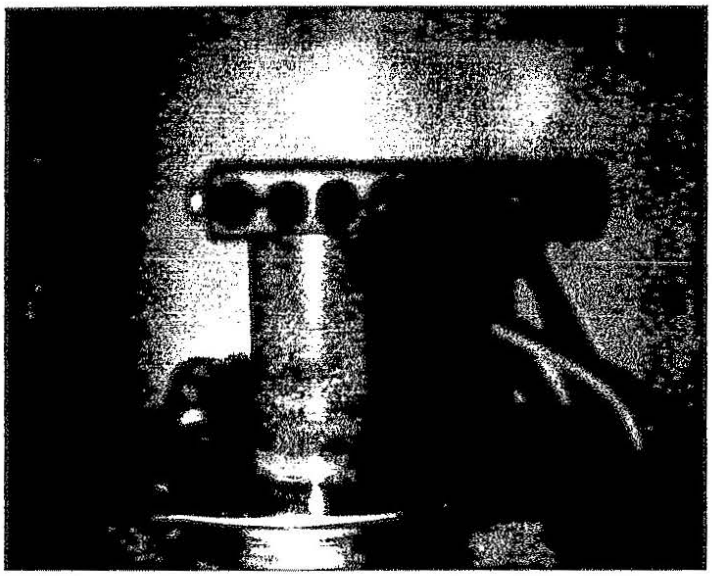
Data entry by: NAA Date: 5/2/95
Checked by: MGS Date: 5-3-95
FileName:B:GOYOGTS1

ADVANCED TERRA TESTING, INC.

CONSOLIDATION DATA

GTS-1, 201.9-202.5', PZ-106-KS





Golder Assoc.
GTS-2 PZ-106-KS
229.5 – 230.1'

2003-51
Tx/Php
25200 PSF

PERMEABILITY TEST - BACK PRESSURE SATURATED - FLOW PUMP METHOD
ASTM D 5084

CLIENT	Golder Assoc.	JOB NO.	2003-51
BORING NO.	GTS-2	SAMPLED	3-15-95 BT
DEPTH	229.6-230.1'	TEST STARTED	4-21-95 DCW
SAMPLE NO.	PZ-106-KS	TEST FINISHED	4-30-95 DCW
SOIL DESCR.		CELL NUMBER	3N
TEST TYPE	TX/Pbp	SATURATED TEST	Yes
CONF. PRES. PSF	25200		

MOISTURE/DENSITY DATA		BEFORE TEST	AFTER TEST
Wt. Soil + Moisture	(g)	297.0	303.9
Wt. Wet Soil & Pan	(g)	300.7	307.6
Wt. Dry Soil & Pan	(g)	288.1	288.1
Wt. Lost Moisture	(g)	12.6	19.5
Wt. of Pan Only	(g)	3.7	3.7
Wt. of Dry Soil	(g)	284.4	284.4
Moisture Content %		4.4	6.9
Wet Density PCF		154.5	143.3
Dry Density PCF		148.0	134.1

Init. Diameter	(in)	1.758	(cm)	4.465
Init. Area	(sq in)	2.427	(sq cm)	15.661
Init. Height	(in)	3.016	(cm)	7.661
Vol. Bef. Consol.	(cu ft)	0.00424		
Vol. After Consol.	(cu ft)	0.00468		
Porosity %		14.73		
Constant Head	(PSI)	0.00	(cm)	0.00

FLOW PUMP CALCULATIONS

Pump Setting	1.0
Velocity (cm/s)	7.44E-06
Q (cc/s)	2.38E-07
Height	3.005
Diameter	1.850
Pressure (psi)	10.210
Area after consol. (cm*cm)	17.346
Gradient	94.049
Permeability k (cm/s)	1.5E-10
Back Pressure (psi)	88.0
Cell Pressure (psi)	263.0
Ave. Effective Stress (psi)	169.895

Data entry by: NAA Date: 5/2/95
Checked by: MGT Date: 5-3-95
FileName:B:GOYOGTS2

ADVANCED TERRA TESTING, INC.

