

# NEIC

EPA-330/2-82-001

SUMMARY OF PINE RIVER RESERVOIR  
SEDIMENT SAMPLING SURVEY

St. Louis, Michigan  
November 20-22, 1981

April 1982

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National Enforcement Investigations Center, Denver

U.S. Environmental Protection Agency



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## INTRODUCTION

In June 1980\* NEIC collected water and sediment samples from the Pine River to document the contamination contributed to the Pine River by previous operations of the Velsicol Chemical Corporation (VCC) at its St. Louis, Michigan facility.

At the request of Region 5, Enforcement Division, additional sediment sampling was conducted November 20 to 22, 1981 to supplement the June 1980 sampling and to more adequately define the areal and vertical distribution of total DDT, HBB, and PBB in the Pine River Reservoir. This new information was needed to support settlement negotiations between the regulatory agencies and VCC.

## CONCLUSIONS

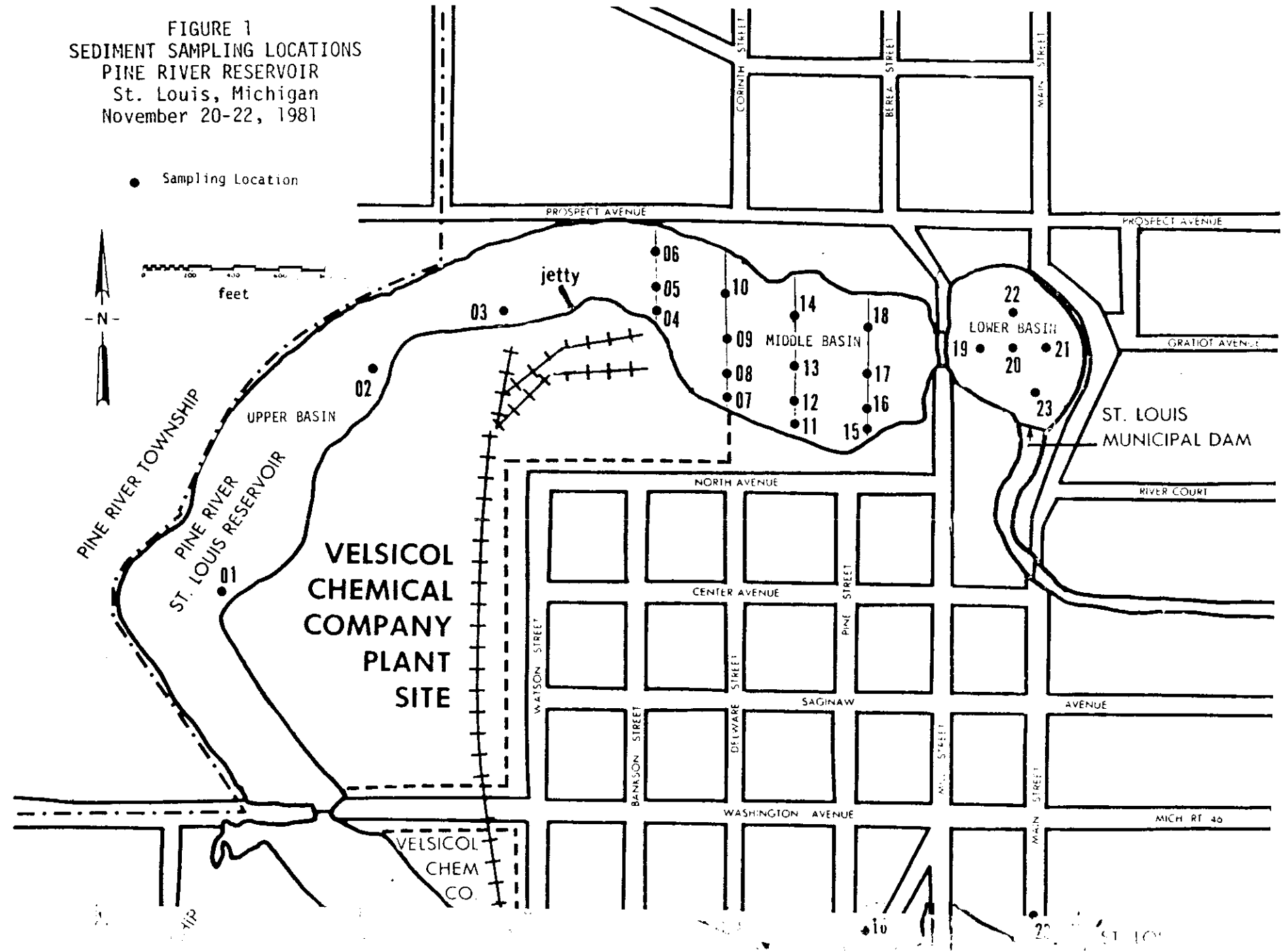
The NEIC sediment sampling data showed widespread contamination of the Pine River Reservoir by DDT, hexabromobenzene (HBB), and polybrominated biphenyl (PBB). An estimated 56,000 lb DDT, 10,000 lb HBB, and 800 lb PBB are contained in the Pine River Reservoir sediments.

The highest levels of contaminants were found in the middle basin (sampling Stations 04 to 18) of the reservoir located between the VCC Plant Site Jetty and the Mill Street Bridge [Figure 1]. Within this basin, the highest concentration of contaminants was found near the VCC plant site boundary, offshore from the former discharge points for the VCC organics production area. The maximum concentrations of total DDT, HBB, and PBB found in the segments of cores were 26,000 µg/g, 9,300 µg/g, and 330 µg/g, respectively. The lower basin (sampling Stations 19 to 23), located between

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\* EPA-330/2-8-031 - Pine River Contamination Survey, St. Louis, Michigan - October 1980.  
EPA-330/2-8-030 - Investigation for Hazardous Waste Contamination, Velsicol Chemical Corporation Plant Site, St. Louis, Michigan - October 1980.

FIGURE 1  
SEDIMENT SAMPLING LOCATIONS  
PINE RIVER RESERVOIR  
St. Louis, Michigan  
November 20-22, 1981



the Mill Street Bridge and the St. Louis Dam, was found to be contaminated, but to a lesser degree than the middle basin. Maximum concentrations of total DDT, HBB, and PBB found in this area were 560 µg/g, 180 µg/g, and 5.2 µg/g, respectively. In the upper basin (sampling Stations 01, 02, and 03), located upstream of the VCC plant site jetty, the contaminant levels were lower with maximum total DDT, HBB, and PBB concentrations of 25 µg/g, 3.2 µg/g, and 2.8 µg/g, respectively.

Regardless of the areal distribution of the contaminants, the highest DDT levels were found in the deeper portions of the sediment cores with lower concentrations in the top 4 inches. High levels of DDT are also found in surface sediments (4,000 µg/g at Station 14) in areas of the reservoir where scouring had apparently exposed the older sediments. The highest levels of HBB and PBB were found in the top (0 to 16 in.) of the cores. Logically, the HBB and PBB should be more prevalent in the surface sediments, and DDT should be prevalent in the deeper sediments because HBB and PBB were produced until the mid-1970s, while DDT production ceased in 1959.

#### METHODS

Sediment cores were collected and water and sediment depths measured at 23 sampling locations [Figure 1, Table 1]. The sediment depths were measured by penetrating the reservoir bottom with a ½ in. diameter steel rod until resistance was met. Water depth was obtained by dropping a disc (approximately 16 in. diameter) into the reservoir bottom and measuring the submerged portion of the attached cord.

