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**JANUARY 2020
STORMWATER INVESTIGATION REPORT
RESPONSE TO COMMENTS
COAKLEY LANDFILL
North Hampton and Greenland
New Hampshire**

**NHDES Site #: 198712001
Project Type: Superfund Site**

Prepared For:
New Hampshire Department of Environmental
Services
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Date of Memo: (January 2020)

January 22, 2020

Richard Hull
US Environmental Protection Agency, Region I
5 Post Office Square, Suite 100
Boston, Massachusetts 02109-3912

**Re: Stormwater Investigation Report – Response to Comments
Coakley Landfill – North Hampton and Greenland, New Hampshire**

Dear Mr. Hull:

On behalf of the Coakley Landfill Group (CLG), CES, Inc. (CES) is hereby submitting the following Response to Comments provided by the United States Environmental Protection Agency (USEPA) in their November 22, 2019 letter to Peter Britz of the CLG. A revised Stormwater Investigation Report (Report) will be submitted following completion of the additional activities outlined in the enclosed scope of work and will incorporate the USEPA's proposed revisions as appropriate.

A summary of responses to comments is provided below:

USEPA

- 1. Water infiltrating within Areas 1 and 2 is collected by the underdrain piping system while water infiltrating in Area 3 enters a gravel-filled toe drain system, but the ultimate discharge location for the toe drain system is not identified.**

CLG Response

The location and ultimate discharge locations for the toe drains will be identified on a revised Figure 1 – Stormwater Investigation Sampling Locations included with Attachment A of this letter and used in future reporting.

USEPA

- 2. The Introduction briefly describes the stormwater sampling that was proactively conducted in spring 2018. The data from that sampling event should be provided in either its own table or included in Table 3 to allow for comparison of results over time.**

CLG Response

The data for the stormwater sampling completed in Spring 2018 were included with Table 3. These samples were collected from three locations (PD-2, OFP-2, and UP-2) and can be identified by their sampling date of 4/26/2018. Future presentation of these data will include notation to identify these as the initial samples collected in the Spring 2018.

USEPA

- 3. Section 2 describes the perimeter drainage ditches and “rip-rap let-down structures” and cites Figure 1, but the figure does not have the let-down structures labeled. Given that the Stormwater Report references several rip-rap structures, it would be useful to specifically label the let-down structures and toe-drains in Figure 1.**

CLG Response

The referenced rip rap-lined letdown structures referenced in Section 2 will be included on a revised Figure 1 – Stormwater Investigation Sampling Locations included with this letter (Attachment A) and in final reporting efforts. For toe drain locations, see response to USEPA Comment No. 1.

USEPA

- 4. First paragraph of Section 2 describes the “stormwater retained in the basins” as subsequently discharging to “adjacent wetland areas through infiltration and via an outlet structure in each basin...”. This description is a bit simplistic compared to the more accurate description provided throughout the rest of the Stormwater Report. Consider expanding the description here to explain the infiltration from the basins to shallow groundwater, and subsequently to adjacent wetland areas.**

CLG Response

The description included in the first paragraph of Section 2 (Background) was designed specifically to provide a more generalized description of the basins and infiltration with the more thorough description provided elsewhere in the report (e.g. Section 3.1). Future reporting will use a more consistent version of the description with an explanation offered to include the infiltration of stormwater within the basins to shallow groundwater and subsequent discharge to surface water.

USEPA

- 5. Section 3.1 describes the landfill cap construction, including the “plastic drainage netting (geonet) with bonded geotextile fabric on top and textured flexible membrane liner (FML) located below the geonet.” Figure 2 describes the geonet as being bonded with geotextile on both sides, and as-built drawing 5-5 also describes the geonet as being bonded on top for the slopes up to 5% and bonded on both sides for side slopes.**

CLG Response

Multiple forms of geonet were used in the construction of the landfill cap based on landfill side slope. For example, Landfill Cap Types 1 and 3 (Drawing 5-5) do not include the use of a geonet, with Type 2 and Type 4 having geotextile bonded to the top and both surfaces of the geonet, respectively. Figure 2 was designed to reference the Cap Type selected for landfill cap sampling with other cap types referenced in Drawing 5-5.

USEPA

- 6. Figure 2 presents a cross-section of the landfill cap based on the Type 4 model but does not provide cross-sections for the other cap types. It would be helpful to include cross-sections for landfill cap Types 1, 2 and 3 as figures, or to reference the cross-sections included in Landfill Cover System Design Report Drawing 5-5 in Appendix A in the text descriptions.**

CLG Response

The CLG concurs that a reference to the cross sections included in the Landfill Cover System Design Report – Drawing 5-5 (Appendix A; Stormwater Investigation Report) would be helpful to describe and/or reference the other landfill cap types. Future descriptions of the various landfill cap types will be accompanied by either a representative detail cross section or appropriate design drawing references as were included with Drawing 5-5 in Appendix A of the Stormwater Investigation Report as submitted on September 24, 2019.

USEPA

- 7. In the description of the sources of the cover soil provided in Section 3.1.1, the term “topsoil” is used to describe the cover soil in that section.**

CLG Response

The term cover soil should have been used in the description of the cover soil source material instead of topsoil and will be corrected in subsequent reporting efforts described above.

USEPA

- 8. Section 3.2, second paragraph should clarify that piezometers PZ-1 and PZ-2 were constructed of stainless steel and that PZ-3 was constructed of PVC.**

CLG Response

The CLG concurs that the second paragraph of Section 3.2 could clarify the variations in construction materials used in piezometer construction; however, we feel the description provided in the first paragraph of Section 3.2 and the provided piezometer construction diagrams are sufficient to establish the locations of PZ-1 and PZ-2 with regards to the construction materials outlined in the second paragraph. Future stormwater reporting efforts will include more detailed descriptions of piezometer construction.

USEPA

9. Section 3.3 and Table 1 describe the surface and groundwater elevation and provide the data from fall 2018 and spring 2019 monitoring. Table 1 is confusing as both surface water and groundwater elevations are provided in the columns labeled as “GW. EL. FT.” A map should be provided that includes all locations used for water elevation measurements (see Table 1). Not all the monitoring wells listed in Section 3.3 are shown on Figure 1; nor are all the surface water locations listed in Table 1.

CLG Response

The CLG concurs that the column headers are confusing with respect to the static water levels being represented. A revised Table 1 has been provided with this response to comments letter (Attachment A) to clarify any misunderstanding related to the column headers. Any future figures generated in support of stormwater characterization or reporting activities will include all locations referenced or reported. This includes revising the scale of figures to encompass areas where these features are located.

USEPA

10. Section 3.4.1 does not identify or describe the analytical methods used for the analysis of the various cap components. It is presumed that the varying sample types (soil, pipe, membrane) would require different analytical testing procedures. The laboratory methods and procedures should be described. Section 3.4.1 should also describe the methods for sampling the cap materials (hand auger, test pit, shovel, etc.) and the depths of the various samples and how those depths compared to the design drawings. The last paragraph of Section 3.4.1 states that the soil matrix samples were a 4-point composite, but only a single sampling location is shown on Figure 1, and that a 2-point composite was used for sampling the construction materials. The Stormwater Report should describe the sample collection methods and analytical preparation procedures for the cap soils and materials, and detail the analytical methods used.

CLG Response

Analytical methods used in the analysis of stormwater investigation samples were included on corresponding tables. See response to comment 11, below. Relative to the laboratory methods and procedures used in the analysis of the cap components, based on correspondence with the contracted laboratories, that although different methods are often used in the analysis of materials, the primary difference is in sample preparation/extraction and not in the analytical method used. These preparation and extraction methods are typically a proprietary technique specific to the laboratory and only general information is provided by the lab specific to their analysis process. As per a response from Vista Analytical Laboratories (Vista), HDPE underdrain piping was “...sonicated in methanol - the methanol was then analyzed to determine the levels of the leached analytes.” This was completed in accordance with Vista SOP 49, rev. 22.

Cap construction materials were sampled using a stainless-steel bucket auger with notes made on materials encountered relative to those referenced on cap construction details provided in Drawing 5-5 of the Landfill Cover Design Report (Appendix A; Stormwater Investigation Report). It was observed that materials encountered matched in both composition and depth/thickness as provided in the Landfill Cover Design Report. In support of the text provided in the last paragraph of Section 3.4.1 describing the 2-point and 4-point composite techniques used, corresponding composite sample IDs were provided on Figure 1 in parentheses and accompanying explanation in the notes included with Figure 1.

USEPA

- 11. Section 3.5 does not list the analytical methods used for the various samples, or even the laboratory used. Again, the Stormwater Report should specify the analytical methods used for all samples.**

CLG Response

Eastern Analytical was used for the analysis of 1,4-dioxane and general landfill chemistry parameters, with PFAS analysis completed by Vista Analytical under subcontract to Eastern Analytical. The analytical methods used for the various samples are specified in Tables 2, 3 and 4. Analyses were completed as per USEPA Method 537 in accordance with Vista SOP 49, rev. 22. For additional information related to the analysis of cap components, please refer to the response of Comment No. 10, above.

USEPA

- 12. Table 2 indicates that bold text denotes concentrations above reporting limits (Note 10), but the results in Table 2 that appear to be above the reporting limits and are not flagged, do not appear in bold text.**

CLG Response

The CLG concurs that those values above the reporting limits should be in bold. A revised Table 2 has been included with Attachment A of this letter and will be included as part of future stormwater reporting.

USEPA

- 13. Section 4.1 discusses results for PFOA and PFOS but does not mention the distribution and types of the other PFAS compounds analyzed and detected.**

CLG Response

The discussion of PFAS compounds was specific to address those that were regulated in groundwater at the time of report submittal. Additional PFAS compounds detected within cap materials, if detected in groundwater, were not regulated and not included in the discussion of results. Future reporting and discussions of PFAS compounds in soil materials will include those regulated and will, at a minimum, include a list of detections.

USEPA

14. Section 4.2.1 details the results from location L-1 as part of the stormwater investigation, but these results are not included in Table 3. While Table 4 presents the historical results for L-1, the results from samples collected as part of the stormwater investigation should also be provided in Table 3 for comparison with the results from the other locations sampled as part of the investigation.

CLG Response

The CLG concurs that historical data for L-1 could be provided in Table 3 for comparison and will include this in future presentation of stormwater analytical data as referenced above.

USEPA

15. Section 5.1 concludes that “some infiltration of shallow groundwater may be entering the annular space between the corrugated steel piping of the outfall system and surrounding bedding material during periods when shallow groundwater levels are high.” Shallow groundwater levels would be high during wet periods when surface water may be present in the stormwater basin. Another conclusion could be that during high groundwater level conditions, stormwater discharging from the basin is leaking down around the overflow pipe and flowing through the bedding material and out into the L-1 area. The head driver for that pathway would be substantially higher than for shallow groundwater.

CLG Response

The CLG concurs that the hydraulic head conditions present during wet conditions/increased shallow groundwater elevations could result in stormwater discharge via bypassing the overflow pipe and be transported through the overflow pipe bedding material.

USEPA

16. Section 5.2 describes an “average annual precipitation” of 59.55 inches, based on NOAA precipitation data for 2018. The amount of water falling on the landfill in 2018 (39 million gallons) is described as calculated using the average annual precipitation value and the landfill area. If 59.55 inches of rainfall for 2018 is used in this calculation, wouldn't it be more accurately described as total rainfall for 2018 rather than average annual precipitation? And that the total amount of water falling on the landfill would be specifically for 2018 rather than an annual average?

CLG Response

The CLG concurs that the amount of rainfall used in the calculation could be more accurately described as total rainfall for 2018 rather than average annual precipitation. The use of terminology (precipitation) was coincident to that referenced by source data used during modeling. Though the term precipitation accounts for all forms of recordable precipitation, including rainfall, clarification of the term precipitation and how the volume of water was calculated will be provided in future reporting.