TRIAXAL COMPRESSION TEST DATA

CLIENT Golder Assoc. JOB NO. 2003-51

BORING NO.	GTS-2	SAMPLED	3-15-95 BT
DEPTH	229.6-230.1'	TEST STARTED	4-21-95 DCW
SAMPLE NO.	PZ-106-KS	TEST FINISHED	4-30-95 DCW
SOIL DESCR.		SETUP NO.	3N
TEST TYPE	TX/Pbp	SATURATED TEST	Yes
CONF. PRES. PSF	25200		

SATURATION DATA

Cell Pres. (PSI)	Back Pres. (PSI)	Burette Reading (CC)		Pore Pressure (PSI)		Change	B
		Close	Open	Close	Open		
40.0	38.0	6.7	13.0				
50.0	48.0	12.1	12.8	38.3	46.2	7.9	0.79
60.0	58.0	12.7	13.3	48.7	56.8	8.1	0.81
70.0	68.0	13.4	14.0	58.9	67.1	8.2	0.82
80.0	78.0	14.3	14.9	68.9	78.1	9.2	0.92
90.0	88.0	14.8	15.3	78.5	87.9	9.4	0.94
100.0		15.6	15.7	88.1	97.6	9.5	0.95

CONSOLIDATION DATA

Elapsed Time (Min)	SQRT Time (Min)	Burette Reading (CC)	Volume Defl. (cc)
0.00	0.00	0.80	0.00
0.25	0.50	10.90	-10.10
0.5	0.71	11.30	-10.50
1	1.00	11.83	-11.02
2	1.41	11.95	-11.15
4	2.00	12.05	-11.25
9	3.00	12.10	-11.30
16	4.00	12.33	-11.52
30	5.48	12.53	-11.73
60	7.75	12.70	-11.90
120	10.95	13.03	-12.23
240	15.49	13.03	-12.23
360	18.97	13.10	-12.30

Initial Height	(in)	3.016	Init. Vol.	(CC)	119.99
Height Change	(in)	0.011	Vol. Change	(CC)	21.30
Ht. After Cons.	(in)	3.005	Cell Exp.	(CC)	33.73
Initial Area	(sq in)	2.427	Net Change	(CC)	-12.43
Area After Cons.	(sq in)	2.689	Cons. Vol.	(CC)	132.42

Data entry by: NAA Date: 5/2/95
Checked by: MGJ Date: 5-3-95 ADVANCED TERRA TESTING, INC.
FileName:B:GOYOGTS2