The sediment samples were collected in 1-3/4 in. I.D. hexane-rinsed aluminum or galvanized steel core tubes. To facilitate sampling and handling, core tubes of 3, 4, or 6 ft in length were used. The samples were collected by slowly pushing or driving the core tubes into the sediment until a sediment layer, which was compacted hard enough to plug the end of the core tube, was reached. Care was taken to allow several inches of water to

Table 1  
SEDIMENT SAMPLING LOCATIONS  
PINE RIVER RESERVOIR  
ST. LOUIS, MICHIGAN  
November 20-22, 1981

| Core Sampling | Sampling Date & Time (ft) | Depth of Water (ft) | Depth of Sediment (ft) | Core Tube Length | Station Description   |
|---------------|---------------------------|---------------------|------------------------|------------------|---|
| 01            | 11/20/81<br>1315 hrs      | 8                   | 1.5                    | 3                | 50 feet from the shoreline adjacent to the Velsicol Chemical Corporation (VCC) plant site, 2100 feet upstream of the VCC jetty.         |
| 02            | 11/20/81<br>1340 hrs      | 2                   | 1.5                    | 3                | Same as above (01) except 900 feet upstream of the VCC jetty.   |
| 03            | 11/20/81<br>1420 hrs      | 4                   | 9                      | 4                | Same as above (01) except 300 feet upstream of the VCC jetty.   |
| 04            | 11/20/81<br>1530 hrs      | 1                   | 8                      | 4                | 50 feet from the shoreline adjacent to the VCC plant site on the north-south transect located 1200 feet west of the Mill Street Bridge. |
| 05            | 11/20/81<br>1545 hrs      | 1.5                 | 9                      | 6                | Same as above (04) except 150 feet from the VCC shoreline.  |
| 06            | 11/20/81<br>1600 hrs      | 5                   | 9                      | 6                | Same as above (04) except 300 feet from the VCC shoreline.  |
| 07            | 11/21/81<br>1125 hrs      | 4                   | 6                      | 4                | 50 feet from the shoreline adjacent to the VCC plant site on the north-south transect located 900 feet west of the Mill Street Bridge.  |
| 08            | 11/21/81<br>1140 hrs      | 3                   | 3                      | 3                | Same as above (07) except 150 feet from the VCC shoreline.  |
| 09            | 11/21/81<br>1200 hrs      | 3                   | 4.5                    | 4                | Same as above (07) except 300 feet from the VCC shoreline.  |
| 10            | 11/21/81<br>1215 hrs      | 3                   | 7                      | 6                | Same as above (07) except 500 feet from the VCC shoreline.  |
| 11            | 11/21/81<br>1230 hrs      | 5.5                 | 4                      | 4                | 50 feet from the shoreline adjacent to the VCC plant site on the north-south transect located 600 feet west of the Mill Street Bridge.  |
| 12            | 11/21/81<br>1245 hrs      | 5                   | 8                      | 6                | Same as above (11) except 150 feet from the VCC shoreline.  |
| 13            | 11/21/81<br>1300 hrs      | 4                   | 8                      | 6                | Same as above (11) except 300 feet from the VCC shoreline.  |
| 14            | 11/21/81<br>1335 hrs      | 4                   | 2                      | 4                | Same as above (11) except 500 feet from the VCC shoreline.  |
| 15            | 11/21/81<br>1430 hrs      | 7                   | 7                      | 6                | 50 feet from the shoreline adjacent to the VCC plant site on the north-south transect located 300 feet west of the Mill Street Bridge.  |
| 16            | 11/21/81<br>1445 hrs      | 5                   | 8                      | 6                | Same as above (15) except 150 feet from the VCC shoreline.  |
| 17            | 11/21/81<br>1500 hrs      | 5                   | 8                      | 6                | Same as above (15) except 300 feet from the VCC shoreline.  |
| 18            | 11/21/81<br>1520 hrs      | 7                   | 3                      | 4                | Same as above (15) except 500 feet from the VCC shoreline.  |
| 18-dup        | 11/21/81<br>1520 hrs      | 7                   | 3                      | 4                | Same as above (18)  |
| 19            | 11/22/81<br>0930 hrs      | 8                   | 2                      | 3                | 150 feet east of the midpoint of the Mill Street Bridge.  |
| 20            | 11/22/81<br>0945 hrs      | 8                   | 2                      | 3                | 300 feet east of the midpoint of the Mill Street Bridge.  |
| 21            | 11/22/81<br>1000 hrs      | 7                   | 4                      | 3                | 450 feet east of the midpoint of the Mill Street Bridge.  |
| 21 dup        | 11/22/81<br>1000 hrs      | 7                   | 4                      | 3                | Same as above (21)  |
| 22            | 11/22/81<br>1015 hrs      | 8                   | 6                      | 3                | 150 feet north of Station 20.   |
| 23            | 11/22/81<br>1020 hrs      | 8                   | 3                      | 3                | 150 feet north of the midpoint of the City of St. Louis municipal dam.  |

remain in the top of the core tubes to ensure that there was minimal disturbance of the surface sediment. The filled tubes were extracted from the bottom, the ends were sealed with aluminum foil, and then they were capped and frozen in an upright position.

After freezing, the 4 and 6 ft core tubes were cut in half, the open ends covered with aluminum foil, and stored in dry ice. At the NEIC laboratory, the frozen samples were extruded from the core tubes by warming the outside of the tubes with water and pushing the frozen cores from the tubes. After extrusion, each frozen core was observed and the physical characteristics recorded [Table 2]. The top 4 inches of each sediment sample was separated from the core and the remainder divided, from top to bottom, in 1 ft intervals or fractions of a foot, as applicable. All segments of each sediment core were wrapped in aluminum foil. These segments were subsequently thawed, thoroughly mixed, and analyzed for PBB, total DDT, and HBB. Complete analytical methodology is shown in Attachment A. NEIC chain-of-custody and document control procedures were followed throughout the survey.

Table 2  
 SEDIMENT CORE DESCRIPTIONS  
 PINE RIVER RESERVOIR  
 St. Louis, Michigan  
 November 20-22, 1981

| Station Number | Extrusion Date and Time | Total Length (in.) | Core Segment (in.)            | Visual Description*   |
|----------------|-------------------------|--------------------|-------------------------------|---|
| 01             | 12/1/81<br>1200 hrs     | 13                 | 0-3<br>3-10<br>10-13          | gray-brown floc grading into<br>gray-brown silt<br>gray-brown silt<br>gray-black sludge                                     |
| 02             | 11/30/81<br>1400 hrs    | 17                 | 0-4<br>8-14<br>14-17          | brown sandy silt<br>white silt (MgO <sub>2</sub> )<br>black sludge  |
| 03             | 12/1/81<br>0955 hrs     | 24                 | 0-6<br>6-10<br>10-24          | black sludge<br>gray-white silt (MgO <sub>2</sub> )<br>white silt (MgO <sub>2</sub> )                                       |
| 04             | 11/30/81<br>1425 hrs    | 13                 | 0-9<br>9-13                   | dark gray-brown sandy silt<br>black silt  |
| 05             | 11/30/81<br>1335 hrs    | 40                 | 0-4<br>4-13<br>13-15<br>15-40 | brown-gray floc grading into<br>gray-brown silt<br>gray-black sludge<br>white silt (MgO <sub>2</sub> )<br>gray-black sludge |
| 06             | 11/30/81<br>1440 hrs    | 32                 | 0-4<br>4-13<br>13-32          | gray-brown floc grading into<br>gray-brown sandy silt<br>gray sandy silt<br>gray-white silt                                 |
| 07             | 11/30/81<br>1450 hrs    | 36                 | 0-6<br>6-20<br>20-36          | brown floc<br>black silty sand<br>gray-black sandy silt   |
| 08             | 11/30/81<br>1325 hrs    | 28                 | 0-4<br>4-28                   | brown-gray floc grading into<br>brown-gray silt<br>gray-black silt  |
| 09             | 11/30/81<br>1315 hrs    | 34                 | 0-34                          | gray-black silt   |
| 10             | 11/30/81<br>1500 hrs    | 24                 | 0-8<br>8-14<br>14-24          | gray sand with streaks of<br>white silt (MgO)<br>gray sand<br>black sandy silt  |
| 11             | 11/30/81<br>1310 hrs    | 16                 | 0-4<br>4-16                   | gray-brown floc grading into<br>gray-black silt<br>gray-black silt  |
| 12             | 11/30/81<br>1520 hrs    | 30                 | 0-3<br>3-30                   | gray-brown floc grading into<br>gray-black silt<br>gray-black silt  |
| 13             | 11/30/81<br>1300 hrs    | 46                 | 0-6<br>6-46                   | gray-brown floc grading into<br>silty gray-black<br>gray-black silt   |
| 14             | 12/1/81<br>0830 hrs     | 28                 | 0-4<br>4-8<br>8-28            | gray-brown floc grading into<br>gray-black silty sand<br>black silty sand<br>gray-brown coarse sand                         |
| 15             | 12/1/81<br>0915 hrs     | 46                 | 0-2<br>2-46                   | black floc<br>dark black sludge   |