USEPA

17. If the average annual precipitation (46 inches) was used in the mass loading calculations rather than the 2018 precipitation (59 inches) as described in Section 5.2, then the model calculations for the average rainfall amount should be described in similar detail and the amounts for surface runoff, infiltration and evapotranspiration should be provided.

CLG Response

The CLG agrees that future assessment of contaminant loading should incorporate a long-term “average” precipitation value and resultant components (surface runoff, infiltration, evapotranspiration) should be based on an average precipitation value. Any future model calculations using an “average” rainfall amount will be described in similar detail with the amounts used for surface runoff, infiltration, and evapotranspiration provided.

USEPA

18. Section 5.2.2 - The area of impacted groundwater discharge to Berry’s Brook (estimated at 40 acres) should be clearly demarcated and labeled on Figure 3. A legend should be added to indicate the meaning of the various line types (3) used on that figure. In addition, no reference is provided for the watershed boundaries shown in Figure 3 and they do not correspond to the boundaries shown in NH GRANIT, a statewide geographic information system clearinghouse <http://www.granit.unh.edu/>. These maps show a considerably different southern boundary of the Berry’s Brook watershed near the landfill and does not show a Bailey Brook watershed but suggest Bailey Brook is included in Berry’s Brook watershed.

CLG Response

A revised Figure 3 has been generated and has been included with this submission. These revisions include a defined area of impacted groundwater to Berry’s Brook, the addition of a legend to define the various line types used, and notes provided to indicate the source of watershed boundaries illustrated. The southern boundary of the Berry’s Brook watershed illustrated on Figure 3 was based on information obtained from the GRANIT GIS database for Level 6 Hydrologic Boundaries, Figure 1 of the Berry’s Brook Watershed Management Plan, the Berry’s Brook Watershed Wetland Soils and Tax Parcels Map (Rockingham Planning Commission), and high-resolution LiDAR surface topography obtained from GRANIT. According to metadata provided by GRANIT for the Level 6 Boundaries and notes provided in the Wetland Soils and Tax Parcels Map, the watershed boundary layer (shapefile) in GRANIT was generated from topographic information obtained from 1:24,000 scale USGS topographic maps (1969-1984) and from existing Level 11 Sub-watershed Data. The more recent LiDAR data (based on collection of data from 2010-2014) includes topography for the southern portion of the landfill following the regrading and capping of the landfill in the late 1990’s and is not believed to have been included with the original watershed delineation efforts completed during generation and digitization of the GRANIT shapefile. The interpreted Bailey Brook Watershed boundary is

interpreted from surface topography obtained from LiDAR data as contoured and illustrated on Figure 3. Notation has been added to Figure 3 to include this information.

USEPA

- 19. Section 5.2.2 – Why wasn't data from more wells (AE-3A, PZ-3) and L1 seep used in the representation of groundwater quality? How was the 40-acre groundwater discharge area defined, and why wasn't it defined using monitoring wells and groundwater contours?**

CLG Response

The primary purpose of the Stormwater Investigation was to evaluate potential PFAS loading to surface water (wetland complex and Berry's Brook) due to runoff from the landfill cover system. The HELP model is well-suited to estimate runoff volumes from the landfill cover surface and that analysis provide relatively detailed information with respect to stormwater runoff. Performing a detailed analysis of contaminant mass loading from groundwater to surface water was not specifically included in the investigation scope of work. However, it was determined that a rough estimate of contaminant loading from groundwater could provide a basis for a comparison to stormwater contaminant loading to determine if the stormwater PFAS loading was a "significant" contribution to contaminants in surface water compared to groundwater discharge.

The PFAS concentrations used in the groundwater loading estimate were based on isoconcentration contour maps provided in previous Annual Monitoring Reports and review of PFAS concentrations in shallow overburden wells that were judged to be representative of groundwater that would most likely be discharging to surface water at this point in time (i.e., for comparison to the 2018 HELP model results). The area of groundwater discharge was estimated to include much of the wetland area west of the landfill and extending north to Breakfast Hill Road. That area was determined to be approximately 40 acres in size. Because a surface water sampling location (SW-110) is present where Berry's Brook crosses Breakfast Hill Road, groundwater discharges north of Berry's Brook were not included.

We agree that more refined estimates of groundwater could be made, but based on the more generalized mass loading estimates, it is clear that stormwater runoff provides a significant PFAS loading to surface water. The purpose of this part of the evaluation was to verify this hypothesis, and the analysis performed was sufficient to do so. Following the completion of efforts outlined in the scope of work provided below, an evaluation of mass loading estimates will be performed, and comparisons made to initial estimates provided in the Stormwater Investigation Report. These efforts include the evaluation of additional sources of analytical data within a more refined discharge area.

USEPA

- 20. Section 5.2.2 should more specifically describe the data set used to calculate the average concentration of PFAS.**

CLG Response

See response to comment 19.

USEPA

21. Section 5.2.2 does not adequately explain how the PFAS mass discharge via groundwater from the landfill was calculated. It is not clear how the average value for recharge from precipitation (22.3”) can be applied to a ‘groundwater discharge area’ in a wetland to estimate PFAS mass flux in groundwater from the landfill by applying an average PFAS concentration from monitoring wells.

A more traditional method would be to calculate the PFAS mass flux in groundwater at a series of transects perpendicular to the groundwater flow across the mapped plume. The groundwater flux is calculated via Darcy’s Law and analytical results from monitoring wells located along the transect(s) are used for the PFAS concentration. This provides a reliable estimate of the PFAS mass leaving the landfill via the groundwater pathway.

CLG Response

The PFAS loading was a simplified assessment that assumed a steady state hydraulic condition where groundwater recharge is balanced by groundwater discharge. Given that no large scale groundwater withdrawals are known to be present within the immediate Berry’s Brook watershed area discussed in the Stormwater Investigation Report, the approach assumed uniform recharge and used a pro-rated discharge area where groundwater impacts are known to occur as the basis for estimating a mass loading estimate.

We agree that more sophisticated methods could have been used to estimate mass flux of PFAS from groundwater to surface water. However, as noted in the response to Comment No. 19, the purpose was only to assess the overall significance of stormwater loading compared to groundwater loading.

Should any future remedial investigation work on this issue include assessment of shallow groundwater, a more rigorous assessment of PFAS loading will be warranted. However, the collection of additional data as outlined in the provided Scope of Work will provide for a more complete understanding of the interaction between shallow groundwater and surface water and allow for more accurate estimates of mass flux within the system. For additional efforts related to loading estimates, please see response to Comment No. 19, above.

USEPA

22. Section 5.2.3 does not adequately explain how the PFAS mass discharge into Berry’s Brook was calculated. It is unclear how an average surface water PFAS concentration based on limited sample results from a single location can be applied to groundwater recharge over the entire watershed to estimate the mass. Further, the resulting recharge mass is then assumed to equate to the mass in Berry’s Brook.

A more traditional method would be to calculate the PFAS mass flux in Berry's Brook using measured PFAS concentrations in the brook at the Breakfast Hill Road crossing and stream discharge rates from the USGS gauging station. The gauging station data can be adjusted to reflect the drainage area upstream from Breakfast Hill Road by applying the ratio method. This method is straightforward and accurate.

This will facilitate a comparison between the three pathways: 1) groundwater PFAS flux in the plume, 2) PFAS mass flux in the stormwater, and 3) PFAS mass flux in the brook. The relative impact of the stormwater on Berry's Brook can then be quantitatively assessed. However, it should be noted that there are other components of the PFAS mass flux that are not considered by this method; refer to Comment 24.

CLG Response

The estimated mass of PFAS leaving the Site via Berry's Brook assumed a baseflow condition. Surface water samples from location SW-110 historically have been collected during normal or low flow conditions rather than during high surface runoff events. As a result, a large component of flow is likely to be considered baseflow of the Brook.

We agree that the surface water sample set is limited, and it is not possible to determine PFAS concentration fluctuations with respect to varying surface water discharge volumes. It is likely that additional PFAS mass is discharged during high runoff events, but significant dilution due to freshwater input within the watershed will also be occurring. Assigning an average value under all discharge conditions that could be applied to an adjusted USGS downstream gauging station would include many assumptions that would be difficult to justify based on the limited data set. More refined mass discharge via Berry's Brook can be calculated as additional data is obtained. Following the collection of additional information related to shallow groundwater water and stormwater contribution to surface water as outlined in the Scope of Work provided below, a more complete data set will be available to facilitate comparisons between multiple pathways referenced above.

USEPA

- 23. In Section 5.2.3, what is meant by "above Breakfast Hill Road"? The description of the watershed area seems to identify the area north of Breakfast Hill Road and SW-110, but it appears that the calculation is for the area providing water volume that is discharged across Breakfast Hill Road?**

CLG Response

The reference to "above Breakfast Hill Road" refers to the watershed area(s) south (upstream) of Breakfast Hill Road.

USEPA

24. The analysis in Section 5.2.3 assumes that all groundwater impacted by the landfill discharges to Berry's Brook upstream of Breakfast Hill Road. This assumption is not accurate. Some overburden and bedrock groundwater containing PFAS migrates under Breakfast Hill Road and continues to flow downgradient. The analysis also ignores any migration of PFAS into the underlying bedrock, which we know takes place due to the detections noted in that unit. The PFAS mass flux for those pathways should be estimated to assess whether they are significant enough to be considered in the evaluation.

CLG Response

The CLG concurs and this is consistent with the general conceptual site model for the Site. However, concentrations of PFAS detected at MW-20, residential well R-3 and the Breakfast Hill Golf Club drinking water supply well, are orders of magnitude lower than concentrations observed in monitoring wells near the landfill and wetland complex. This demonstrates a significant mass of PFAS is not migrating north of Breakfast Hill Road. It should also be noted that the golf club irrigation water contained higher concentrations of PFAS, when sampled by others in 2017 (24 ng/L PFOA), than those detected in the northernmost overburden well within the Coakley GMZ (<1 ng/L at MW-20S). These concentrations in the golf club irrigation well may affect groundwater and surface water concentrations of PFAS north of Breakfast Hill Road. PFAS detected in golf course irrigation water is believed to be unrelated to the Coakley Landfill as the irrigation well is constructed within overburden, is located side gradient of the golf club drinking water supply well, and is located across a watershed divide (located in Winnicut River Watershed) from the area located downstream from the Coakley Landfill and north of Breakfast Hill Road (located in Berry's Brook Watershed). In addition, water level monitoring of wells within the Coakley Landfill monitoring network and near the irrigation well completed during a well yield test performed on the irrigation well in 2017 resulted in no evidence of influence in the monitored wells during pumping. Continued monitoring of newly installed overburden and bedrock groundwater monitoring wells will aid in assessing migration of PFAS in the vicinity of Breakfast Hill Road.

USEPA

25. A sensitivity analysis should be conducted for all calculations detailed in Sections 5.2.1, 5.2.2, and 5.2.3 by modifying the inputs and assumptions (volume of discharge, average concentration, discharge area, etc.) to allow for an evaluation of the inputs relative to outputs; which will allow the accuracy of the various components of the assessment to be estimated.

CLG Response

The CLG concurs that a sensitivity analysis could provide additional accuracy of the various components and inputs used for calculations described in Sections 5.2.1 through 5.2.3. However, the scope of work that has been developed to further investigate the extent of contaminant loading to Berry's Brook will allow for more accurate information (inputs) to be used in additional calculations and modelling. The scope of work will be developed to include the collection and evaluation of data in the context of contaminant loading from the cap (stormwater contribution)

relative to that of shallow groundwater and to evaluate the interaction of surface water and shallow groundwater in Berry's Brook and the adjacent wetland complex. The information gathered as part of this effort will aid in the overall accuracy of these calculations and will be presented further in future reporting.