CONSOLIDATION DATA

GTS-2, 229.6-230.1', PZ-106-KS

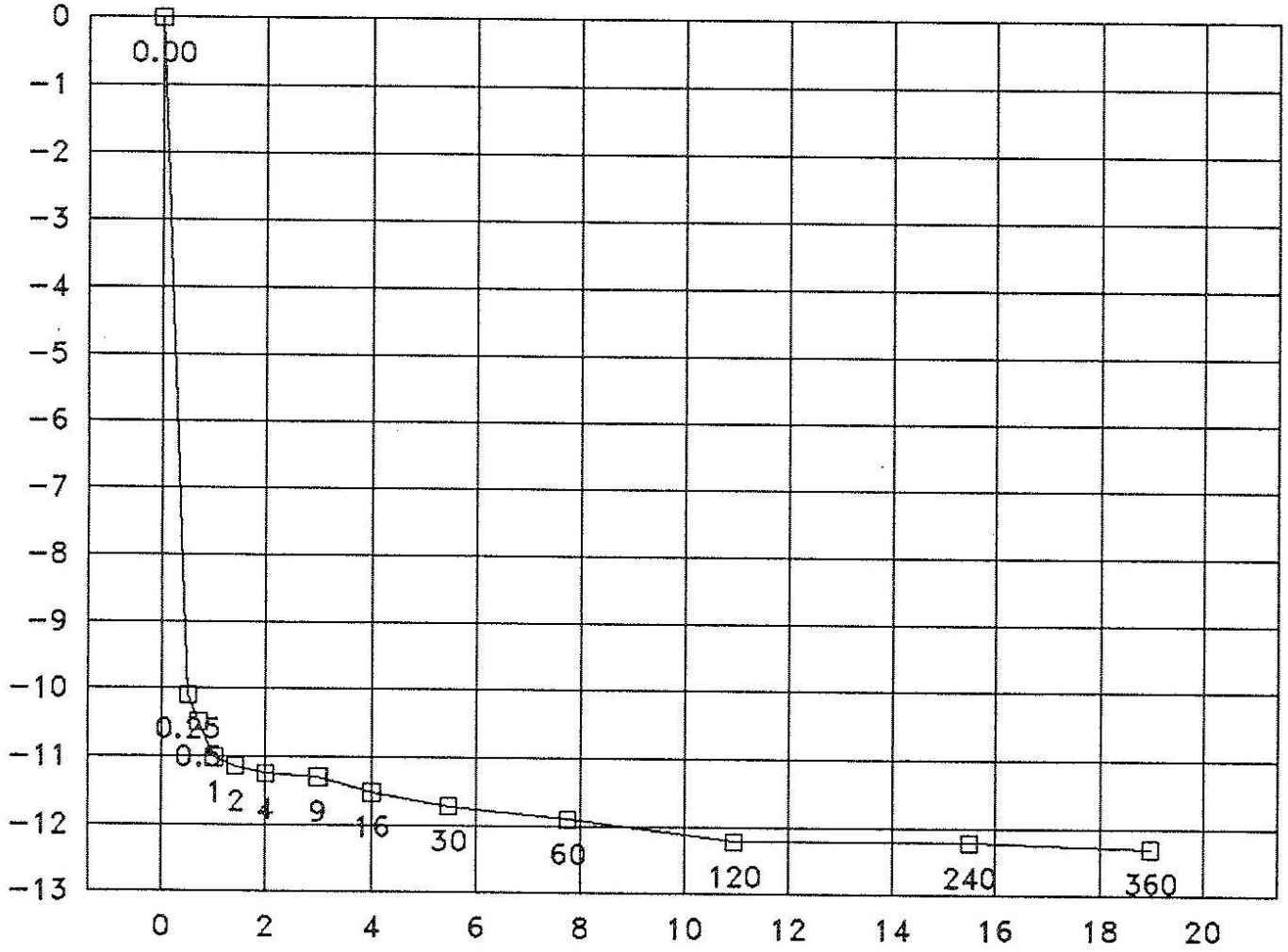


Table 3-5. Summary of Flexible Wall Permeability Test Results, West Lake Landfill

Sample Number	Sample Length (cm)	Sample Diameter (cm)	Sample Dry Density (pcf)	Maximum Dry Density (pcf)	Compaction (%)	Initial Moisture Content (%)	Optimum Moisture Content (%)	Effective Pressure (psi)	Back Pressure (psi)	Gradient	Average Permeability (cm/sec)
PZ-101-SS 6-8	7.99	7.22	91.7	---	---	24.4	---	6	94	2	3×10^{-4}
PZ-102-SS 4-6	8.82	7.07	92.2	---	---	28.2	---	5	95	9	8×10^{-7}
PZ-103-SS 14-16	7.73	7.18	97.7	---	---	28.3	---	13	87	4	2×10^{-6}
PZ-104-KS 6-8	9.11	7.14	95.7	---	---	23.6	---	6	94	24	2×10^{-7}
PZ-106-KS 6-8	8.89	7.14	103.0	---	---	22.2	---	6	94	5	3×10^{-6}
PZ-106-KS GTS-1 201.9-202.5	7.63	4.50	151.9	---	---	4.5	---	153	98	129	$<1.1 \times 10^{-10}$
PZ-106-KS GTS-2 229.6-230.1	7.66	4.47	148.0	---	---	4.4	---	170	88	94	1.5×10^{-10}
PZ-200-SS 6-8	9.59	7.17	95.3	---	---	27.5	---	6	94	4	2×10^{-6}
PZ-201-SS 26-28	8.11	7.13	86.4	---	---	34.5	---	23	77	14	3×10^{-6}
PZ-202-SS 6-8	8.08	7.10	96.4	---	---	26.7	---	6	94	10	3×10^{-7}
PS-1 10	9.56	7.23	100.8	105.0	96	18.4	19.0	5	95	6	2×10^{-7}
PS-2 7	9.55	7.24	101.7	106.0	96	17.5	17.5	5	95	10	3×10^{-7}
LR-103	10.16	7.22	79.9	---	---	37.4	17.5	5	95	3	2×10^{-4}