Table 2 (Cont.)  
 SEDIMENT CORE DESCRIPTIONS  
 PINE RIVER RESERVOIR  
 St. Louis, Michigan  
 November 20-22, 1981

| Station Number | Extrusion Date and Time | Total Length (in.) | Core Segment (in.)          | Visual Description*  |
|----------------|-------------------------|--------------------|-----------------------------|--|
| 16             | 11/30/81<br>1250 hrs    | 42                 | 0-12<br>12-42               | gray-brown silt<br>black sludge  |
| 17             | 12/1/81<br>0935 hrs     | 45                 | 0-4<br>4-9<br>9-40<br>40-45 | brown floc<br>black and gray-white silt layers<br>black silt<br>brown-gray clay    |
| 18             | 11/30/81<br>1220 hrs    | 35                 | 0-11<br>11-35               | gray-brown floc grading into<br>fine gray-brown silt<br>black silt                 |
| 18-dup         | 11/30/81<br>1240 hrs    | 34                 | 0-11<br>11-34               | gray-brown floc grading into<br>fine gray brown silt<br>black silt                 |
| 19             | 12/1/81<br>1015 hrs     | 22                 | 0-3<br>3-18<br>18-22        | brown-gray floc grading into<br>black silt<br>black sludge<br>fine gray-brown silt |
| 20             | 11/30/81<br>1345 hrs    | 27                 | 0-5<br>5-19<br>19-27        | gray-black silt<br>black sludge<br>light brown clay                                |
| 21             | 12/1/81<br>1035 hrs     | 21                 | 0-5<br>5-13<br>13-21        | brown-gray floc grading into<br>black silt<br>black silt<br>gray-black silt        |
| 21 dup         | 12/1/81<br>1135 hrs     | 14                 | 0-4<br>4-14                 | brown-gray floc grading<br>into black silt<br>black silt                           |
| 22             | 12/1/81<br>1145 hrs     | 23                 | 0-6<br>6-18<br>18-23        | brown-gray floc grading<br>into black silt<br>black silt<br>gray-black silt        |
| 23             | 12/1/81<br>1200 hrs     | 34                 | 0-3<br>3-28<br>28-34        | gray-brown floc<br>black silt<br>gray-brown silty sand                             |

\* Descriptions are from visual observations of the outside of the frozen cores after extrusion from the core tubes.

## SURVEY FINDINGS

### PHYSICAL OBSERVATIONS

Total sediment depth at the sampling Stations varied between 1.5 and 9 ft [Table 1]. The deepest sediments (8 to 9 ft) were found in the extreme upper end (Stations 04, 05, and 06) and lower end (Stations 12, 13, 16, and 17) of the middle basin.

After extrusion of the sediment cores, the physical characteristics of the sediment cores were observed and recorded [Table 2]. Many of the cores (78%) contained a surface layer (1 to 6 inches) of gray-brown floc (light silty filamentous material). Nearly all the cores contained layers of varying thickness of black or gray-black sludge. A sulfurous odor was noticed in the cores which contained this black sludge. The strongest odors were from samples collected at Stations 07, 08, 15, 19, 20, and 23. Many of the cores contained layers of white sludge which, according to Company officials, is probably magnesium oxide (MgO). Both the black and white layers had a very small grain size, usually indiscernible to the naked eye.

The black and white layers of materials seen in the cores varied in thickness and depth; hence, no visual correlation of the layers between sampling stations could be made. These varying depths and thicknesses of sediment layers and the differences in total sediment depths at the sampling stations showed the expected variability in deposition rates within the reservoir.

### ANALYTICAL RESULTS

Approximately 56,000 lbs DDT, 10,000 lbs HBB, and 800 lbs PBB are contained in the Pine River sediments. Less than 5% of the DDT is found in the top 4 in. of sediment, but over 13% of the HBB and 57% of the PBB was found in the top 4 in. of the cores. These loadings were calculated by

integrating sediment density, contaminant concentration by depth, and the areas assigned to each of the sampling Stations [Appendix A].

The highest concentrations of total DDT, HBB, and PBB [Table 3] were found in the middle basin of the Pine River Reservoir (Stations 04-18) which extends from the VCC plant site jetty to the Mill Street Bridge [Figure 1]. Average maximum total DDT, HBB, and PBB concentrations\* in the samples collected in this basin were 3,500 µg/g, 1,000 µg/g, and 42 µg/g, respectively. Wastewater from the former VCC organics production area was discharged to this portion of the basin. Within this basin, the highest total DDT concentrations were found at Stations 07 (26,000 µg/g) and 08 (8,800 µg/g). The highest concentrations of HBB were also found at Station 07 (9,300 µg/g) and 08 (2,600 µg/g). Highest PBB concentrations were found at Station 04 (330 µg/g), 10 (66 µg/g), 07 (64 µg/g), and 08 (58 µg/g). Stations 07 and 08 are the Stations nearest to the former organics wastewater discharges, and they are close to the location where the highest total DDT concentration (44,000 µg/g) was found during the June 1980 NEIC survey.\*\* Contaminant concentrations within the middle basin generally decreased [Figures 2, 3, and 4] toward the northern shore. The old river channel is located along this shoreline.

Compared to the middle basin, the average concentrations of contaminants in the upper basin are low. Average maximum core concentrations of total DDT, HBB, and PBB of 11 µg/g, 1.8 µg/g, and 1.5 µg/g, respectively, were found in this portion of the reservoir which extends from the Washington Street Bridge to the VCC plant site jetty (Stations 01, 02, and 03).

The lower basin (Stations 19 to 23) of the reservoir between the Mill Street Bridge and the St. Louis Municipal Dam was found to be contaminated; however, contaminant concentrations were lower than the levels found in the middle basin. Average maximum core concentrations of total DDT, HBB, and PBB found in this area were 310 µg/g, 81 µg/g, and 4.2 µg/g, respectively.

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\* The average maximum concentrations were calculated by averaging the concentrations of the most contaminated segment of each core.

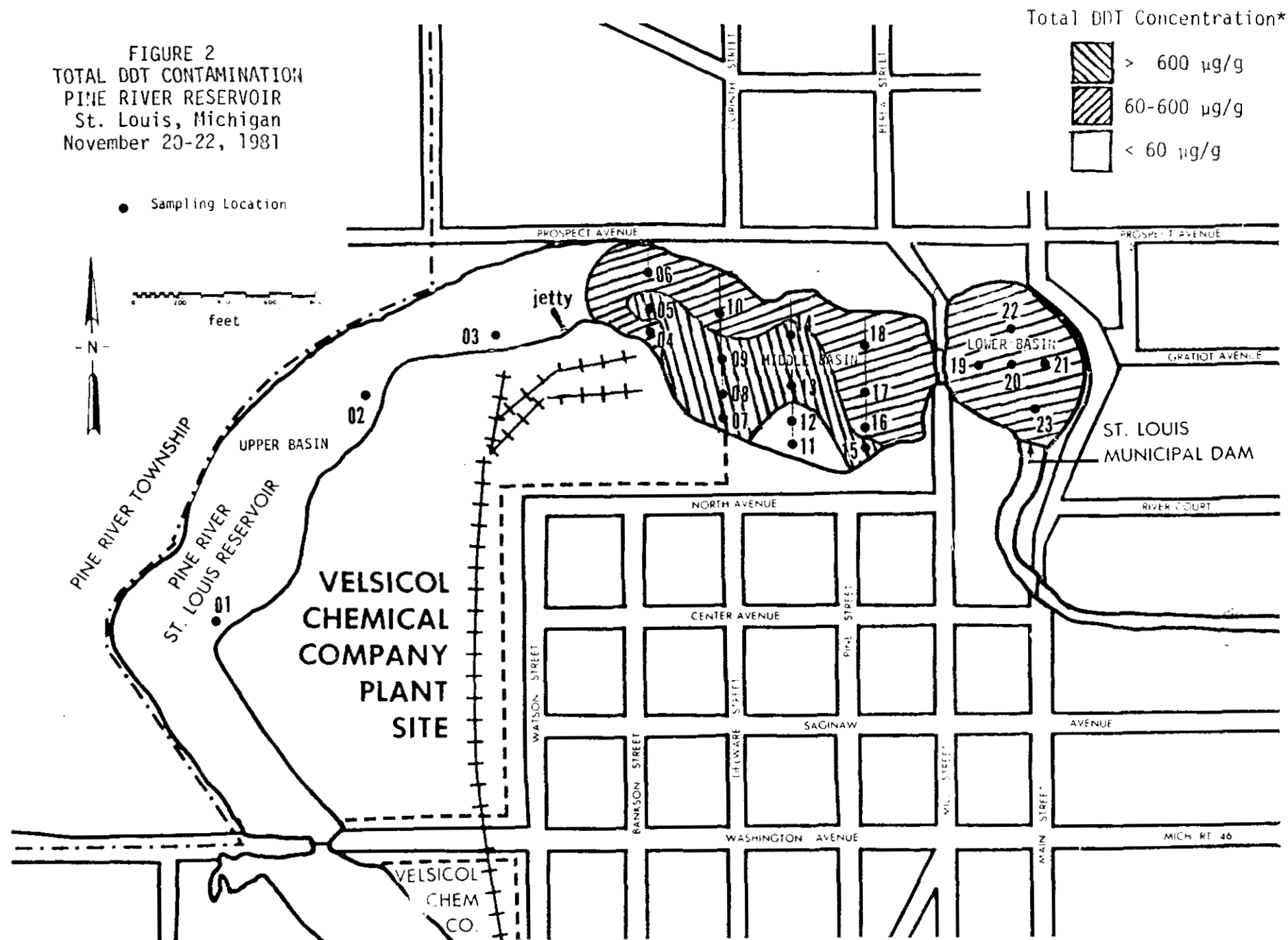
\*\* EPA-330/2-80-031 - Pine River Contamination Survey, St. Louis, Michigan - October 1980.