USEPA

26. One of the findings is that, based on 1,4-dioxane results from PZ-2 in fall 2018 (ND) and a detection in spring 2019, along with iron results from OFP-1, PZ-1, PZ-2 and PZ-3, shallow groundwater beyond the landfill boundary interacts with discharges from the northwest outfall pipe (OFP-2) during periods of high overburden groundwater levels. How are the iron results from OFP-1 and PZ-1 in the northeast basin related to the interaction between groundwater and the discharge from OFP-2? And how does the detection of 1,4-dioxane in PZ-2 relate to the discharge from OFP-2 when it is measuring shallow groundwater just beneath the basin?

CLG Response

Based on the iron results at OFP-1 (3 mg/L) and PZ-1 (4.6 mg/L), there is likely an interaction between shallow groundwater and stormwater within the northeast basin (SB-1) similar to that believed to be occurring in the northwest basin (SB-2). This is supported by low levels (<1 mg/L) of iron in perimeter ditch and underdrain pipe samples (no supposed direct interaction with shallow groundwater) and concentrations similar to those observed from the same structure locations (i.e. UP) in the northwest corner of the landfill. It is reasonable to assume that shallow groundwater can migrate through the bedding material of the OFP structure at times when overburden groundwater reaches seasonal high levels. As iron was only analyzed for during the Spring 2019 sampling event, additional information on seasonal iron concentrations may be needed to generate a more comprehensive model for stormwater and shallow groundwater interaction. However, despite iron being an important indicator to landfill influence, it is a parameter that can be influenced by several environmental factors. As such, iron concentrations will be used with other general groundwater chemistry parameters to assist with evaluating the interaction between stormwater and shallow groundwater.

With regard to the detection of 1,4-dioxane in PZ-2 (5.7 ug/L) and OFP-2 (<0.2 ug/L) during Spring 2019, the relationship between shallow groundwater (as monitored by PZ-2) and discharge from OFP-2 may be a function of seasonal variations in water levels and/or changes in the amount of contact time the shallow groundwater has with refuse before migrating downgradient. As with the reported iron concentrations, additional information on seasonal 1,4-dioxane concentrations and hydraulics may be needed to generate a more comprehensive model for stormwater and shallow groundwater interaction.

USEPA

27. Conclusions state that “stormwater and groundwater contribute significant percentages of PFAS to the wetland complex” while the annual contributions of PFAS from stormwater and groundwater discharge to surface water is described

as exceeding the mass estimate of PFAS calculated in Berry's Brook by a factor of 2.5. The conclusions should more clearly represent this calculated relationship and summarize the potential causes of this discrepancy.

CLG Response

The CLG concurs that the conclusions stated in the report should more clearly represent the calculated relationship between stormwater and groundwater contributions of PFAS to the wetland complex. Future reporting will include revised conclusions relative to the discussion of the relationships and contribution of PFAS to the wetland complex by stormwater and shallow groundwater.

USEPA

- 28. The Stormwater Report makes no mention of the underdrain system cleanouts. Were these inspected? Are these routinely checked? Is there any reason to believe that the system may not be functioning as designed due to the discharge piping being fouled?**

CLG Response

The underdrain cleanouts were visually inspected during the verification of the stormwater system components; however, these are not routinely inspected. Due to the photographic documentation of discharge of the underdrain piping during and immediately following precipitation events, there is no reason to suspect that the discharge piping has been fouled. In addition, water clarity (no visual evidence of soil particulates or iron fouling/staining) does not indicate the presence of material that would be characteristic of a blockage or fouling within the pipes.

USEPA

- 29. The PFAS compositional plots included in Appendix D are not referenced or discussed anywhere in the document. They are only mentioned briefly in Section 6.1. A discussion of how the plots were prepared and what they represent should be included.**

CLG Response

The CLG concurs that additional reference to compositional plots included as Appendix D of the Stormwater Investigation Report should be made and will include this with future reporting efforts proposed. The plots were prepared for select locations using six PFAS compounds analyzed for during the Fall 2018 stormwater sampling event. The compositional plots were generated to visually illustrate a "signature" for PFAS composition within stormwater. This signature can be visually correlated to the composition of PFAS within shallow groundwater (e.g. MW-9) to illustrate the impact of stormwater to shallow groundwater in areas immediately adjacent to stormwater discharge locations.

SENSIBLE SOLUTIONS



**SURFACE WATER EVALUATION
SCOPE OF WORK
COAKLEY LANDFILL SUPERFUND SITE
NORTH HAMPTON
AND GREENLAND, NEW HAMPSHIRE**

FOR

COAKLEY LANDFILL GROUP

**1 Junkins Avenue
Portsmouth, New Hampshire**

**January 2020
JN: 10424.020**



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FIGURES

Figure 1	Stormwater Sampling and Gauging Locations
Figure 2	Proposed Piezometer Locations
Figure 3	Proposed Porewater Sampling Locations

ATTACHMENTS

Attachment A	Select Revised Stormwater Investigation Report Tables, and Figures
Attachment B	Standard Operating Procedure No. 16 (SOP-16): <i>Groundwater/Surface Water Interface Sampling Using A Pore Water Sampler</i>

SURFACE WATER EVALUATION SCOPE OF WORK COAKLEY LANDFILL SUPERFUND SITE NORTH HAMPTON AND GREENLAND, NEW HAMPSHIRE

1.0 | INTRODUCTION

On behalf the Coakley Landfill Group (CLG), CES, Inc. (CES) has prepared the following Surface Water Evaluation Scope of Work (SOW) to provide an approach and protocols for the collection and analysis of additional information relative to migration of contaminants from stormwater and shallow groundwater to Berry's Brook. The intent of this investigation is to better understand contaminant distribution and migration as it relates to the interaction between surface water, stormwater discharge from the landfill, and shallow groundwater.

The sampling and investigation activities are being conducted by the CLG, at the request of the United States Environmental Protection Agency (USEPA) and New Hampshire Department of Environmental Services (NHDES) as outlined in a letter from the USEPA to the CLG dated November 22, 2019. This letter contained comments generated from a review of stormwater investigation activities presented in the *Stormwater Investigation Report* submitted to the Agencies on September 24, 2019. The SOW will include an assessment of options for limiting the contaminant loading to Berry's Brook and for the evaluation of collection and treatment options through pilot or treatability studies. These assessment actions will serve to address requirements included in New Hampshire House Bill 494 (HB494).

2.0 | PROJECT BACKGROUND AND DESCRIPTION

As part of Site remedy design and construction activities implemented in the mid and late 1990s and evaluated during the Stormwater Investigation completed in the Fall of 2019, the majority of stormwater runoff from the landfill surface is conveyed to two unlined stormwater retention basins. These basins are located in the northeast and northwest corners of the landfill and are designated as SB-1 and SB-2, respectively. The stormwater runoff (sheet flow) enters each basin via a series of perimeter drainage ditches and rip-rap let-down structures on the landfill (**Figure 1**). Stormwater retained in the basins is subsequently discharged to adjacent wetland areas via an outlet structure in each basin and associated corrugated metal piping or to shallow groundwater via infiltration.

In addition to surface stormwater runoff, precipitation that infiltrates through the landfill's vegetative layer and cover soil is collected in a drainage layer and geonet filtration layer placed immediately above the flexible membrane liner (FML) of the cap system. Water along the east side of the landfill is conveyed via underground perforated piping of the underdrain system to the northeast stormwater retention basin (SB-1), while water along the west side of the landfill is conveyed via similar underdrain piping to a rip rap lined discharge swale located west of SB-2 (**Figure 1**).

As detailed in the September 24, 2019 Stormwater Investigation Report, a significant contribution of per- and polyfluoroalkyl substances (PFAS) to the adjacent wetland complex and shallow groundwater is from stormwater runoff and stormwater discharge from the landfill cover system. These components of contaminant input to surface water and shallow groundwater resulted in a request by the USEPA to further investigate the interaction between stormwater, groundwater and contaminant concentrations detected in Berry's Brook.

Concurrent with the completion of activities described in the Stormwater Investigation Report, the passage of HB494 in August of 2019 resulted in a requirement that the CLG work with the NHDES and USEPA to "...propose, under the applicable consent decree involving the Coakley Landfill superfund site, an appropriate remedy including a design solution and associated costs to ensure the substantial reduction of the contaminants entering Berry's Brook from the Coakley Landfill superfund site."

The CLG, NHDES, and USEPA have jointly worked to identify activities and remedies that can be implemented to address both the comments of the USEPA in its November 22, 2019 letter and the requirements of HB 494. This SOW provides details of activities to be completed that will assist in assessing options to reduce contaminant concentrations in Berry's Brook.

2.1 Study Objectives

The overall objective of this evaluation will be to further assess the extent of contaminant distribution and migration to Berry's Brook and shallow groundwater from stormwater discharge at the Coakley Landfill. This evaluation will allow for a better understanding of the interaction between stormwater, surface water discharging to the wetland complex, and groundwater that ultimately discharges to Berry's Brook. Results of the evaluation will also be used to assess potential mitigation measures to reduce contaminant concentrations in Berry's Brook.

3.0 | SAMPLING AND INVESTIGATION ACTIVITIES

The SOW is comprised of several efforts or phases and is designed to provide the information necessary to make informed decisions on subsequent investigation activities.

3.1 Piezometer Installation

A total of three piezometers (PZ-1, PZ-2, and PZ-3) were installed as part of the Stormwater Investigation completed in September 2019. PZ-1 was installed in the northeast stormwater retention basin (SB-1) and PZ-2 was installed in the northwest basin (SB-2) to monitor localized subsurface soil saturation conditions resulting from direct infiltration of stormwater through the bottom of the unlined basins. PZ-3 was installed in the vicinity of the L-1 seep sampling point to establish a discrete sampling location representative of shallow groundwater discharging to the wetlands in the area downgradient from the outfall discharge from stormwater retention basin SB-2. To supplement these existing monitoring locations, the installation of eight additional piezometers is proposed to further evaluate the relationships between surface water and shallow groundwater north and west of the landfill.

Piezometers will be installed at several existing surface water sampling locations (BB-2, SW-4, SW-103, and SW-110) and in areas where surface water is not currently being monitored as illustrated on **Figure 2**. These include areas immediately north of the landfill boundary and in an area west of the railroad easement between BB-1 and BB-2. As a result of a prolonged period of below average precipitation prior to the Fall 2019 Semiannual Sampling event, several surface water locations did not contain sufficient water (SW-4, SW-5, BB-1, and BB-2) to obtain a representative sample. SW-4 and BB-2, though dry during the Fall 2019 sampling event, represent locations where surface water is typically present and have been identified as locations that will be targeted in the monitoring of surface water as part of this evaluation. Locations SW-5 and BB-1 may not be representative of the natural surface water drainage network, but rather, more characteristic of localized ponded water areas isolated from the more direct surface water drainage network. Analytical results from these locations may not be typical of natural surface water where there is an established gradient allowing for the influx and passage of water through the system; however, availability of historical information from the location of SW-5 within the area of investigation makes it a suitable location for piezometer installation. A piezometer is not planned for installation at BB-1. However, a piezometer will be installed at an alternate location west of the railroad easement. Data from a piezometer in this location will be used in conjunction with data from several existing monitoring locations within the wetland complex west of the tracks and with data obtained from proposed porewater sampling efforts discussed below.

The installation of piezometers at BB-2, SW-4, SW-5, SW-103, SW-110, and SW-111 will allow for the monitoring of shallow groundwater at locations where historical data on surface water is available and allow for the monitoring of both surface water and shallow groundwater elevations at a single location. In addition, the installation of piezometers at locations immediately north of the landfill and in areas adjacent to existing wetlands (**Figure 1**) will provide a more comprehensive network of monitoring to develop a better understanding of interaction between shallow groundwater and surface water at areas of interest.

Monitoring of water levels within these piezometers will be performed on a monthly basis and will be combined with the gauging of overburden groundwater monitoring wells as identified on **Figure 2**. These wells include MW-9, MW-10, FPC-5A, FPC-6A, AE-3A, FPC-7A, FPC-9A, OP-2, and OP-5.