Table 3  
TOTAL DDT, HBB, AND PBB CONCENTRATIONS  
IN SEDIMENTS BY BASIN  
PINE RIVER RESERVOIR  
St. Louis, Michigan  
November 20-22, 1981

| Basin                       | Sample<br>Size<br>Stations | Total DDT                              |                                  | HBB                                    |                                  | PBB                                    |                                  |
|-----------------------------|----------------------------|--|----------------------------------|--|----------------------------------|--|----------------------------------|
|                             |                            | Avg.- Maximum<br>Concentration<br>µg/g | Maximum<br>Concentration<br>µg/g | Avg.- Maximum<br>Concentration<br>µg/g | Maximum<br>Concentration<br>µg/g | Avg.- Maximum<br>Concentration<br>µg/g | Maximum<br>Concentration<br>µg/g |
| UPPER<br>Stations<br>01-03  | 3                          | 11                                     | 25                               | 1.8                                    | 3.2                              | 1.5                                    | 2.8                              |
| MIDDLE<br>Stations<br>04-18 | 15                         | 3500                                   | 26,000                           | 1000                                   | 9300                             | 42                                     | 330                              |
| LOWER<br>Stations<br>19-23  | 5                          | 300                                    | 560                              | 81                                     | 180                              | 4.2                                    | 5.2                              |

\* This average maximum concentration was calculated by averaging the concentrations of the most contaminated segment of each core.

FIGURE 2  
TOTAL DDT CONTAMINATION  
PINE RIVER RESERVOIR  
St. Louis, Michigan  
November 20-22, 1981



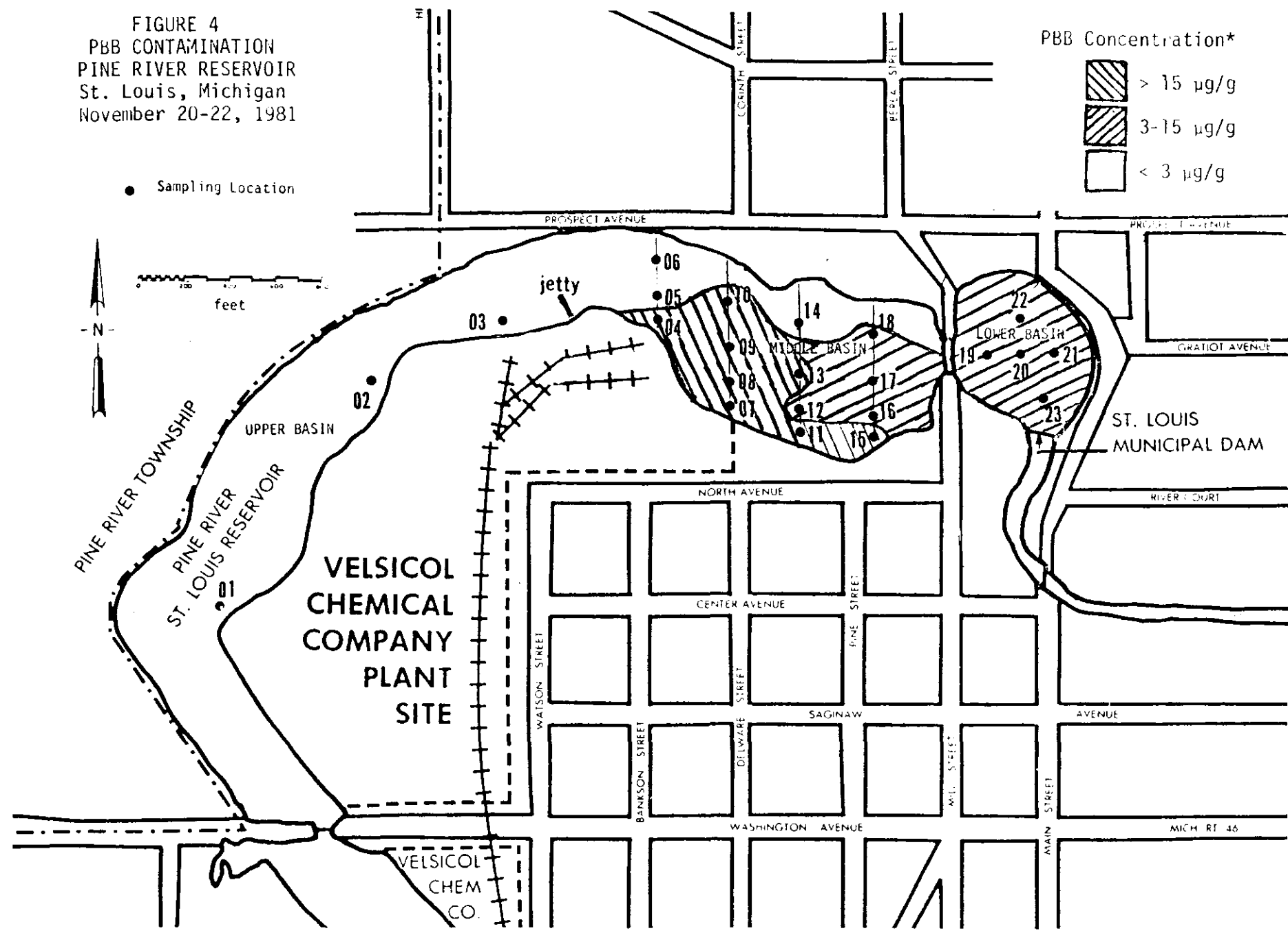
\* Based on maximum concentrations found in individual sediment cores

FIGURE 3  
HBB CONTAMINATION  
PINE RIVER RESERVOIR  
St. Louis, Michigan  
November 20-22, 1981



\* Based on maximum concentrations found in individual sediment cores

FIGURE 4  
 PBB CONTAMINATION  
 PINE RIVER RESERVOIR  
 St. Louis, Michigan  
 November 20-22, 1981



\* Based on maximum concentrations found in individual sediment cores

A concentration profile by depth [Table 4] was developed by summarizing the data from each of 5 specified depths (0 to 4 in., 4 to 16 in., 16 to 28 in., 28 to 40 in., and 40 in. and below) from the 20 sampling Stations in the middle and lower basins (Stations 04 to 23).<sup>\*</sup> This profile showed the highest average total DDT concentrations were found to be in the deeper sediment layers (16 to 28 in. and 28 to 40 in. layers). An average total DDT concentration of 960 µg/g was found in the 16 to 28 in. segments of the sediment cores, and 1,000 µg/g was found in the 18 to 40 in. segments.

Conversely, lower concentrations of total DDT were generally found in the surface portion (0 to 4 in.) of the sediment cores. One station (14), however, had a surface sediment total DDT concentration of 4,000 µg/g. This high concentration is probably due to the deposition and erosion patterns in the reservoir. Station 14 is located at the edge of the main river channel which runs along the north side of the reservoir. The velocity of the currents would be expected to be higher in this area of the reservoir during high flow periods, increasing scouring and exposing the older and deeper layers of sediment which contain higher total DDT levels. The analyses of the three cores which were greater than 40 in. in length showed very low concentrations of contaminants below the 40 in. level.

Maximum HBB and PBB concentrations were generally found to be in the upper sediments (0 to 16 in.). A maximum HBB concentration of 9,300 µg/g was found in the 4 to 16 in. layer at Station 07, and a maximum PBB concentration of 330 µg/g was found in the 0 to 4 in. layer at Station 04.

Complete analytical data for all the sediment samples, as well as the analytical methods and associated quality control data, can be seen in Appendix B.

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<sup>\*</sup> Sediment cores were divided into two to five segments depending on each core's length.



Table 4  
TOTAL DDT, HBB, AND PBB CONCENTRATIONS<sup>1</sup>  
IN SEDIMENTS BY BASIN  
PINE RIVER RESERVOIR  
St. Louis, Michigan  
November 20-22, 1981

| Core Seg.<br>Depth<br>(in.) | Sample<br>Size<br>Stations | Total DDT   |                                  | HBB   |                                  | PBB   |                                  |
|-----------------------------|----------------------------|---|----------------------------------|---|----------------------------------|---|----------------------------------|
|                             |                            | Avg. <sup>2</sup> -Maximum<br>Concentration<br>µg/g | Maximum<br>Concentration<br>µg/g | Avg. <sup>2</sup> -Maximum<br>Concentration<br>µg/g | Maximum<br>Concentration<br>µg/g | Avg. <sup>2</sup> -Maximum<br>Concentration<br>µg/g | Maximum<br>Concentration<br>µg/g |
| 0-4                         | 19                         | 34  | 4,000                            | 61  | 2,600                            | 8.6   | 330                              |
| 4-16                        | 19                         | 159   | 2,900                            | 255   | 9,300                            | 7.4   | 66                               |
| 16-28                       | 17                         | 957   | 26,000                           | 5.8   | 100                              | 0   | 1                                |
| 28-40                       | 9 <sup>3</sup>             | 1014  | 4,800                            | 0.13  | 44                               | 0   | 0                                |
| 40-46                       | 3                          | 3.3   | 9.5                              | 0   | 0                                | 0   | 0                                |

1 Dry weight concentrations

2 This average was derived by comparing the mean concentration of the entire set (Stations 04-23) at the various depths with individual values, dismissing values which were more than 2 standard deviations from the mean, and calculating a new average with the remaining values. This average is not the true average but an expected average with depth. The high values dismissed are valid concentrations although not typical for the majority of the cores.

3 A sample size of 8 was used to derive the average concentrations for HBB.

**APPENDIX A**

**TOTAL DDT, HBB, AND PBB LOADING APPROXIMATIONS**

TOTAL DDT, HBB, AND PBB LOADING APPROXIMATIONS\*  
PINE RIVER RESERVOIR  
St. Louis, Michigan

A-1

| Sample<br>Number* | % H <sub>2</sub> O | Sediment<br>Density<br>lbs/ft <sup>3</sup> | Area<br>ft <sup>3</sup> | Total DDT<br>Loading<br>lbs | HBB<br>Loading<br>lbs | PBB<br>Loading<br>lbs |
|-------------------|--------------------|--|-------------------------|-----------------------------|-----------------------|-----------------------|
| 01-1              | 64.3               | 80.6                                       | -                       | -                           | -                     | -                     |
| 01-2              | 63.9               | 81.0                                       | -                       | -                           | -                     | -                     |
| 02-1              | 55.4               | 87.3                                       | 185,760                 | 12.1                        | 2.41                  | 2.41                  |
| 02-2              | 48.2               | 93.6                                       | "                       | 63.0                        | 9.91                  | 6.84                  |
| 03-1              | 64.9               | 80.1                                       | 216,000                 | 3.44                        | 1.94                  | 1.70                  |
| 03-2              | 64.1               | 82.9                                       | "                       | 125                         | -                     | -                     |
| 03-3              | 51.8               | 90.2                                       | "                       | 235                         | -                     | -                     |
| 04-1              | 34.8               | 107.2                                      | 54,000                  | 340                         | 18.9                  | 415                   |
| 04-2              | 45.2               | 96.5                                       | "                       | 343                         | 257                   | 65.7                  |
| 05-1              | 63.2               | 81.3                                       | 36,000                  | 5.03                        | 33.0                  | 0.34                  |
| 05-2              | 65.3               | 79.9                                       | "                       | 24.0                        | 6.19                  | -                     |
| 05-3              | 68.1               | 78.1                                       | "                       | 888                         | -                     | -                     |
| 05-4              | 61.6               | 82.4                                       | "                       | -                           | -                     | -                     |
| 06-1              | 57.1               | 85.8                                       | 54,000                  | 1.71                        | 7.95                  | 1.46                  |
| 06-2              | 43.7               | 98.8                                       | "                       | 10.5                        | 84.1                  | 1.68                  |
| 06-3              | 60.5               | 83.3                                       | "                       | 13.9                        | 1.63                  | -                     |
| 06-4              | 51.9               | 90.2                                       | "                       | -                           | -                     | -                     |
| 07-1              | 72.0               | 75.8                                       | 18,000                  | 12.7                        | -                     | 1.78                  |
| 07-2              | 71.5               | 76.0                                       | "                       | 148                         | 3626                  | 25.0                  |
| 07-3              | 61.3               | 82.7                                       | "                       | 14980                       | 57.6                  | -                     |
| 07-4              | 63.4               | 81.2                                       | "                       | 2.51                        | 0.53                  | -                     |
| 08-1              | 70.3               | 76.7                                       | 50,400                  | 13.8                        | 994                   | 22.2                  |
| 08-2              | 70.8               | 76.5                                       | "                       | 3265                        | 2027                  | -                     |
| 08-3              | 63.2               | 81.3                                       | "                       | 14940                       | -                     | -                     |
| 09-1              | 65.6               | 79.8                                       | 54,000                  | 16.3                        | 69.2                  | 8.90                  |
| 09-2              | 68.3               | 78.0                                       | "                       | 801                         | 32                    | 24                    |
| 09-3              | 59.6               | 84.0                                       | "                       | 143                         | -                     | -                     |
| 09-4              | 62.4               | 81.8                                       | "                       | 9.13                        | -                     | -                     |
| 10-1              | 68.0               | 78.2                                       | 57,600                  | 2.79                        | 26.4                  | 6.73                  |
| 10-2              | 64.1               | 80.7                                       | "                       | 751                         | 734                   | 110                   |
| 10-3              | 56.3               | 86.6                                       | "                       | 17.0                        | 30.5                  | -                     |
| 11-1              | 68.5               | 77.9                                       | 25,200                  | 3.5                         | 20.0                  | 1.0                   |
| 11-2              | 65.6               | 79.8                                       | "                       | 22.8                        | 422                   | 14.5                  |
| 12-1              | 68.7               | 77.8                                       | 32,400                  | 3.94                        | 23.7                  | 1.31                  |
| 12-2              | 63.5               | 81.2                                       | "                       | 15.4                        | 163                   | 7.68                  |
| 12-3              | 55.9               | 86.9                                       | "                       | -                           | -                     | -                     |
| 13-1              | 67.1               | 78.7                                       | 61,200                  | 7.92                        | 23.2                  | 2.22                  |
| 13-2              | 67.7               | 78.3                                       | "                       | 24.8                        | 774                   | 38.7                  |
| 13-3              | 67.4               | 78.5                                       | "                       | 345                         | 43.9                  | 1.57                  |
| 13-4              | 62.2               | 82.0                                       | "                       | 9105                        | -                     | -                     |
| 13-5              | 55.2               | 87.4                                       | "                       | 18                          | -                     | -                     |
| 14-1              | 66.5               | 79.1                                       | 64,000                  | 2289                        | 3.26                  | 1.55                  |
| 14-2              | 13.5               | 140.0                                      | "                       | 243                         | -                     | -                     |
| 14-3              | 15.1               | 137.0                                      | "                       | -                           | -                     | -                     |
| 15-1              | 71.9               | 75.8                                       | 12,960                  | 1.93                        | 7.36                  | 0.37                  |
| 15-2              | 68.9               | 77.7                                       | "                       | 6.58                        | 207                   | 5.01                  |
| 15-3              | 67.1               | 78.7                                       | "                       | 1804                        | 18                    | -                     |
| 15-4              | 58.8               | 84.5                                       | "                       | 1940                        | 19.9                  | -                     |

APPENDIX B

COMPLETE ANALYTICAL DATA AND METHODS  
AND ASSOCIATED QUALITY CONTROL DATA

ENVIRONMENTAL PROTECTION AGENCY  
OFFICE OF ENFORCEMENT  
NATIONAL ENFORCEMENT INVESTIGATIONS CENTER  
BUILDING 53, BOX 25227, DENVER FEDERAL CENTER  
DENVER, COLORADO 80225

B-1

to Russell Forba, Project Coordinator

DATE January 14, 1982

FROM Charles P. Rzeszutko, Chemist  
THRU: Dean F. Hill, Chief *DFH*  
Pesticide and Toxic Substances Branch  
SUBJECT Project #624, Pine River, St. Louis, MI

Attached you will find the results of analysis for all core samples received for Project #624. All cores were analyzed for DDT and related compounds, hexabromobenzene (HBB), and polybrominated biphenyls (PBB). Methodology and quality control data are provided. Results previously reported on December 16, 1981, are included in this report.