Piezometers will be constructed using either 1.25-inch diameter stainless steel drive point well screens or 1-inch diameter Schedule 40 PVC well screen and riser. Piezometer construction will be based on field conditions at the time of installation. Following installation, piezometers will be surveyed relative to existing surveyed locations that include survey pins, staff gauges, or monitoring wells surveyed during the Stormwater Investigation. This will allow for water level comparisons to existing surveyed monitoring wells in the vicinity of the piezometers.

3.2 Stormwater and Shallow Groundwater Sampling

To minimize duplication of sampling, surface water sampling locations that are part of the routine semiannual sampling program will continue to be sampled during regularly scheduled semiannual events separate from stormwater and shallow groundwater (piezometer) sampling outlined below. However, efforts will be made to schedule stormwater and shallow groundwater sampling in conjunction with routine sampling events to allow for more direct correlation of analytical results.

3.2.1 Stormwater Sampling Locations

Based on results of stormwater sampling completed during the stormwater investigation, select locations have been identified for continued sampling to establish a more extensive database of results. Due to similarities in PFAS composition and concentrations between samples from the northeast and northwest retention basins, locations proposed for continued sampling will be primarily from the northwest basin (SB-2) due to the proximity to the primary area of investigation (i.e., wetland complex and Berry's Brook). Shallow groundwater within PZ-1 and surface water within SB-1 (located in the northeast retention basin) will continue to be sampled due to the contribution of stormwater to the wetland area located immediately north of SB-1. Analytical data from these locations will be correlated with past results and data from shallow groundwater samples.

Sample designations (STM) will be consistent with those used for stormwater samples during the stormwater investigation. Samples related to the Northeast Stormwater Basin will have the designation of 1 while samples related to the Northwest Stormwater Basin will have the designation of 2. Stormwater samples will be collected from a total of six locations as illustrated in **Figure 1** and include:

- ◆ Landfill Seep (L-1)
- ◆ Northeast Stormwater Retention Basin (STM-SB-1)
- ◆ Northwest Stormwater Retention Basin (STM-SB-2)
- ◆ Northwest Outfall Pipe (STM-OFP-2)
- ◆ Northwest Perimeter Ditch (STM-PD-2)
- ◆ Northwest Underdrain Piping (STM-UP-2)

These locations will continue to be sampled for comparison with past and future analytical results. This analytical information will aid in the continued assessment of water quality of the landfill seep at L-1. Samples from L-1 will be collected during conditions where there is minimal or no discharge from the adjacent SB-2 outfall pipe (STM-OFP-2) or when the seep at L-1 is not visibly influenced by other stormwater discharge. These conditions ensure that the samples at L-1 are isolated and representative of the discharge of shallow groundwater to surface water.

The potential exists for some locations (e.g. STM-OFP-2) to be dry during sampling events, based on the absence or presence of water within the stormwater basin; however, these conditions will be noted and reported accordingly.

Surface water locations, as stated above, will continue to be collected during regularly scheduled groundwater monitoring events. Surface water locations SW-5 and SW-103 are locations in closest proximity to the stormwater control system locations in the northwest portion of the landfill and are approximately 75-ft and 300-ft north of L-1, respectively.

3.2.2 Groundwater Sampling

Shallow groundwater samples will be collected from proposed piezometer locations as identified in **Section 3.1** and will also include piezometers previously installed as part of the stormwater investigation. These samples are designed to be representative of groundwater water that is in direct communication with surface water. Results can be compared to co-located surface water sample results to more directly compare surface water results with shallow groundwater analytical results. These locations include PZ-1, PZ-2, PZ-3, PZ-4, PZ-5, PZ-6, PZ-7, PZ-8, PZ-9, PZ-103, and PZ-110.

In addition to groundwater samples collected from piezometers, overburden groundwater samples obtained from monitoring wells sampled during regular biannual sampling events will be used during data evaluation.

3.2.3 Porewater Sampling

In an effort to obtain samples representative of the interaction between shallow groundwater and surface water (Berry's Brook), porewater samples will be completed at up to 9 locations as illustrated on **Figure 3**. These locations have been identified based on the expected groundwater discharge to surface water as determined by surface water elevations and overburden groundwater potentiometric surfaces recorded during semiannual sampling events. These locations are designed to provide information between locations monitored by piezometers (existing and proposed). Porewater sample locations were selected to reduce the number of locations where permanent installations were needed that would require landowner approval. Samples will be collected using a push point sampler with water withdrawn using a syringe or peristaltic pump in accordance with Standard Operating Procedure #16 (SOP-16): *Groundwater/Surface Water Interface Sampling Using A Pore Water Sampler* included as **Attachment B**.

3.2.4 Sampling Schedule

The sampling of locations as outlined in **Section 3.2.1** will be completed in conjunction with the semiannual sampling events completed during the Spring and Fall; however, stormwater locations will be sampled based on the presence of a precipitation event sufficient to generate flow at selected stormwater locations. It is anticipated the sampling event will occur in the Spring 2020 with the installation and development of piezometers occurring prior to the sampling event to allow for the monitoring of water levels prior to spring precipitation. The Spring event will be completed during March and April, based on weather conditions, to coincide with the period of seasonal high groundwater flow and recharge as reported in the *Assessment of Ground-Water Resources in the Seacoast Region of New Hampshire* (Mack, 2009). A second sampling event will occur during Summer 2020 at a subset of piezometer and porewater locations based on results

obtained during the Spring sampling event. The Summer sampling will be completed during July to coincide when the effective groundwater recharge in the area could be zero or negative based on precipitation and evapotranspiration rates (Mack, 2009). Additionally, this time period will coincide with base flow conditions within the Brook when there is direct contribution of groundwater to surface water.

3.2.5 Laboratory Analysis

Stormwater, porewater, and shallow groundwater samples (**Figure 1**) will be submitted for analysis of PFAS, 1,4-dioxane, and general landfill parameters (alkalinity, ammonia, nitrate, and iron) as shown on **Table 1**. Analysis of PFAS compounds will include an expanded list of analytes analyzed in previously completed sampling events at the Site. Samples will be submitted to Alpha Analytical of Westborough, Massachusetts (Alpha) following collection and in accordance with sample collection, handling, and chain of custody procedures documented in the project SAP.

3.3 Water Level Measurements

Water level measurements will be recorded from surface water staff gauges, piezometers and select overburden groundwater monitoring wells on a monthly basis to account for seasonal water level fluctuations. Several piezometers will be instrumented with continuously recording water level transducers to assess the rate and duration of influence on shallow groundwater levels following precipitation events and to monitor short term effects of beaver dam removal as discussed in **Section 3.5**. The correlation of this information with historic overburden and bedrock groundwater elevations will allow for a more comprehensive understanding of the interaction between groundwater and surface water.

In addition to providing surface water elevations at previously gauged locations, as detailed in the Stormwater Investigation Report, steel survey pins will be installed and used to monitor surface water elevations in wetland areas east of SW-103, south of GZ-114/GZ-115, east of MW-21S, and east of FPC-6A/6B. These steel pins will allow monitoring of surface water elevations in areas where shallow overburden groundwater is monitored and/or sampled as part of routine groundwater monitoring events. Surface water elevations will also be measured at piezometers installed at current surface water sampling locations (e.g. SW-4, SW-5, etc.) and referenced from the measuring point of the piezometer (top of riser).

3.4 Stage Discharge Rating Curve

The relationship between the depth of water within Berry's Brook and Brook discharge rate will be established through the development of a rating curve. Water depths are recorded during periods of base flow (dry conditions when groundwater is a primary source of water to the stream), periods of peak flow (immediately following precipitation events), and during seasonal periods (spring recharge periods) in conjunction with Brook flow rates measured with stream flow meters and channel configuration.

Stage discharge measurements will be completed using the velocity area method pursuant to USGS protocols. A minimum of 6-8 measurements will be recorded at a range of flow rates to adequately evaluate changes in flow during the monitoring period. It is proposed that these measurements be recorded during a minimum of three separate events at up to three locations along Berry's Brook located between the headwaters south of Breakfast Hill Road and SW-111. The coordination of these events will coincide with the measurement of water levels detailed in Section 3.3.

3.5 Beaver Dam Removal

The presence of two beaver dams within the survey area (**Figure 3**) has created localized ponded areas north and west of the landfill. These areas had previously been monitored and/or controlled by the railroad due to the flooding conditions that resulted on the railroad bed and subsequent rail trail due to beaver dams. The ponding caused by beaver dams may affect the fate and transport of contaminants in the wetland complex serving as the headwaters to Berry's Brook due to an altered distribution of contaminants being discharge via both groundwater and stormwater discharges. The removal of these dams will allow for the establishment of more defined surface water drainage conditions within the existing wetland complex and allow for better evaluation of groundwater and surface water interaction. It should be noted that the railroad easement has been purchased from PanAm Railways with plans for conversion to a recreational trail for use by the public. Beaver dam removal will aid in eliminating seasonal flooding observed along the trail. The establishment of more defined surface drainage conditions (hydraulic gradients and flow patterns) will be valuable in the assessment and monitoring of remedial alternatives evaluated/implemented as part of HB494.

3.6 Refined System Modeling

Following the collection and analysis of stormwater, surface water, and shallow groundwater information, additional/refined mass flux calculations will be completed. These efforts will be used to incorporate new information into the current understanding of mass flux within the surface water and shallow groundwater within the wetland complex and Berry's Brook.

3.7 Remedial Alternatives Evaluation

Following the collection and analysis of data in accordance with this SOW, a list of remedial alternatives will be generated, and an initial qualitative assessment performed. This assessment will include identifying remedial alternatives that can be implemented with the goal of "...substantial reduction of the contaminants entering Berry's Brook from the Coakley Landfill superfund site." As part of the assessment process, remedial alternatives suitable for bench-scale evaluation will be identified relative to design concepts and treatment effectiveness. This will enable determination of field-sensitive design parameters prior to scaling a design for a Pilot Study or direct field application. The assessment will include, but not be limited to, the evaluation of available "off the shelf" technologies used for the treatment of surface water and stormwater to identify an approach using new or proprietary technologies.

4.0 | REPORTING

Data transmittals, memoranda, and/or brief task-specific reports will be generated during the investigation as part of consultation with USEPA and NHDES regarding interpretations of data and subsequent modifications to investigation scope of work or schedule. Upon completion of the scope of work, a surface water evaluation report will be prepared for review by the Agencies. The report will include a narrative of activities completed, analytical data collected, interpretation of results, associated tables, figures and appendices, and recommendations for future activities, if any.

5.0 | REFERENCES

CES, Inc. (2017), Quality Assurance Project Plan (Revision 1), Coakley Landfill Superfund Site, North Hampton and Greenland, New Hampshire (September 2017). Prepared by CES, Inc. for The Coakley Landfill Group

CES, Inc. (2018), Sampling and Analysis Plan, Coakley Landfill Superfund Site, North Hampton and Greenland, New Hampshire (July 2018). Prepared by CES, Inc. for The Coakley Landfill Group

Golder Associates, Inc. (1996), Final (100%) Design Report, Coakley Landfill, North Hampton, New Hampshire (May 1996). Prepared by Golder Associates, Inc. for The Coakley Landfill Group

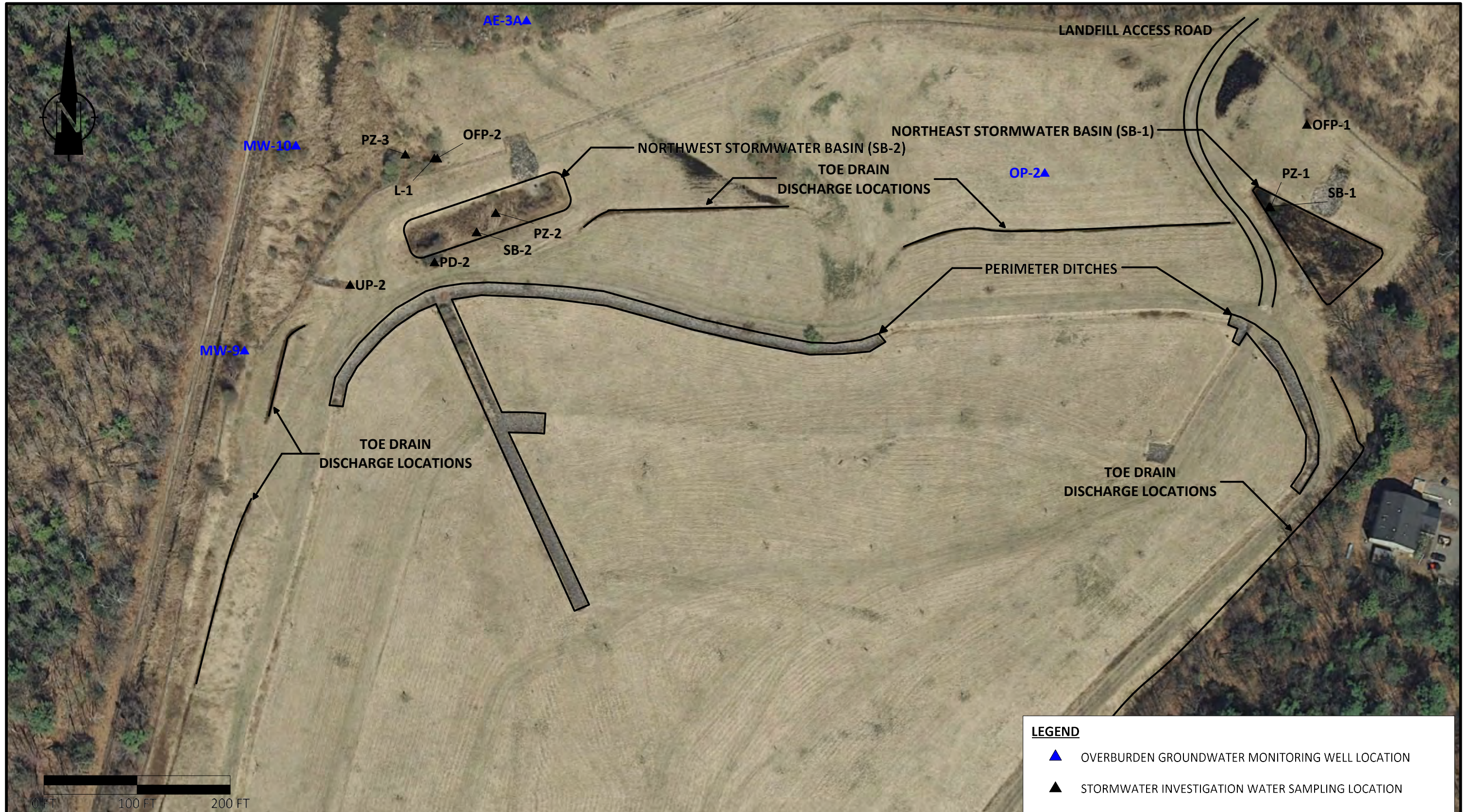
Mack, Thomas J., 2009, *Assessment of Ground-Water Resources in the Seacoast Region of New Hampshire*, United States Geological Survey Scientific Investigations Report 2008-5222

TABLE

TABLE 1
 Summary of Proposed Analytical Parameters
 Coakley Landfill Superfund Site - North Hampton and Greenland, New Hampshire

SAMPLE LOCATION ID	PFAS	1,4 DIOXANE	GENERAL LANDFILL PARAMETERS
STORMWATER			
L-1	X	X	X
SB-1	X	X	X
SB-2	X	X	X
OFP-2	X	X	X
PD-2	X	X	X
UP-2	X	X	X
PIEZOMETER			
PZ-1	X	X	X
PZ-2	X	X	X
PZ-3	X	X	X
PZ-4	X	X	
PZ-5	X	X	X
PZ-6	X	X	X
PZ-7	X	X	
PZ-8	X	X	X
PZ-9	X	X	
PZ-103	X	X	
PZ-110	X	X	X
POREWATER			
PW-1	X	X	X
PW-2	X	X	
PW-3	X	X	X
PW-4	X	X	
PW-5	X	X	
PW-6	X	X	X
PW-7	X	X	X
PW-8	X	X	
PW-9	X	X	X

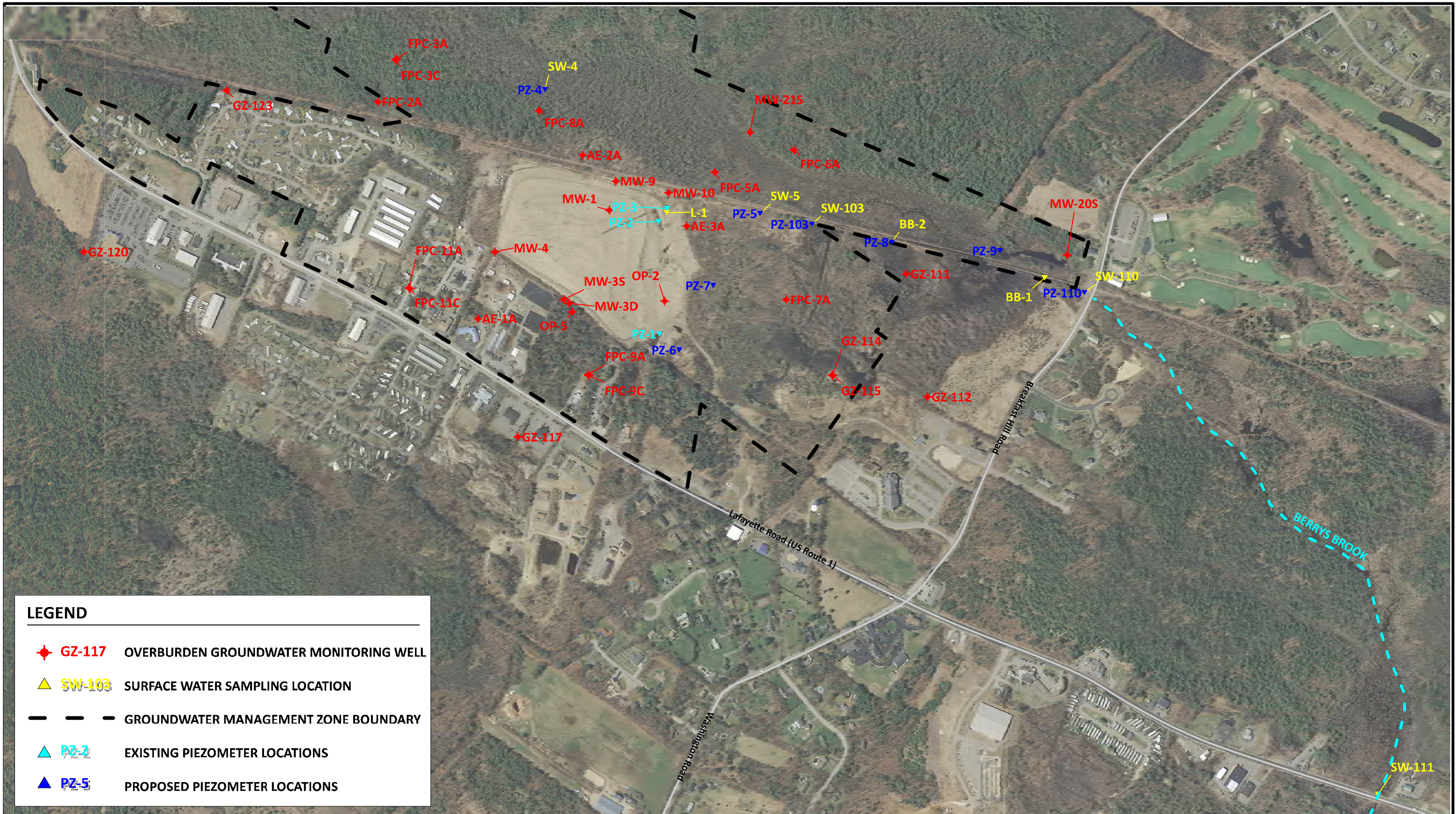
FIGURES



LEGEND

- ▲ OVERBURDEN GROUNDWATER MONITORING WELL LOCATION
- ▲ STORMWATER INVESTIGATION WATER SAMPLING LOCATION

PROJECT TITLE: COAKLEY LANDFILL SUPERFUND SITE NORTH HAMPTON & GREENLAND, NEW HAMPSHIRE	DWG FIGURE 1	BY: CFB DATE: 2020-01-20	REV: REV DATE ISSUE ISSUE DATE	NOTE EXISTING CONDITIONS BASEMAP FROM PLAN TITLED "AS-BUILT SURVEY OF THE COAKLEY LANDFILL, BREAKFAST HILL ROAD, NORTH HAMPTON, N.H." PREPARED BY RICHARD D. BARTLETT & ASSOCIATES, INC. DATED SEPT. 23, 1998. COVER MATERIAL SAMPLE IDENTIFICATION NOMENCLATURE IS BASED ON SAMPLE MATERIAL AND LOCATION. STM-STORMWATER, SO-SOIL, SB-STORMWATER BASIN, UP-UNDERDRAIN PIPE, PD-PERIMETER DITCH, OFF-OUTFALL PIPE, TS-TOPSOIL, CM-CONSTRUCTION MATERIAL, DL-DRAINAGE LAYER, (1)-COMPOSITE SAMPLE NUMBER.
SHEET TITLE: STORMWATER SAMPLING AND GAUGING LOCATIONS	JN: 10424.020 SCALE: AS SHOWN	APPROVED BY: MAD CHECKED BY: CFB		



LEGEND

- ◆ **GZ-117** OVERBURDEN GROUNDWATER MONITORING WELL
- ▲ **SW-103** SURFACE WATER SAMPLING LOCATION
- - -** GROUNDWATER MANAGEMENT ZONE BOUNDARY
- ▲ **PZ-2** EXISTING PIEZOMETER LOCATIONS
- ▲ **PZ-5** PROPOSED PIEZOMETER LOCATIONS

PROJECT TITLE:	COAKLEY LANDFILL SUPERFUND SITE NORTH HAMPTON & GREENLAND, NEW HAMPSHIRE
SHEET TITLE:	PROPOSED PIEZOMETER LOCATIONS