If you have any questions, please contact me at your convenience.

cc: R. Laidlaw  
T. Meiggs  
Attachments

All samples were screened for compounds of interest by packed column electron-capture gas chromatography. Based on the screening results, high-level samples were simply diluted, whereas low-level samples were cleaned up by column chromatography. All samples requiring dilutions were diluted to the appropriate levels with hexane. All samples that did not require a dilution were cleaned up using Florisil column chromatography. The sample extract was placed on the head of a glass column packed with 20 grams of activated Florisil and eluted with 200 mls of 6% ethyl ether in hexane. The fraction was concentrated to less than 25 mls using a Kuderna-Danish evaporation apparatus and further concentrated to an appropriate volume using a nitrogen blowdown apparatus.

All sample extracts were analyzed by fused silica capillary column electron-capture gas chromatography using a 15 meter DB-5 column and a 25 meter OV-101 column. All extracts were analyzed for (1) Total DDT's, which included o,p'-DDE, p,p'-DDE, o,p'-DDD, p,p'-DDD, o,p'-DDT, p,p'-DDT; (2) hexabromobenzene (HBB); and (3) polybrominated biphenyls (PBB).

Several of the sample extracts were also analyzed for these compounds by gas chromatography/mass-spectroscopy (GC/MS).

NOTE: The following samples were extracted in the same manner as described above with the exception that a 10g sample size was weighed-out with 5 g of anhydrous  $\text{Na}_2\text{SO}_4$  and extracted with 20 mls of 50% acetone in hexane for the first extraction: 09-1, 09-2, 09-3, 11-1, 11-2, 13-1, 13-2, 13-3, 16-1, 16-2, 16-3, 18-1, 18-2, 18-3, 18-1 Dup., 18-2 Dup., and 18-3 Dup.

## RESULTS

The results of analysis by fused silica capillary column electron capture gas chromatography are given in Table 1. All results were calculated on a dry weight basis. Also listed in this table are the results for the percent moisture determinations for each core section. The results of analysis by GC/MS for several selective samples are listed in Table 2. A list of the gas chromatographic conditions are provided in Table 3.

Table 1  
RESULTS

| Sample # | % Moisture | Concentrations (µg/g) <sup>1</sup> |                 |                 |                 |                  |                 | Total<br>DDT and Analogues | HBB             | PBB             |
|----------|------------|------------------------------------|-----------------|-----------------|-----------------|------------------|-----------------|----------------------------|-----------------|-----------------|
|          |            | DDE                                |                 | DDD             |                 | DDT              |                 |                            |                 |                 |
|          |            | o,p'                               | p,p'            | o,p'            | p,p'            | o,p'             | p,p'            |                            |                 |                 |
| 01-1     | 64.3       | ND <sup>2,6</sup>                  | 0.07            | 0.08            | 0.10            | ND <sup>3</sup>  | 0.18            | 0.43                       | 3.2             | 2.8             |
| 01-2     | 63.9       | ND <sup>6</sup>                    | 0.10            | 0.12            | 0.13            | ND <sup>3</sup>  | ND              | 0.35                       | 0.42            | 0.46            |
| 02-1     | 55.4       | ND <sup>3</sup>                    | 0.31            | 0.22            | 0.58            | 0.10             | 3.8             | 5.0                        | 1.0             | 1.0             |
| 02-2     | 48.2       | 0.06                               | 0.48            | 0.22            | 0.58            | 0.36             | 5.3             | 7.0                        | 1.1             | 0.76            |
| 03-1     | 64.9       | ND <sup>3</sup>                    | 0.32            | 0.22            | 0.57            | ND <sup>3</sup>  | 0.61            | 1.7                        | 0.96            | 0.84            |
| 03-2     | 61.1       | ND <sup>4</sup>                    | 1.1             | 4.2             | 12              | ND <sup>5</sup>  | 1.2             | 18                         | ND <sup>7</sup> | ND <sup>7</sup> |
| 03-3     | 51.8       | 0.12                               | 1.0             | 4.8             | 12              | 0.49             | 6.4             | 25                         | ND <sup>4</sup> | ND <sup>4</sup> |
| 04-1     | 34.8       | 0.27                               | 2.2             | 12              | 20              | 32               | 200             | 270                        | 15              | 330             |
| 04-2     | 45.2       | ND <sup>4</sup>                    | 7.2             | 32              | 32              | 4.8              | 47              | 120                        | 90              | 23              |
| 05-1     | 63.2       | 0.06                               | 0.48            | 0.64            | 1.5             | 0.11             | 11              | 14                         | 92              | 0.94            |
| 05-2     | 65.3       | 1.2                                | 2.8             | 4.2             | 8.8             | 0.22             | 7.2             | 24                         | 6.2             | ND <sup>5</sup> |
| 05-3     | 68.1       | 2.2                                | 5.3             | 22              | 58              | 110              | 790             | 990                        | ND <sup>5</sup> | ND <sup>5</sup> |
| 05-4     | 61.6       | ND <sup>6</sup>                    | ND <sup>6</sup> | ND <sup>3</sup> | ND <sup>3</sup> | ND <sup>3</sup>  | ND <sup>3</sup> | -                          | ND <sup>5</sup> | ND <sup>5</sup> |
| 06-1     | 57.1       | ND <sup>3</sup>                    | 0.18            | 0.32            | 1.1             | 0.19             | 0.84            | 2.6                        | 12              | 2.2             |
| 06-2     | 43.7       | 0.08                               | 0.34            | 0.62            | 0.66            | 0.21             | 1.6             | 3.5                        | 28              | 0.56            |
| 06-3     | 60.5       | 0.24                               | 0.68            | 2.1             | 2.6             | ND <sup>4</sup>  | 2.2             | 7.8                        | 0.92            | ND <sup>5</sup> |
| 06-4     | 51.9       | ND <sup>3</sup>                    | ND <sup>3</sup> | ND <sup>4</sup> | ND <sup>4</sup> | ND <sup>4</sup>  | ND <sup>4</sup> | -                          | ND <sup>5</sup> | ND <sup>5</sup> |
| 07-1     | 72.0       | 0.31                               | 1.8             | 9.7             | 24              | 4.6              | 64              | 100                        | ND <sup>5</sup> | 14              |
| 07-2     | 71.5       | 3.8                                | 9.7             | 7.0             | 220             | ND <sup>8</sup>  | 74              | 380                        | 9300            | 64              |
| 07-3     | 61.3       | 130                                | 160             | 3400            | 3700            | 7300             | 11000           | 26000                      | 100             | ND <sup>9</sup> |
| 07-4     | 63.4       | 0.06                               | 0.05            | 0.68            | 0.85            | 1.1              | 2.0             | 4.7                        | 1.0             | ND <sup>5</sup> |
| 08-1     | 70.3       | ND <sup>3</sup>                    | 2.1             | 6.0             | 17              | ND <sup>10</sup> | 11              | 36                         | 2600            | 58              |
| 08-2     | 70.8       | ND <sup>3</sup>                    | 22              | 700             | 1100            | 140              | 890             | 2900                       | 1800            | ND <sup>5</sup> |
| 08-3     | 63.2       | 21                                 | 47              | 2000            | 2200            | 1400             | 3200            | 8800                       | ND <sup>5</sup> | ND <sup>5</sup> |
| 09-1     | 65.6       | 0.12                               | 0.64            | 2.3             | 6.5             | 1.6              | 22              | 33                         | 140             | 18              |
| 09-2     | 68.3       | ND <sup>3</sup>                    | 4.5             | 180             | 260             | 32               | 130             | 600                        | 24              | 18              |
| 09-3     | 59.6       | ND <sup>3</sup>                    | ND <sup>3</sup> | 27              | 26              | 6.5              | 18              | 78                         | ND <sup>5</sup> | ND <sup>5</sup> |
| 09-4     | 62.4       | ND <sup>3</sup>                    | ND <sup>3</sup> | 2.5             | 1.6             | 0.39             | 1.0             | 5.5                        | ND <sup>5</sup> | ND <sup>5</sup> |