DWG:	FIGURE 2
JN:	10424.020
SCALE:	AS SHOWN

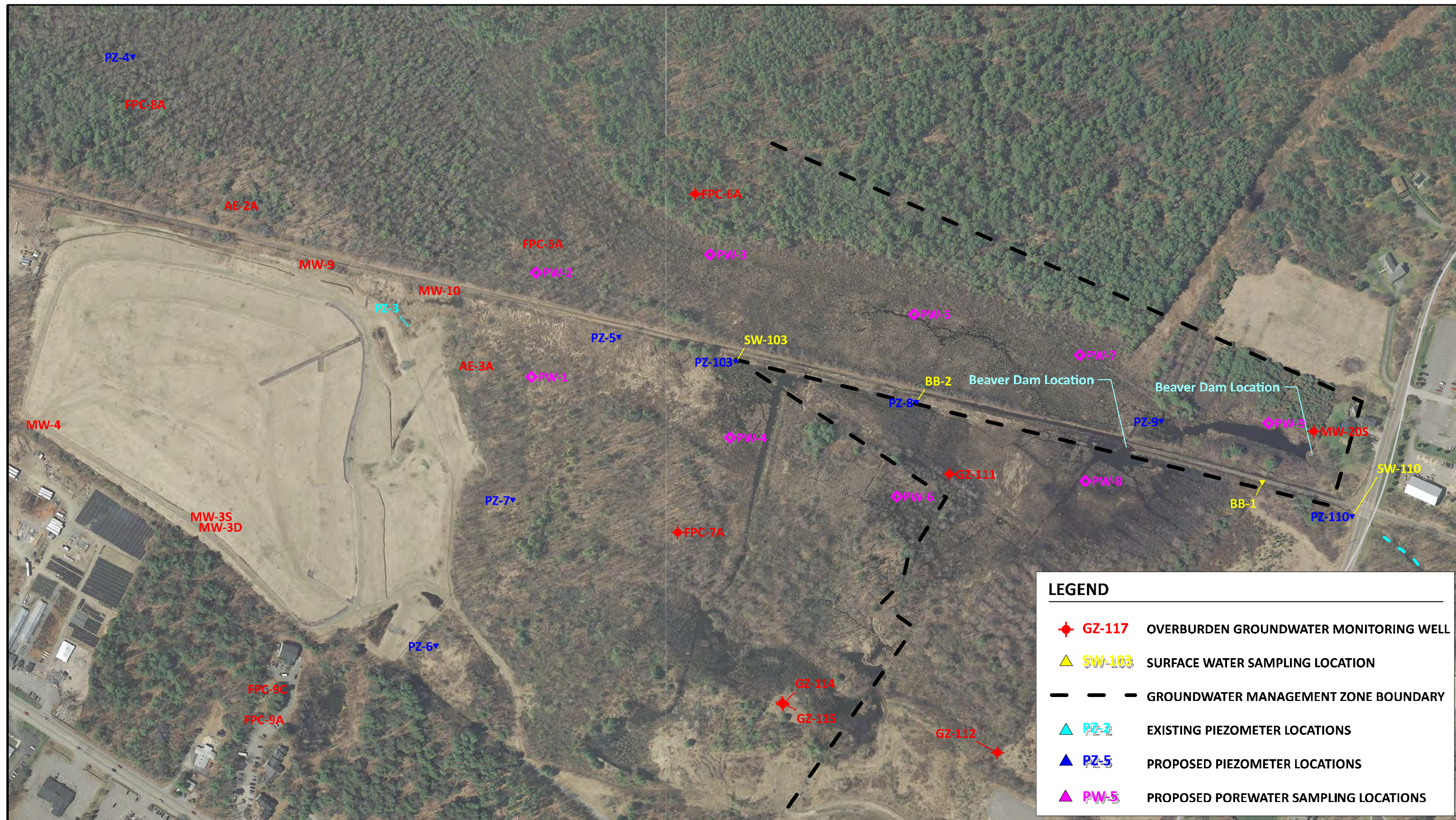
BY:	KWD
DATE:	2020-01-03
APPROVED BY:	MAD
CHECKED BY:	CFB

REV:	
REV DATE:	
ISSUE:	
ISSUE DATE:	

NOTE:

- THIS SITE PLAN IS BASED ON EXISTING SAMPLING LOCATIONS AS PER THE COAKLEY LANDFILL SUPERFUND SITE REVISED SAMPLING AND ANALYSIS PLAN DATED JULY 18, 2018.
- GMZ BOUNDARY IS BASED UPON "GMZ BOUNDARY PLAN" DATED MAY 9, 2008 INCLUDED IN THE 2008 GMP APPLICATION PREPARED BY HANCOCK ASSOCIATES AND 2013 GMZ EXPANSION AREA ESTABLISHED BY THE 2013 GMP DATED JANUARY 7, 2014.
- GIS DATA COURTESY OF NEW HAMPSHIRE ONLINE GRANITE DATABASE.
- MAP IS PROJECTED USING THE NEW HAMPSHIRE STATE PLANE PROJECTION, US FEET AND REFERENCES THE NORTH AMERICAN VERTICAL DATUM OF 1983.





LEGEND

- ◆ **GZ-117** OVERBURDEN GROUNDWATER MONITORING WELL
- ▲ **SW-103** SURFACE WATER SAMPLING LOCATION
- GROUNDWATER MANAGEMENT ZONE BOUNDARY
- ▲ **PZ-2** EXISTING PIEZOMETER LOCATIONS
- ▲ **PZ-5** PROPOSED PIEZOMETER LOCATIONS
- ◆ **PW-5** PROPOSED POREWATER SAMPLING LOCATIONS

PROJECT TITLE: **COAKLEY LANDFILL SUPERFUND SITE
NORTH HAMPTON & GREENLAND, NEW HAMPSHIRE**

SHEET TITLE: **PROPOSED POREWATER SAMPLING LOCATIONS**

DWG: **FIGURE 3**

JN: 10424.020

SCALE: AS SHOWN

BY: KWD

DATE: 2020-01-10

APPROVED BY: MAD

CHECKED BY: CFB

REV: _____

REV DATE: _____

ISSUE: _____

ISSUE DATE: _____

NOTE:

1. THIS SITE PLAN IS BASED ON EXISTING SAMPLING LOCATIONS AS PER THE COAKLEY LANDFILL SUPERFUND SITE REVISED SAMPLING AND ANALYSIS PLAN DATED JULY 18, 2018.

2. GMZ BOUNDARY IS BASED UPON "GMZ BOUNDARY PLAN" DATED MAY 9, 2008 INCLUDED IN THE 2008 GMP APPLICATION PREPARED BY HANCOCK ASSOCIATES AND 2013 GMZ EXPANSION AREA ESTABLISHED BY THE 2013 GMP DATED JANUARY 7, 2014.

3. GIS DATA COURTESY OF NEW HAMPSHIRE ONLINE GRANITE DATABASE.

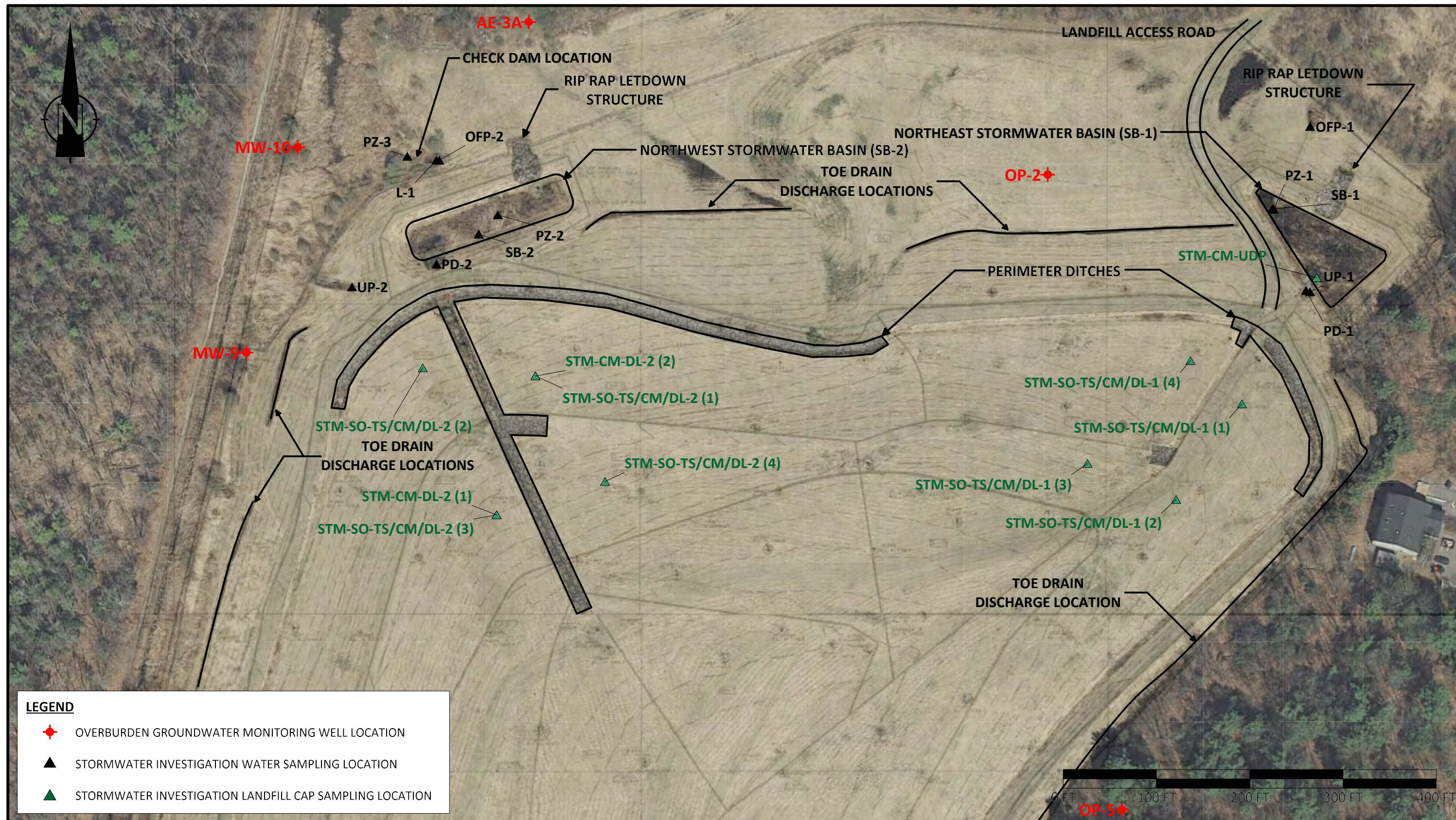
4. MAP IS PROJECTED USING THE NEW HAMPSHIRE STATE PLANE PROJECTION, US FEET AND REFERENCES THE NORTH AMERICAN VERTICAL DATUM OF 1983.



ATTACHMENT A

SELECT REVISED STORMWATER INVESTIGATION REPORT

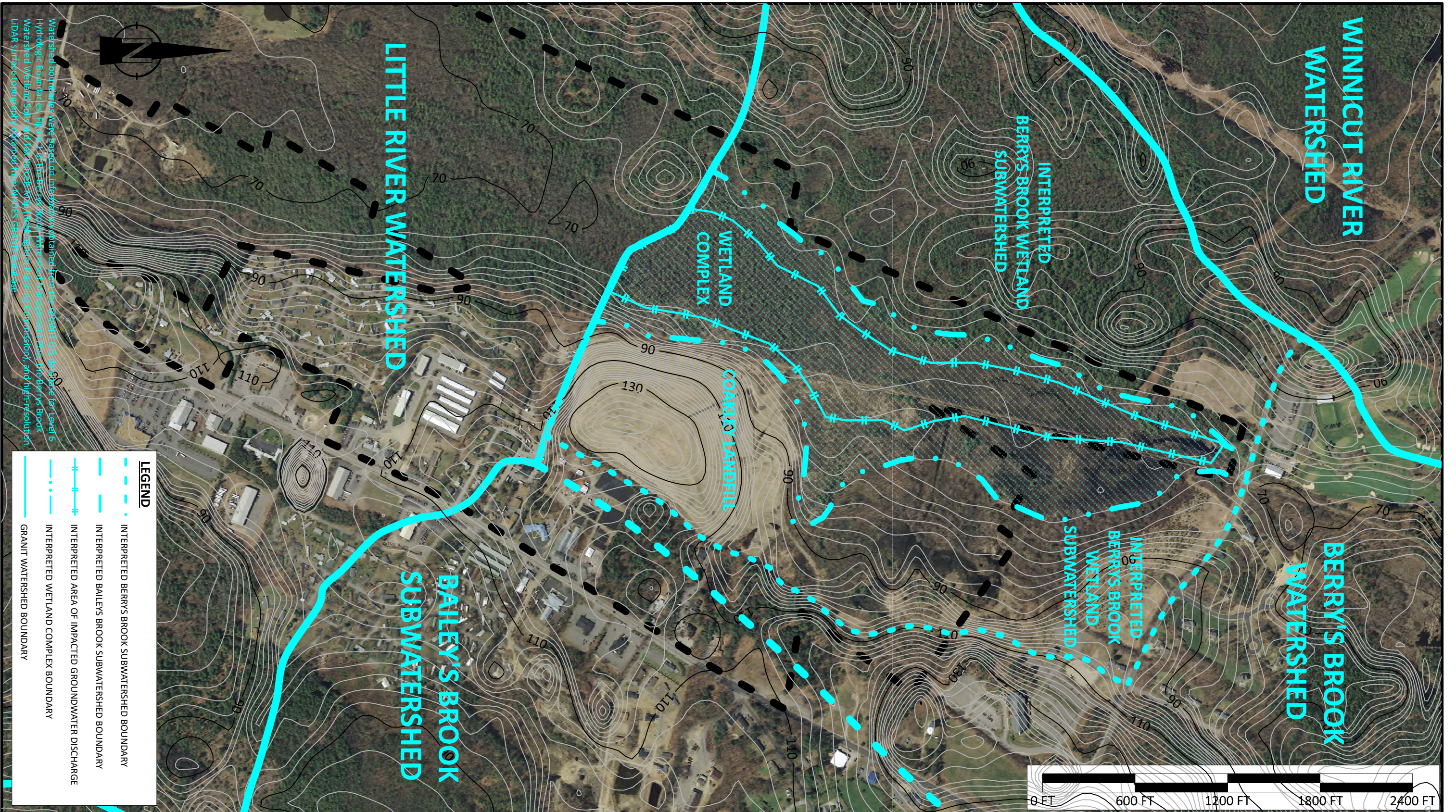
TABLES, FIGURES, AND SOP



LEGEND	
	OVERBURDEN GROUNDWATER MONITORING WELL LOCATION
	STORMWATER INVESTIGATION WATER SAMPLING LOCATION
	STORMWATER INVESTIGATION LANDFILL CAP SAMPLING LOCATION

PROJECT TITLE:	COAKLEY LANDFILL SUPERFUND SITE NORTH HAMPTON & GREENLAND, NEW HAMPSHIRE	DWG:	FIGURE 1	BY:	CFB	REV:		NOTE EXISTING CONDITIONS BASEMAP FROM PLAN TITLED "AS-BUILT SURVEY OF THE COAKLEY LANDFILL, BREAKFAST HILL ROAD, NORTH HAMPTON, N.H." PREPARED BY RICHARD D. BARTLETT & ASSOCIATES, INC. DATED SEPT. 23, 1998. COVER MATERIAL SAMPLE IDENTIFICATION NOMENCLATURE IS BASED ON SAMPLE MATERIAL AND LOCATION. STM-STORMWATER, SO-SOIL, SB-STORMWATER BASIN, UP-UNDERDRAIN PIPE, PD-PERIMETER DITCH, OFF-OUTFALL PIPE, TS-TOPSOIL, CM-CONSTRUCTION MATERIAL, DL-DRAINAGE LAYER, (1)-COMPOSITE SAMPLE NUMBER.
SHEET TITLE:	STORMWATER SAMPLING AND GAUGING LOCATIONS	JN:	10424.020	DATE:	2019-09-24	REV DATE:		
		SCALE:	AS SHOWN	APPROVED BY:	MAD	ISSUE:		
				CHECKED BY:	CFB	ISSUE DATE:		





PROJECT TITLE: **COAKLEY LANDFILL SUPERFUND SITE
NORTH HAMPTON & GREENLAND, NEW HAMPSHIRE**

SHEET TITLE: **COAKLEY LANDFILL WATERSHED BOUNDARY LOCATIONS**

DWG: **FIGURE 3**

JN: 10424.020

SCALE: AS SHOWN

BY: CFB

DATE: 2020-01-14

APPROVED BY: MAD

CHECKED BY: CFB

REV: [REDACTED]

REV DATE: [REDACTED]

ISSUE: [REDACTED]

ISSUE DATE: [REDACTED]

NOTE:

- GMZ BOUNDARY IS BASED UPON "GMZ BOUNDARY PLAN" DATED MAY 9, 2008 INCLUDED IN THE 2008 GMP APPLICATION PREPARED BY HANCOCK ASSOCIATES AND 2013 GMZ EXPANSION AREA ESTABLISHED BY THE 2013 GMP DATED JANUARY 7, 2014.
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- MAP IS PROJECTED USING THE NEW HAMPSHIRE STATE PLANE PROJECTION, US FEET AND REFERENCES THE NORTH AMERICAN VERTICAL DATUM OF 1983.

CES INC
Engineers • Environmental Scientists • Surveyors

TABLE 1
 Summary of Groundwater and Surface Water Elevation Data
 Stormwater Investigation Report
 Coakley Landfill Superfund Site
 North Hampton and Greenland, New Hampshire

	Easting NH State Plane NAD 1983 Feet	Northing NH State Plane NAD 1983 Feet	Ref. Pt Elev. (FT. NGVD)	Fall 2018 Water Elev. FT.	Spring 2019 Water Elev. FT.	Comments
Operable Unit 1						
MW-9	1211077.36	183947.41	81.70	76.55	76.33	Top of Riser
MW-10	1211132.54	184167.68	79.10	73.46	73.62	Top of Riser
OP-2	1211936.99	184138.16	99.00	93.35	93.89	Top of Riser
OP-5	1212016.54	183457.15	108.40	93.39	94.29	Top of Riser
Operable Unit 2						
AE-3A	1211380.24	184301.83	85.00	77.18	76.83	Top of Riser
FPC-5A	1210979.69	184509.92	73.80	73.46	71.98	Top of Riser
FPC-6A	1210835.64	185063.10	78.19	72.43	74.33	Top of Riser
FPC-7A	1211925.71	185037.99	87.60	87.27	87.18	Top of Riser
FPC-9A	1212479.83	183576.85	114.10	93.85	94.28	Top of Riser
Stormwater						
PZ-1	1212179.59	184101.08	99.50	95.25	96.41	Top of Riser
PZ-2	1211347.26	184095.08	84.50	82.38	83.04	Top of Riser
PZ-3	1211250.12	184157.76	81.58	NA	78.60	Top of Riser
L-1	1211281.31	184153.70	78.50	77.19	77.94	Top of Staff Gauge
OFP-1	1212218.65	184189.78	93.20	NA	NA	Invert Elevation of Pipe
OFP-2	1211190.95	184018.72	76.90	NA	NA	Invert Elevation of Pipe
PD-1	1212214.11	184013.95	101.80	NA	NA	Invert Elevation of Pipe
PD-2	1211281.47	184042.12	87.10	NA	NA	Invert Elevation of Pipe
UP-1	1212218.32	184012.51	100.30	NA	NA	Invert Elevation of Pipe
UP-2	1211190.93	184017.80	83.20	NA	NA	Invert Elevation of Pipe
SB-1	1212178.05	184101.54	97.70	97.20	96.44	Top of Staff Gauge
SB-2	1211326.74	184074.27	84.00	81.74	80.93	Top of Staff Gauge
Surface Water						
SW-5	1211286.92	184845.04	75.00	74.04	74.20	Top of Staff Gauge
SW-103	1211367.44	185228.27	74.80	73.52	73.71	Top of Staff Gauge
SW-110	1211874.68	187243.98	68.70	67.21	67.15	Top of Staff Gauge
BB-1	1211763.51	186949.74	72.00	71.74	71.56	Top of Steel Pin
BB-2	1211500.44	185818.19	73.50	72.59	72.44	Top of Steel Pin
LRB - Little River	1208971.20	179648.17	68.90	65.32	64.69	Top of Concrete Headwall

NOTES:

Elevations and locations of reference points were surveyed by TF Moran on 11/16/18 and 3/25/19.

TABLE 2
Landfill Cover Material Analytical Results
Stormwater Investigation Report
Coakley Landfill Superfund Site - North Hampton and Greenland, New Hampshire

SAMPLE IDENTIFICATION	SOILS						CONSTRUCTION MATERIALS	
	STM SO-CM 01	STM SO-CM 02	STM SO-TS 01	STM SO-TS 02	STM SO-DL-01	STM SO-DL-02	STM CM DL 01	STM CM UDP
MATERIAL TYPE	Cover Soil	Cover Soil	Topsoil	Topsoil	Grading Fill/Sand	Grading Fill/Sand	Geotextile	HDPE Pipe
DATE SAMPLED	12/4/2018	12/4/2018	12/4/2018	12/4/2018	12/20/2018	12/20/2018	12/20/2018	12/4/2018
PERFLUORINATED CHEMICALS BY MODIFIED 537 - (mg/kg)								
Perfluorobutanoic Acid (PFBA)	0.000139 U	0.000137 U	0.000416 J	0.000671 J	0.000134 U	0.000138 U	0.000131 U	0.000106 U
Perfluoropentanoic Acid (PFPeA)	0.000200 U	0.000198 U	0.000748 J	0.001090 J	0.000194 U	0.000199 U	0.000189 U	0.000153 U
Perfluorohexanoic Acid (PFHxA)	0.000201 U	0.000199 U	0.000639 J	0.000717 J	0.000194 U	0.000200 U	0.000190 U	0.000154 U
Perfluoroheptanoic Acid (PFHpA)	0.000203 U	0.000200 U	0.000994 J	0.001150 J	0.000196 U	0.000202 U	0.000192 U	0.000156 U
Perfluorohexane Sulfonate (PFHxS)	0.000307 U	0.000303 U	0.000455 J	0.000497 J	0.000297 U	0.000306 U	0.000290 U	0.000235 U
6:2 Fluorotelomer Sulfonic Acid (6:2 FTS)	0.000227 U	0.000224 U	0.000226 U	0.000229 U	0.000219 U	0.000226 U	0.000214 U	0.000174 U
Perfluoroheptane Sulfonic Acid (PFHpS)	0.000168 U	0.000166 U	0.000168 U	0.000170 U	0.000163 U	0.000168 U	0.000159 U	0.000129 U
Perfluorononanoic Acid (PFNA)	0.000579 J	0.001510 J	0.00332	0.00408	0.000171 U	0.000176 U	0.000313 J	0.000135 U
Perfluorooctane Sulfonamide (PFOSA)	0.000225 U	0.000222 U	0.00388	0.00425	0.000217 U	0.000390 J	0.000212 U	0.000172 U
Perfluorodecanoic Acid (PFDA)	0.00275	0.00369	0.0115	0.0137	0.000245 U	0.000253 U	0.000724 J	0.000194 U
8:2 Fluorotelomer Sulfonate (8:2 FTS)	0.000282 U	0.000279 U	0.0024	0.00297	0.000273 U	0.000281 U	0.000266 U	0.000216 U
N-Methyl Perfluorooctane Sulfonamidoacetic Acid (MeFOSAA)	0.000299 U	0.000295 U	0.000882 J	0.000739 J	0.000289 U	0.000298 U	0.000282 U	0.000229 U
N-Ethyl Perfluorooctane Sulfonamidoacetic Acid (EtFOSAA)	0.000318 U	0.000314 U	0.00593	0.00682	0.000308 U	0.000317 U	0.000300 U	0.000244 U
Perfluoroundecanoic Acid (PFUnA)	0.000928 J	0.000979 J	0.0106	0.0107	0.000339 U	0.000349 U	0.000528 J	0.000269 U
Perfluorodecane Sulfonate (PFDS)	0.000533 J	0.000524 J	0.00592	0.00506	0.000193 U	0.000198 U	0.000188 U	0.000153 U
Perfluorododecanoic Acid (PFDoA)	0.000314 J	0.000270 U	0.00543	0.00588	0.000264 U	0.000272 U	0.000315 J	0.000210 U
N-Methyl Perfluorooctane Sulfonamide (MeFOSA)	0.000934 U	0.000922 U	0.000931 U	0.000945 U	0.000903 U	0.000931 U	0.000881 U	0.000716 U
Perfluorotridecanoate (PFTrDA)	0.000121 U	0.000119 U	0.001060 J	0.001210 J	0.000117 U	0.000120 U	0.000114 U	0.0000926 U
Perfluorotetradecanoic Acid (PFTeDA)	0.000196 U	0.000194 U	0.001080 J	0.001000 J	0.000190 U	0.000195 U	0.000185 U	0.000150 U
N-Ethyl Perfluorooctane Sulfonamide (EtFOSA)	0.000133 U	0.001310 U	0.001320 U	0.001340 U	0.001280 U	0.001320 U	0.001250 U	0.001020 U
Perfluorohexadecanoic Acid (PFHxDA)	0.0000346 U	0.0000341 U	0.000148 J	0.000145 J	0.0000334 U	0.0000344 U	0.0000326 U	0.0000265 U
N-Methyl Perfluorooctane Sulfonamidoethanol (MeFOSE)	0.001930 U	0.001910 U	0.006210 J	0.006210 J	0.001870 U	0.001920 U	0.001820 U	0.001480 U
N-Ethyl Perfluorooctane Sulfonamidoethanol (EtFOSE)	0.001000 U	0.000988 U	0.001200 J	0.001040 J	0.000968 U	0.000997 U	0.000944 U	0.000767 U
Perfluorobutane Sulfonic Acid (PFBS)	0.000359 U	0.000355 U	0.000359 U	0.000364 U	0.000348 U	0.000358 U	0.000339 U	0.000276 U
Perfluorooctanoic Acid (PFOA)	0.000497 J	0.000755 J	0.00365	0.00425	0.000226 U	0.000233 U	0.000386 J	0.000179 U
Perfluorooctane Sulfonate (PFOS)	0.00648	0.012	0.0279	0.0396	0.000809 U	0.000834 U	0.00317	0.000642 U