Table 1 (Cont'd)

| Sample #  | % Moisture | Concentrations (µg/g) <sup>1</sup> |                 |                 |                 |                  |                 | Total<br>DDT and Analogues | HBB             | PBB             |
|-----------|------------|------------------------------------|-----------------|-----------------|-----------------|------------------|-----------------|----------------------------|-----------------|-----------------|
|           |            | DDE                                |                 | DDD             |                 | DDT              |                 |                            |                 |                 |
|           |            | o,p'                               | p,p'            | o,p'            | p,p'            | o,p'             | p,p'            |                            |                 |                 |
| 18-1      | 64.0       | 0.10                               | 0.29            | 4.5             | 6.2             | 1.8              | 7.8             | 21                         | 4.3             | 1.2             |
| 18-2      | 31.3       | ND <sup>3</sup>                    | ND <sup>3</sup> | 0.12            | 0.24            | ND <sup>4</sup>  | ND <sup>4</sup> | 0.36                       | 0.58            | ND <sup>5</sup> |
| 18-3      | 61.6       | 1.0                                | 1.4             | 48              | 50              | 1.2              | 19              | 120                        | ND <sup>5</sup> | ND <sup>5</sup> |
| 18-1 Dup. | 66.3       | 0.10                               | 0.27            | 3.4             | 5.6             | 0.81             | 4.0             | 14                         | 5.0             | 1.3             |
| 18-2 Dup. | 30.2       | ND <sup>3</sup>                    | ND <sup>3</sup> | 0.16            | 0.51            | ND <sup>4</sup>  | 3.2             | 3.9                        | 0.81            | 6.8             |
| 18-3 Dup. | 56.9       | 0.56                               | 1.1             | 28              | 34              | 14               | 64              | 140                        | ND <sup>5</sup> | ND <sup>5</sup> |
| 19-1      | 56.5       | 0.08                               | 0.28            | 2.3             | 5.0             | 0.21             | 3.4             | 11                         | 34              | 3.0             |
| 19-2      | 70.5       | 1.0                                | 1.6             | 40              | 35              | ND <sup>10</sup> | 10              | 88                         | 42              | 4.8             |
| 19-3      | 34.8       | ND <sup>6</sup>                    | ND <sup>6</sup> | ND <sup>3</sup> | ND <sup>3</sup> | ND <sup>3</sup>  | ND <sup>3</sup> | -                          | ND <sup>4</sup> | ND <sup>4</sup> |
| 20-1      | 61.8       | 0.11                               | 0.38            | 1.7             | 3.9             | 0.18             | 6.7             | 1.3                        | 82              | 3.4             |
| 20-2      | 68.6       | 4.0                                | 6.0             | 170             | 160             | 12               | 210             | 560                        | 28              | ND <sup>5</sup> |
| 20-3      | 18.4       | ND <sup>3</sup>                    | ND <sup>3</sup> | 0.50            | 04.6            | ND <sup>4</sup>  | 0.10            | 1.1                        | ND <sup>5</sup> | ND <sup>5</sup> |
| 21-1      | 66.6       | 0.06                               | 0.26            | 2.0             | 4.2             | 0.16             | 2.7             | 9.4                        | 54              | 3.4             |
| 21-2      | 69.4       | 2.6                                | 3.0             | 88              | 84              | 3.1              | 18              | 200                        | 32              | ND <sup>7</sup> |
| 21-3      | 51.9       | ND <sup>6</sup>                    | ND <sup>6</sup> | ND <sup>3</sup> | ND <sup>3</sup> | ND <sup>3</sup>  | ND <sup>3</sup> | -                          | ND <sup>4</sup> | ND <sup>4</sup> |
| 21-1 Dup. | 67.9       | 0.06                               | 0.26            | 2.0             | 4.2             | 0.20             | 2.3             | 9.0                        | 52              | 3.3             |
| 21-2 Dup. | 70.0       | 2.2                                | 2.6             | 78              | 70              | ND <sup>7</sup>  | 2.3             | 160                        | 39              | ND <sup>7</sup> |
| 22-1      | 70.3       | 0.06                               | 0.32            | 2.3             | 4.8             | ND <sup>4</sup>  | 1.1             | 8.6                        | 35              | 2.1             |
| 22-2      | 72.3       | 4.5                                | 5.2             | 180             | 170             | ND <sup>7</sup>  | 7.0             | 370                        | 48              | 5.2             |
| 22-3      | 64.9       | 0.19                               | 0.30            | 5.1             | 9.6             | ND <sup>4</sup>  | 0.74            | 16                         | ND <sup>5</sup> | ND <sup>5</sup> |
| 23-1      | 66.6       | 0.08                               | 0.36            | 1.6             | 3.4             | 0.22             | 2.0             | 7.7                        | 180             | 4.4             |
| 23-2      | 67.6       | 0.70                               | 1.8             | 13              | 32              | 1.0              | 38              | 87                         | 22              | ND <sup>5</sup> |
| 23-3      | 67.1       | 3.8                                | 4.0             | 150             | 140             | ND <sup>5</sup>  | 9.7             | 310                        | ND <sup>7</sup> | ND <sup>7</sup> |
| 23-4      | 46.6       | ND <sup>6</sup>                    | ND <sup>6</sup> | ND <sup>3</sup> | ND <sup>3</sup> | ND <sup>3</sup>  | ND <sup>3</sup> | -                          | ND <sup>4</sup> | ND <sup>4</sup> |



Table 2  
GC/MS CONFIRMATION RESULTS

| Compound                | Detection<br>Limit | Concentration ( $\mu\text{g/g}$ ) <sup>1</sup> |       |       |       |       |
|-------------------------|--------------------|--|-------|-------|-------|-------|
|                         |                    | #05-3  | #08-1 | #08-2 | #08-3 | #15-4 |
| o,p'-DDE                | 10                 | ND <sup>2</sup>                                | ND    | ND    | 22    | 19    |
| p,p'-DDE                | 20                 | ND   | ND    | ND    | 38    | 25    |
| o,p'-DDD                | 50                 | ND   | ND    | 680   | 1900  | 820   |
| p,p'-DDD                | 50                 | ND   | ND    | 1100  | 2200  | 970   |
| o,p'-DDT                | 50                 | 93   | ND    | 170   | 1300  | 210   |
| p,p'-DDT                | 50                 | 720  | ND    | 780   | 3600  | 480   |
| Hexabromobenzene        | 100                | ND   | 2500  | 1800  | ND    | ND    |
| Polybrominated Biphenyl | 600                | ND   | ND    | ND    | ND    | ND    |

(1) dry weight basis

(2) ND = none detected

Table 4  
QUALITY CONTROL SUMMARY

|                           | #07-3           |       |                  | #08-3 |      |                  | #12-1 |      |                  | #16-3 |      |                  |
|---------------------------|-----------------|-------|------------------|-------|------|------------------|-------|------|------------------|-------|------|------------------|
|                           | 1               | 2     | RPD <sup>1</sup> | 1     | 2    | RPD <sup>1</sup> | 1     | 2    | RPD <sup>1</sup> | 1     | 2    | RPD <sup>1</sup> |
| <u>Duplicate Analyses</u> |                 |       |                  |       |      |                  |       |      |                  |       |      |                  |
| o,p'-DDE                  | 130             | 120   | 8                | 21    | 25   | 9                | 0.10  | 0.08 | 22               | 0.66  | 0.74 | 11               |
| p,p'-DDE                  | 160             | 160   | 0                | 47    | 59   | 23               | 0.39  | 0.48 | 21               | 0.80  | 0.84 | 5                |
| o,p'-DDD                  | 3400            | 3700  | 8                | 2000  | 2400 | 18               | 2.9   | 3.0  | 3                | 18    | 22   | 10               |
| p,p'-DDD                  | 3700            | 5000  | 30               | 2200  | 2600 | 17               | 6.4   | 7.2  | 12               | 20    | 24   | 18               |
| o,p'-DDT                  | 7300            | 8600  | 16               | 1400  | 2200 | 44               | 1.1   | 0.70 | 44               | 2.4   | 2.6  | 8                |
| p,p'-DDT                  | 11000           | 12000 | 9                | 3200  | 4600 | 36               | 3.9   | 6.4  | 48               | 12    | 14   | 15               |
| HBB                       | 100             | 100   | 0                | ND    | ND   | -                | 90    | 78   | 14               | ND    | ND   | -                |
| PBB                       | ND <sup>2</sup> | ND    | -                | ND    | ND   | -                | 5.0   | 4.0  | 22               | ND    | ND   | -                |