NOTES:

1. J = Estimated concentration below the reporting limit.
2. Q = Ion ratio outside of the 70 - 130 % standard ratio.
3. U = Not detected above the reporting limit
4. ND = Not detected
5. STM-SO-CM = Cover Soil Common Borrow (frost protection) Layer Soil Sample
6. STM-SO-TS - Top Soil (vegetative layer) Sample
7. STM-SO-DL = Grading Fill/Sand Drainage Layer Sample
8. STM-CM-UDP = Construction Material Under Drain Pipe (HDPE) Sample
9. STM-CM-DL = Construction Material Geotextile Fabric over Sand Drainage Layer
10. **Bold** denotes concentrations reported above the applicable reporting limit/Limit of Quantitation

ATTACHMENT B

STANDARD OPERATING PROCEDURE NO. 16 (SOP-16):

GROUNDWATER/SURFACE WATER INTERFACE SAMPLING USING A PORE WATER SAMPLER

GROUNDWATER/SURFACE WATER INTERFACE SAMPLING USING A POREWATER SAMPLER

PURPOSE

The purpose of this standard operating procedure (SOP) is to obtain pore water samples from a location of groundwater/surface water interface using a porewater sampler for analyses that are representative of environmental conditions at the Coakley Landfill Superfund Site in North Hampton and Greenland, New Hampshire. The collection of these samples using the following sampling procedures will be carried out at the locations identified in the Coakley Landfill Sampling and Analysis Plan (SAP).

Any modifications to this SOP shall be approved in advance by the New Hampshire Department of Environmental Services (NHDES) Project Manager and Quality Assurance (QA) Coordinator, in consultation with the United States Environmental Protection Agency (USEPA), documented in the site logbook, and presented in the final report.

It is assumed that sampling can be conducted either from the shore, or by a sampler standing in the water wearing boots or waders.

SAFETY

If a sample cannot be obtained safely, the sample should not be taken at all and the conditions documented in the sampler's field book. Potential dangers include, but are not limited to, uneven and rocky terrain that may cause a fall or other personal injury. All necessary precautionary measures should be heeded when performing these sampling techniques.

GENERAL INFORMATION

1. Each of the regular sampling locations is permanently marked in the field so that sampling points are consistent for each round. All porewater samples shall be located using a global positioning system (GPS) unit.
2. Digital photographs shall be taken at each sampling location, upstream and downstream from the same position. Consistency should be maintained between sampling rounds.
3. Porewater sampling will occur congruent to the groundwater sampling event. Based on weather reports, the sampling team will select the driest period during the Site sampling events to collect the samples, unless otherwise directed by the project manager.
4. Additional information to be recorded on the Porewater Worksheet includes the following:
 - Past 7 days of local meteorological data showing a minimum of daily precipitation totals and barometric pressure;
 - General physical description of the samples and sampling locations; and
 - Descriptions/ID's of digital photographs

POREWATER SAMPLING

This SOP specifically describes the procedures for collecting porewater samples.

EQUIPMENT AND MATERIALS

- Informational materials for sampling event: A copy of the current approved site-specific Health and Safety Plan, site-specific SAP, location map(s), field data from prior sampling events, manuals for sampling, and the monitoring instrument's operation and maintenance manuals, should be brought to the site.
- Appropriate personal protective equipment (PPE).
- New laboratory-supplied wide-mouth glass sample containers (jar) for each sampling location. Extras will be used as transfer vessels to fill pre-preserved sampling containers.
- 0.45-micron filters for each sampling location to collect dissolved metals, as required.
- Logbook, pencil/pen, calculator.
- Appropriate sample containers, pre-preserved as necessary by the laboratory.
- Re-sealable plastic bags to protect and store samples.
- Cooler and loose ice.
- Multi-parameter water quality parameter unit to take in-situ readings for pH, Specific Conductivity, Temperature, oxygen reduction potential (ORP) and dissolved oxygen (DO).
- Appropriate calibration solutions for the multi-parameter instrument.
- Turbidity Meter.
- Calibration solutions for the Turbidity meter.
- Field data from last sampling event, if available.
- Field data sheets, sample labels, chain of custody forms.
- The manufactures instruction manuals for all equipment.
- Paper towels.
- Trash bags to containerize used consumable field supplies.
- Toolbox to include general items such as large and small wrenches, pliers, screw drivers, 25' measuring tape, hose connectors, sharp knife (locking blade), duct tape, at a minimum.
- Decontamination supplies as described in the Decontamination SOP included in the SAP.
- Digital camera.
- Adjustable rate Geotech Peristaltic Pump Series II Variable Speed pump 300 + 600 RPM with Easy Load Peristaltic Pump Heads (that allow 50 ml/minute) and a battery (marine, battery pack, etc)
- ¼" ID x 3/8" OD polyethylene tubing for sample collection – new tubing will be used at each sampling location and disposed.
- Pharmaceutical or surgical grade silicon tubing for pump. For sampling: Thin walled tubing #16 (1/8" x ¼" x 1/16") and/or thin walled tubing #14 (1/16" x 3/16" x 1/16") if necessary to reduce flow to 50 ml/min. For connections: thick walled tubing #15 (3/16" x 3/8" x 3/32" – new tubing will be used at each sampling location and disposed.
- A three way stop cock to divert sample flow (before the multi-parameter meter) to collect turbidity samples.
- Equipment to keep monitoring and sampling equipment off the ground (e.g. table, bucket or polyethylene sheeting).

PRELIMINARY PROCEDURES

1. In general, all instrumentation necessary for field monitoring and health and safety purposes shall be maintained, tested, and inspected according to the manufacturer's instructions. The manufacturer's instruction manuals for field equipment shall be kept on-site with the equipment.
2. All instruments will be successfully calibrated once by the sampling team prior to the sampling event. Instruments will be calibrated and checked according to the Calibration SOP in the SAP.
3. Sampling occurs sequentially from downstream to upstream. Each sampling location is entered from downgradient side.
4. Prepare sampling equipment and bottles on shore.

PROCEDURE USING THE PERISTALTIC PUMP

Preliminary Procedure

1. Set up sampling equipment on shore as if following the low flow sampling procedure. Refer to the attached set-up diagram from the low flow sampling procedure in the SAP. Low flow purging and protocol is not necessary for this procedure. Lay out sheet of clean polyethylene for monitoring and sampling equipment, unless equipment is elevated above the ground (e.g., on a table, bucket, etc.). Be sure to tilt the low flow cell in the ring stand with the outflow connection facing upward to eliminate and prevent air bubbles. Field parameters should be collected from the surface water body that is being recharged from the porewater to be sampled, which will be used to compare to field parameters collected from the porewater.
2. Carefully insert a porewater sampler into the river/stream bed to the desired depth, typically around eight inches in depth. After insertion, remove the strengthening rod from the porewater sampler.
3. Determine and cut the appropriate length of tubing needed to reach the porewater sampling location. Connect the tubing to the porewater sampler.

Sampling Procedure

1. Start the pump at its lowest speed setting and slowly increase the speed until discharge occurs. Continue purging until purge water is relatively clear. Once the purge water has cleared, connect the tubing to the flow through cell and allow parameters to stabilize for at least two minutes.
2. Once the readings have stabilized, record the pH (unit), Specific Conductivity ($\mu\text{S}/\text{cm}$), Temperature ($^{\circ}\text{C}$), ORP (millivolts) and DO (mg/L) on the worksheet.
3. Collect an aliquot of water from the three way stop cock for the Hach and analyze the sample for turbidity. Record the NTU value on the Surface Water Worksheet.
4. Check the tubing; the water flow during sampling needs to be a laminar flow without air bubbles. If air bubbles are observed they can usually be removed by elevating the discharge tube and pump to allow the air to continue rising until discharged with the water.

5. Once a laminar flow is achieved, begin collecting the samples.
 - a) Remove the cap from the sample container and place it on the plastic sheet or in a location where it won't become contaminated.
 - b) Refer to the SAP for specific samples to be collected. The order in which samples should be collected from each well includes:
 - VOCs
 - 1,4-Dioxane, as applicable
 - PFAS - **(Refer to SOP-10 for specific sampling procedures related to PFAS sampling)**
 - Total metals (Dissolved metals, as required)
 - Other parameters, as required
 - c) All sample containers should be filled by allowing the discharge to flow gently down the inside of the container with minimal turbulence. Cap sample containers securely after filling each bottle. Sample containers should be wiped dry.
 - d) If dissolved metals are required, stop the pump, attach a one use only 0.45 micron in-line filter to the tubing, start the pump again, and allow water to rinse through the filter before collecting the sample.
 - e) Field duplicate and matrix spike, matrix spike duplicate (MS/MSD) samples should be collected by filling a separate container for each analysis immediately following the actual field sample collection and should be in the same priority order as indicated above. Refer to SAP for specific QC sampling requirements and appropriate COC notations required for MS/MSD samples.
 - f) Place samples in re-sealable plastic bags and then in loose ice within the cooler. Metals samples do not require cooling.
4. Once the samples have been collected, stop the pump.
5. Disconnect equipment and dispose of the sampling tubing.

REFERENCES

“Protocol for Groundwater/Surface Water Interface Sampling Using A Porewater Sampler”, MEDEP Division of Remediation SOP No. RWM-DR-023, Revision 3, April 28, 2015

ATTACHMENTS

Porewater Sampling Worksheet

**FIELD DATA INFORMATION
PORE WATER SAMPLING LOG**

SITE INFORMATION	
Project:	Date:
Sample ID:	Job Number:
SURFACE WATER INFORMATION	SAMPLE COLLECTION INFORMATION
Channel Width: (ft/inches)	Sample Collection Method:
Depth at Center: (ft/inches)	Water Body/Location ID Sampled:
Approximate Flow Rate: (ft/second)	

SURFACE WATER PARAMETERS

TIME	pH (S.U.)	SP. COND. (μS/CM)	TURB. (NTU)	D.O. (MG/L)	TEMP. (°C)	OBSERVATIONS

PORE WATER PARAMETERS

TIME	pH (S.U.)	SP. COND. (μS/CM)	TURB. (NTU)	D.O. (MG/L)	TEMP. (°C)	OBSERVATIONS

Calibration Record	Date:	Type of Meter:
	Time:	Comments:

Notes:

<u>LOCATION SITE SKETCH</u>

Signature of CES Sampler: _____