(1) RPD = Relative Percent Difference

(2) ND = none detected

Table 5  
SPIKE RECOVERIES

| Compound | Amount<br>Added ( $\mu\text{g}$ ) | % Recovery      |       |       |       |
|----------|-----------------------------------|-----------------|-------|-------|-------|
|          |                                   | #10-1           | #17-2 | #18-2 | #20-3 |
| o,p'-DDE | 2.5                               | 84              | 104   | 95    | 84    |
| p,p'-DDE | 2.5                               | 96              | 108   | 97    | 84    |
| o,p'-DDD | 2.5                               | 76              | 108   | 99    | 84    |
| p,p'-DDD | 2.5                               | 60              | 100   | 100   | 87    |
| o,p'-DDT | 2.5                               | 80              | 104   | 92    | 75    |
| p,p'-DDT | 2.5                               | NA <sup>1</sup> | 108   | 94    | 71    |
| HBB      | 2.5                               | NA              | 160   | 118   | 87    |
| PBB      | 2.5                               | NA              | 180   | 104   | 90    |

(1) NA = not applicable

TEST NO. C-1895PAGE 7SAMPLING STATION Sulfur Unit No. 1 DATE 1-20-73

## GAS VELOCITY DATA

| TIME  | POINT | VEL. HEAD<br>IN. H <sub>2</sub> O | TEMP.<br>°F | VELOCITY<br>FT/SEC | VEL. HEAD<br>IN. H <sub>2</sub> O | TEMP.<br>°F | VELOCITY<br>FT/SEC | VEL. HEAD<br>IN. H <sub>2</sub> O | TEMP.<br>°F | VELOCITY<br>FT/SEC |
|-------|-------|-----------------------------------|-------------|--------------------|-----------------------------------|-------------|--------------------|-----------------------------------|-------------|--------------------|
| 10:15 | 1     | .15                               | 130         | 27.5               | .15                               |             | 27.5               | .15                               |             | 27.5               |
|       | 2     | .17                               |             | 29.0               | .17                               |             | 29.0               | .17                               |             | 29.0               |
|       | 3     | .19                               |             | 29.0               | .19                               |             | 29.0               | .19                               |             | 29.0               |
|       | 4     | .18                               |             | 29.9               | .19                               |             | 29.5               | .18                               |             | 29.5               |
|       | 5     | .22                               |             | 33.0               | .23                               |             | 33.8               | .22                               |             | 33.0               |
|       | 6     | .23                               |             | 34.5               | .25                               |             | 35.2               | .23                               |             | 34.5               |
|       | 7     | .26                               |             | 35.0               | .26                               |             | 35.0               | .26                               |             | 35.0               |
|       | 8     | .23                               |             | 33.8               | .21                               |             | 32.2               | .23                               |             | 33.8               |
|       | 9     | .18                               |             | 26.3               | .12                               |             | 24.4               | .18                               |             | 26.3               |
|       | 10    | .17                               |             | 29.0               | .16                               |             | 28.2               | .17                               |             | 29.0               |
|       | 11    | .18                               |             | 29.0               | .16                               |             | 28.2               | .18                               |             | 29.0               |
|       | 12    | .20                               |             | 31.5               | .18                               |             | 29.9               | .20                               |             | 31.5               |
|       | 13    | .22                               |             | 33.0               | .22                               |             | 33.0               | .21                               |             | 32.0               |
|       | 14    | .25                               |             | 35.0               | .26                               |             | 35.0               | .25                               |             | 35.2               |
|       | 15    | .27                               |             | 36.6               | .28                               |             | 37.3               | .27                               |             | 36.6               |
|       | 16    | .26                               |             | 35.0               | .24                               |             | 34.5               | .26                               |             | 35.5               |
| 10:18 |       |                                   | 130         |                    |                                   |             |                    |                                   |             |                    |
|       | Avg   |                                   |             | 32.0               |                                   |             | 31.6               |                                   |             | 32.0               |

Static + .19" H<sub>2</sub>OA. INDICATED VELOCITY (TRAVERSE) FT/SEC 31.8

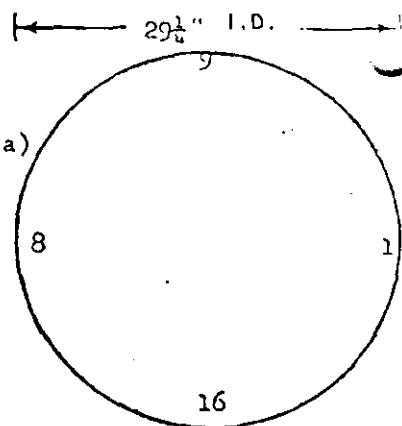
B. INDICATED VELOCITY (REFERENCE PT.) FT/SEC \_\_\_\_\_

C. FLUE FACTOR, A/B 1.00D. PITOT CORRECTION FACTOR 1.00E. GAS DENSITY CORRECTION FACTOR 1.02 (a)F. GAS PRESSURE IN STACK, IN. HG. ABS. 30.15G. GAS PRESS. CORREC. FACTOR,  $\sqrt{29.9/F}$  .996H. CORRECTED VELOCITY, AxDxExG, FT/SEC 32.4

OR BxCxDxExG, FT/SEC \_\_\_\_\_

J. AREA OF FLUE, SQ. FT. 4.67K. AVERAGE FLUE TEMPERATURE, °F 130L. FLOW RATE, HxJx60, CFM 9080M. FLOW RATE,  $(F/29.9) \times 520 \times L / (K+460)$ , SCFM 8100

(a) Assumed value based upon gas composition info. in permit application.



TEST NO. C-1895

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SAMPLING STATION Sulfur Unit No. 1

DATE 1-10-71

WATER VAPOR AND GAS DENSITY CALCULATIONS

PERCENT WATER VAPOR IN GASES

|  | NaOH<br>Train | ZnCO <sub>3</sub><br>Train |
|--|---------------|----------------------------|
| A. GAS PRESSURE AT METER, IN. HG (ABSOLUTE)          | 29.15         | 29.15                      |
| B. VAPOR PRESSURE OF WATER AT IMPINGER TEMP., IN. HG | .469          | .465                       |
| C. GAS VOLUME METERED, SCF                           | 15.68         | 15.73                      |
| D. WATER VAPOR METERED, C X B/A, SCF                 | .25           | .24                        |
| E. WATER VAPOR CONDENSED, VAPOR VOLUME, SCF          | 2.27          | 1.51                       |
| F. TOTAL WATER VAPOR IN GAS SAMPLE, D + E, SCF       | 2.52          | 2.05                       |
| G. TOTAL GAS VOLUME SAMPLED, C + E, SCF              | 17.95         | 17.63                      |
| H. PER CENT WATER VAPOR IN GAS SAMPLE, 100 X F/G     | 14            | 12                         |

GAS DENSITY CORRECTION FACTOR

| COMPONENT         | VOLUME PER CENT/100 | MOISTURE CORRECTION<br>1 - H/100 | MOL. WT. | WEIGHT<br>PER MOLE OF<br>STACK GAS |
|-------------------|---------------------|----------------------------------|----------|------------------------------------|
| WATER             |                     | 1.0                              | 18.0     |                                    |
| CARBON DIOXIDE    | DRY BASIS           |                                  | 44.0     |                                    |
| CARBON MONOXIDE   | DRY BASIS           |                                  | 28.0     |                                    |
| OXYGEN            | DRY BASIS           |                                  | 32.0     |                                    |
| NITROGEN & INERTS | DRY BASIS           |                                  | 28.2     |                                    |
|                   |                     |                                  |          |                                    |
|                   |                     |                                  |          |                                    |

J. MOLECULAR WEIGHT OF STACK GAS

K. DENSITY OF GAS REFERRED TO AIR =  $J/28.95$

L. GAS DENSITY CORRECTION FACTOR =  $\sqrt{1.00/K}$